
**Measurement of radioactivity in the
environment — Air: radon-222 —**

Part 3:

**Spot measurement method of the
potential alpha energy concentration
of its short-lived decay products**

Mesurage de la radioactivité dans l'environnement — Air: radon 222 —

*Partie 3: Méthode de mesure ponctuelle de l'énergie alpha potentielle
volumique de ses descendants à vie courte*



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Published in Switzerland

Contents

	Page
Foreword	iv
Introduction	v
1 Scope	1
2 Normative references	1
3 Terms, definitions and symbols	1
3.1 Terms and definitions	1
3.2 Symbols	2
4 Principle of the measurement method	3
5 Equipment	3
6 Sampling	4
6.1 General	4
6.2 Sampling objective	4
6.3 Sampling characteristics	4
6.4 Sampling conditions	5
6.4.1 General	5
6.4.2 Installation of sampling system	5
6.4.3 Sampling duration	5
6.4.4 Volume of air sampled	5
7 Detection method	5
8 Measurement	5
8.1 Procedure	5
8.2 Influence quantities	6
8.3 Calibration	6
9 Expression of results	7
9.1 General	7
9.2 Potential alpha energy concentration	7
9.3 Standard uncertainty	7
9.4 Decision threshold	8
9.5 Detection limit	9
9.6 Limits of the confidence interval	9
10 Test report	9
Annex A (informative) Examples of gross alpha counting protocols	11
Annex B (informative) Calculation of the coefficients $k_{218\text{Po},j}$, $k_{214\text{Pb},j}$ and $k_{214\text{Bi},j}$	12
Annex C (informative) Measurement method using gross alpha counting according to the Thomas protocol	16
Bibliography	19

Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

The procedures used to develop this document and those intended for its further maintenance are described in the ISO/IEC Directives, Part 1. In particular the different approval criteria needed for the different types of ISO documents should be noted. This document was drafted in accordance with the editorial rules of the ISO/IEC Directives, Part 2 (see www.iso.org/directives).

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For an explanation of the voluntary nature of standards, the meaning of ISO specific terms and expressions related to conformity assessment, as well as information about ISO's adherence to the World Trade Organization (WTO) principles in the Technical Barriers to Trade (TBT) see the following URL: : www.iso.org/iso/foreword.html

This document was prepared by Technical Committee ISO/TC 85, *Nuclear energy, nuclear technologies, and radiological protection*, Subcommittee SC 2, *Radiological protection*.

This second edition cancels and replaces the first edition (ISO 11665-3:2012), of which it constitutes a minor revision. The changes compared to the previous edition are as follows:

- update of the Introduction;
- update of the Bibliography.

A list of all the parts in the ISO 11665 series can be found on the ISO website.

Any feedback or questions on this document should be directed to the user's national standards body. A complete listing of these bodies can be found at www.iso.org/members.html.

Introduction

Radon isotopes 222, 219 and 220 are radioactive gases produced by the disintegration of radium isotopes 226, 223 and 224, which are decay products of uranium-238, uranium-235 and thorium-232 respectively, and are all found in the earth's crust (see ISO 11665-1:2019, Annex A for further information). Solid elements, also radioactive, followed by stable lead are produced by radon disintegration^[1].

When disintegrating, radon emits alpha particles and generates solid decay products, which are also radioactive (polonium, bismuth, lead, etc.). The potential effects on human health of radon lie in its solid decay products rather than the gas itself. Whether or not they are attached to atmospheric aerosols, radon decay products can be inhaled and deposited in the bronchopulmonary tree to varying depths according to their size^{[2][3][4][5]}.

Radon is today considered to be the main source of human exposure to natural radiation. UNSCEAR^[6] suggests that, at the worldwide level, radon accounts for around 52 % of global average exposure to natural radiation. The radiological impact of isotope 222 (48 %) is far more significant than isotope 220 (4 %), while isotope 219 is considered negligible (see ISO 11665-1:2019, Annex A). For this reason, references to radon in this document refer only to radon-222.

Radon activity concentration can vary from one to more orders of magnitude over time and space. Exposure to radon and its decay products varies tremendously from one area to another, as it depends on the amount of radon emitted by the soil and building materials, weather conditions, and on the degree of containment in the areas where individuals are exposed.

As radon tends to concentrate in enclosed spaces like houses, the main part of the population exposure is due to indoor radon. Soil gas is recognized as the most important source of residential radon through infiltration pathways. Other sources are described in other parts of ISO 11665 and ISO 13164 series for water^[7].

Radon enters into buildings via diffusion mechanism caused by the all-time existing difference between radon activity concentrations in the underlying soil and inside the building, and via convection mechanism inconstantly generated by a difference in pressure between the air in the building and the air contained in the underlying soil. Indoor radon activity concentration depends on radon activity concentration in the underlying soil, the building structure, the equipment (chimney, ventilation systems, among others), the environmental parameters of the building (temperature, pressure, etc.) and the occupants' lifestyle.

To limit the risk to individuals, a national reference level of 100 Bq.m⁻³ is recommended by the World Health Organization^[5]. Wherever this is not possible, this reference level should not exceed 300 Bq.m⁻³. This recommendation was endorsed by the European Community Member States that should establish national reference levels for indoor radon activity concentrations. The reference levels for the annual average activity concentration in air should not be higher than 300 Bq.m⁻³^[5].

To reduce the risk to the overall population, building codes should be implemented that require radon prevention measures in buildings under construction and radon mitigating measures in existing buildings. Radon measurements are needed because building codes alone cannot guarantee that radon concentrations are below the reference level.

Variations of a few nanojoules per cubic metre to several thousand nanojoules per cubic metre are observed in the potential alpha energy concentration of short-lived radon decay products.

The potential alpha energy concentration of short-lived radon-222 decay products in the atmosphere can be measured by spot and integrated measurement methods (see ISO 11665-1). This document deals with spot measurement methods. A spot measurement of the potential alpha energy concentration relates to the time when the measurement is taken and has no significance in annual exposure. This type of measurement does not therefore apply when assessing the annual exposure.

NOTE The origin of radon-222 and its short-lived decay products in the atmospheric environment are described generally in ISO 11665-1 together with measurement methods.

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Measurement of radioactivity in the environment — Air: radon-222 —

Part 3:

Spot measurement method of the potential alpha energy concentration of its short-lived decay products

1 Scope

This document describes spot measurement methods for determining the activity concentration of short-lived radon-222 decay products in the air and for calculating the potential alpha energy concentration.

This document gives indications for performing a spot measurement of the potential alpha energy concentration, after sampling at a given place for several minutes, and the conditions of use for the measuring devices.

The measurement method described is applicable for a rapid assessment of the potential alpha energy concentration. The result obtained cannot be extrapolated to an annual estimate potential alpha energy concentration of short-lived radon-222 decay products. Thus, this type of measurement is not applicable for the assessment of annual exposure or for determining whether or not to mitigate citizen exposures to radon or radon decay products.

This measurement method is applicable to air samples with potential alpha energy concentration greater than 5 nJ/m³.

NOTE This document does not address the potential contribution of radon-220 decay products.

2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 11665-1, *Measurement of radioactivity in the environment — Air: radon-222 — Part 1: Origins of radon and its short-lived decay products and associated measurement methods*

ISO/IEC 17025, *General requirements for the competence of testing and calibration laboratories*

IEC 61577-1, *Radiation protection instrumentation — Radon and radon decay product measuring instruments — Part 1: General principles*

IEC 61577-3, *Radiation protection instrumentation — Radon and radon decay product measuring instruments — Part 3: Specific requirements for radon decay product measuring instruments*

3 Terms, definitions and symbols

3.1 Terms and definitions

For the purposes of this document, the terms and definitions given in ISO 11665-1 apply.

3.2 Symbols

For the purposes of this document, the symbols given in ISO 11665-1 and the following apply.

C_i	activity concentration of the nuclide i , in becquerels per cubic metre
$E_{AE,i}$	alpha particle energy produced by the disintegration of the nuclide i , in joules
$E_{AEt,i}$	total alpha particle energy potentially produced by the nuclide i , in joules
$E_{PAE,i}$	potential alpha energy of the nuclide i , in joules
$E_{PAEC,i}$	potential alpha energy concentration of the nuclide i , in joules per cubic metre
$E_{PAEC,i}^*$	decision threshold of the potential alpha energy concentration of the nuclide i , in joules per cubic metre
$E_{PAEC,i}^\#$	detection limit of the potential alpha energy concentration of the nuclide i , in joules per cubic metre
$E_{PAEC,i}^<$	lower limit of the confidence interval of the potential alpha energy concentration of the nuclide i , in joules per cubic metre
$E_{PAEC,i}^>$	upper limit of the confidence interval of the potential alpha energy concentration of the nuclide i , in joules per cubic metre
I_j	j^{th} number of gross counts obtained between times t_j and t_{cj}
$I_{0,j}$	j^{th} number of background counts obtained between times t_j and t_{cj}
$k_{i,j}$	coefficient related to the j^{th} number of gross count for radon decay product i , depending on the decay constants of the radon decay products, the sampling duration, t_s , and the times t_j and t_{cj} , per square second
N_i	number of atoms of the nuclide i
n	counting number depending on the gross alpha counting protocol used
Q	sampling flowrate, in cubic metres per second
t_{cj}	end time of counting j , in seconds
t_j	start time of counting j , in seconds
t_s	sampling duration, in seconds
U	expanded uncertainty calculated by $U = k \cdot u(\)$ with $k = 2$
$u(\)$	standard uncertainty associated with the measurement result
$u_{\text{rel}}(\)$	relative standard uncertainty
V	sampled volume, in cubic metres
ε_c	counting efficiency, in pulses per disintegration
λ_i	decay constant of the nuclide i , per second

4 Principle of the measurement method

Spot measurement of the potential alpha energy concentration of short-lived radon-222 decay products is based on the following elements:

- grab sampling, at time t , of short-lived radon decay products contained in a volume of air representative of the atmosphere under investigation, using a high-efficiency filtering membrane;
- repeated gross alpha measurements of the collected decay products using a detector sensitive to alpha particles; the counting stage starts after sampling has stopped;
- calculation of the activity concentrations of the radon decay products using the laws of radioactive decay and the counting results from a preset duration, repeated at given times.

The gross alpha measurement method quantifies alpha particles emitted by short-lived radon decay products. The ^{222}Rn decay product chain shows that 99,98 % of the decays of ^{218}Po result in the emission of alpha particles. It can, therefore, be considered as a pure alpha emitter. ^{214}Pb and ^{214}Bi are not alpha emitters, but they contribute to the appearance of alpha particles from the decay of ^{214}Po .

After collecting the air sample, the gross alpha activity is measured for various counting durations. Because of the fast decay of radon decay products, the isotopic composition of a sample rapidly changes during collection as well as during the counting durations. Repeated measurements of the gross alpha activity are necessary in order to describe the decay of the sample and thereby calculate the amounts of the various decay products which were originally collected in the air sample.

NOTE Although ^{222}Rn and its decay products are usually found in higher quantity, environmental air samples can also contain significant activity of radionuclides of the ^{220}Rn decay chain as well as other airborne long-lived radionuclides. In such cases, the formulas and procedures given in this document need to be adapted to take into account these additional radionuclides.

5 Equipment

The apparatus shall include a sampling system and a detection system composed of a detector connected to a counting system (see [Figure 1](#)). The measuring devices used shall be in accordance with IEC 61577-1 and IEC 61577-3.

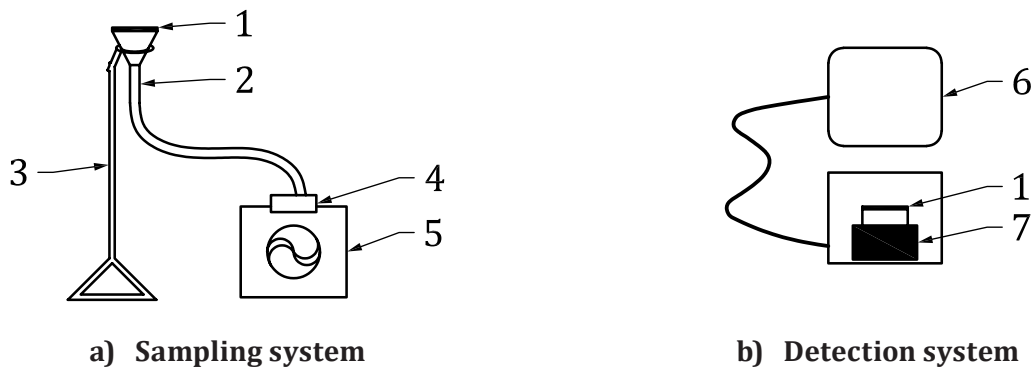
The sampling system shall include the following components:

- an open filter holder allowing fast and easy removal of the filter after sampling;
- a pump;
- a high-efficiency particulate air filter (HEPA filter with a minimum efficiency of 99,97 % for a particle size of $0,3\ \mu\text{m}$);
- a flowmeter and a chronometer;

Possible detectors include the following:

- a photomultiplier associated with a sensitive scintillation surface [for example $\text{ZnS}(\text{Ag})$];
- a silicon semi-conductor that is sensitive to alpha particles.

The detector, connected to a pulse counting system, shall have a sensitive detection surface at least equal in diameter to the filtering membrane.



Key

- 1 filtering membrane
- 2 filter holder
- 3 support
- 4 flowmeter and chronometer
- 5 pump
- 6 counting system
- 7 detector

Figure 1 — Functional diagram of a spot measuring system for potential alpha energy concentration of short-lived radon decay products

6 Sampling

6.1 General

Grab sampling is representative of the potential alpha energy concentration of short-lived radon-222 decay products at a given time and a given place.

6.2 Sampling objective

The sampling objective is to collect, without interruption, all the aerosols, regardless of their size (unattached and attached fractions), carrying short lived radon decay products and contained in the ambient air during a given sampling duration (<1 h).

6.3 Sampling characteristics

The unattached and attached fractions of short-lived radon decay products shall be sampled without interruption from the atmosphere under investigation by pumping and filtering a known volume of air through a high-efficiency collection membrane located in an open filter holder. The air sampling shall be omni-directional.

In order to count the emitted alpha particles correctly, the sampling system shall conduct to the surface deposit of the radionuclides on the filter and shall prevent the aerosols from being buried.

The sampling system shall be used in conditions that preclude clogging of the filtering membrane, which would cause self-absorption of the alpha emissions of particles collected on the filter or a reduction in the sampling flowrate over time.

6.4 Sampling conditions

6.4.1 General

Sampling shall be carried out as specified in ISO 11665-1. The sampling location, date and time shall be recorded.

6.4.2 Installation of sampling system

Installation of the sampling system shall be carried out as specified in ISO 11665-1.

6.4.3 Sampling duration

Given the short half-lives of the radon-222 decay products, particularly ^{218}Po , the sampling duration should normally be less than or equal to 20 min. A longer sampling duration would not improve the detection limit of the method.

6.4.4 Volume of air sampled

The volume of air sampled shall be ascertained by continuous measurement of the flowrate during sampling with a calibrated system (for example a sonic nozzle) (see IEC 61577-3).

7 Detection method

Detection shall be performed using silver-activated zinc sulphide $\text{ZnS}(\text{Ag})$ scintillation or a semi-conductor (alpha detection), as described in ISO 11665-1.

8 Measurement

8.1 Procedure

Measurement shall be carried out as follows.

- a) Select the sampling duration, t_s .
- b) Plan the counting stage, with n countings, and choose start time t_j and end time t_{cj} for each number of counts I_j . The different sets are organized from $j = 1$ to $j = n$. Before a set of counting, a specific waiting time can be required.

NOTE Examples of gross alpha counting protocols are given in [Annex A](#). The measurement method using gross alpha counting according to the Thomas protocol is detailed in [Annex C](#).

- c) Install the detection system (detector and pulse counting system).
- d) Determine the background level of the filtering membrane. Before carrying out sampling, position the virgin membrane opposite the detector, in accordance with manufacturer recommendations. Measure the virgin membrane by means of n successive gross alpha countings during specific counting durations $t_{cj} - t_j$ according to the counting stage selected:
 - 1) $t = 0$ to $t = t_1$ standby, there is no count if $t_1 > 0$;
 - 2) $t = t_1$ to $t = t_{c1}$ count $I_{0,1}$ is performed;
 - 3) $t = t_{cj-1}$ to $t = t_j$ standby, there is no count if $t_j > t_{cj-1}$;
 - 4) $t = t_j$ to $t = t_{cj}$ count $I_{0,j}$ is performed.

If $n > 1$, repeat stages 3) and 4) until $j = n$.

- e) Record values of $I_{0,j}$ for $j = 1$ to $j = n$.
- f) Select and locate the measuring point.
- g) Install the sampling system.
- h) Using grab sampling, obtain an air sample representative of the atmosphere under investigation during the sampling duration t_s .
- i) Record the location and the time (date, hour and minutes) of sampling.
- j) Once sampling is completed, remove the filtering membrane from the sampling system and position it opposite the detector, in accordance with manufacturer recommendations. Given the short half-lives of the radon-222 decay products, the alpha particles shall be detected on the sampling site within a few minutes of sampling.
- k) Perform n successive gross alpha countings of the membrane with specific counting durations $t_{c,j} - t_j$ according to the counting stage selected:
 - 1) $t = 0$ to $t = t_1$ standby, there is no count if $t_1 > 0$;
 - 2) $t = t_1$ to $t = t_{c1}$ count I_1 is performed;
 - 3) $t = t_{c,j-1}$ to $t = t_j$ standby, there is no count if $t_j > t_{c,j-1}$;
 - 4) $t = t_j$ to $t = t_{c,j}$ count I_j is performed.

If $n > 1$, repeat stages 3) and 4) until $j = n$.

- l) Record values of I_j for $j = 1$ to $j = n$.
- m) Determine the potential alpha energy concentration by calculation.

8.2 Influence quantities

Various quantities can lead to measurement bias that could induce non-representative results. Depending on the measurement method and the control of usual influence quantities specified in IEC 61577-1 and ISO 11665-1, the following quantities shall be considered in particular:

- a) influence of atmospheric pressure on the sampling process;
- b) influence of the filtering membrane storage conditions before sampling starts; the storage conditions shall be so designed to avoid contamination of the filtering membrane with radon decay products;
- c) detector surface contamination; the surface contamination of the detector shall be controlled before performing the measurement;
- d) potential presence of other alpha emitters (radium, radon isotopes, etc.) on the filtering membrane or in the ambient air.

Manufacturer recommendations in the operating instructions for the measuring devices shall be followed.

8.3 Calibration

The entire measuring device (sampling system and detection system, i.e. detector and related electronics) shall be calibrated as specified in ISO 11665-1.

The relationship between the variable measured by the detection system and the potential alpha energy concentration of the radon decay products in the air shall be established by using reference radioactive sources or another standard (for example a reference atmosphere) recognized through international inter-comparison programmes.

9 Expression of results

9.1 General

Calculation of the potential alpha energy concentration of short-lived radon-222 decay products is based on the activity concentration of each short-lived decay product as well as the total potential alpha energy concentration.

Calculation of the activity concentration of ^{218}Po , ^{214}Pb and ^{214}Bi is based on several gross alpha counts I_j , the detector background level $I_{0,j}$, the counting efficiency, the flow-rate and the sampling duration. The following hypotheses shall be applied:

- the short-lived radon decay products are the only alpha-emitting nuclides present in the air being analysed;
- their respective activity concentration does not change during sampling;
- the counting efficiency is the same for each decay product.

The activity concentration of each decay product is calculated using equations that express the number of atoms of each decay product present on the filter at the end of the sampling process based on the gross alpha counts obtained over the different time intervals (see [Annex B](#)).

9.2 Potential alpha energy concentration

The potential alpha energy concentration of short-lived radon-222 decay products shall be calculated as given by [Formula \(1\)](#):

$$E_{\text{PAEC},222\text{Rn}} = \sum_i \frac{E_{\text{PAE},i}}{V} = \sum_i \left(\frac{E_{\text{AET},i} \cdot N_i}{V_i} \right) = \sum_i \left(\frac{E_{\text{AET},i} \cdot C_i}{\lambda_i} \right) \quad (1)$$

$$E_{\text{PAEC},222\text{Rn}} = \omega \cdot \sum_j \sum_i \frac{E_{\text{AET},i} \cdot k_{i,j}}{\lambda_i} \cdot (I_j - I_{0,j}) \quad (2)$$

where

$$C_i = \frac{1}{\varepsilon_c \cdot Q} \cdot \sum_j k_{i,j} \cdot (I_j - I_{0,j}) = \omega \cdot \sum_j k_{i,j} \cdot (I_j - I_{0,j}) \quad (3)$$

$$\omega = \frac{1}{\varepsilon_c \cdot Q} \quad (4)$$

A method of calculation of $k_{i,j}$ is detailed in [Annex B](#).

NOTE For ^{218}Po , $E_{\text{AET},i} = E_{\text{AE},218\text{Po}} + E_{\text{AE},214\text{Po}}$. For ^{214}Pb , ^{214}Bi and ^{214}Po , $E_{\text{AET},i} = E_{\text{AE},214\text{Po}}$.

9.3 Standard uncertainty

The uncertainties of the sampling flowrate, the counting efficiency and the number of counts (including the background level) shall be taken into account.

The uncertainties of decay constants, sampling duration and counting durations are considered negligible. The uncertainty of $k_{i,j}$ is therefore considered negligible.

By hypothesis:

- a) the variables are all independent;
- b) the numbers of counts $I_{0,j}$ and I_j are normal variables according to Poisson's law.

Under these conditions, the uncertainties of numbers of counts $I_{0,j}$ and I_j are expressed as follows:

$$u^2(I_{0,j}) = I_{0,j} \text{ and } u^2(I_j) = I_j \quad (5)$$

I_j depends on the activity of each decay product as well as on the time elapsed since the end of the sampling process. The counting uncertainty estimated from the variance of I_j therefore includes uncertainties associated with the variables on which I_j depends.

In accordance with ISO/IEC Guide 98-3^[8], the standard uncertainty of $E_{\text{PAEC},222_{\text{Rn}}}$ shall be calculated as given by [Formula \(6\)](#):

$$u(E_{\text{PAEC},222_{\text{Rn}}}) = \sqrt{\omega^2 \cdot \sum_j [(K_{i,j}) \cdot (I_j + I_{0,j})] + (E_{\text{PAEC},222_{\text{Rn}}})^2 \cdot u_{\text{rel}}^2(\omega)} \quad (6)$$

where

$$u_{\text{rel}}^2(\omega) = u_{\text{rel}}^2(\varepsilon_c) + u_{\text{rel}}^2(Q) \quad (7)$$

$$K_{i,j} = \left[\sum_i \left(\frac{E_{\text{AET},i} \times k_{i,j}}{\lambda_i} \right) \right]^2 \quad (8)$$

Calculation of the characteristic limits [see ISO 11929 (all parts)], requires calculation of $\tilde{u}(\tilde{E}_{\text{PAEC},222_{\text{Rn}}})$, i.e. the standard uncertainty of $E_{\text{PAEC},222_{\text{Rn}}}$ as a function of its true value, calculated as given in [Formula \(9\)](#):

$$\tilde{u}(\tilde{E}_{\text{PAEC},222_{\text{Rn}}}) = \sqrt{\omega^2 \cdot \sum_j [(K_{i,j}) \cdot (\tilde{I}_j + I_{0,j})] + (\tilde{E}_{\text{PAEC},222_{\text{Rn}}})^2 \cdot u_{\text{rel}}^2(\omega)} \quad (9)$$

9.4 Decision threshold

The decision threshold, $E_{\text{PAEC},222_{\text{Rn}}}^*$, is obtained from [Formula \(9\)](#) for $\tilde{E}_{\text{PAEC},222_{\text{Rn}}} = 0$ [see ISO 11929 (all parts)], i.e. each $\tilde{C}_i = 0$ and $\tilde{I}_j = I_{0,j}$. This yields [Formula \(10\)](#):

$$E_{\text{PAEC},222_{\text{Rn}}}^* = k_{1-\alpha} \cdot \tilde{u}(0) = k_{1-\alpha} \cdot \omega \cdot \sqrt{2 \cdot \sum_j [(K_{i,j}) \cdot I_{0,j}]} \quad (10)$$

$\alpha = 0,05$ with $k_{1-\alpha} = 1,65$ is often chosen by default.

9.5 Detection limit

The detection limit, $E_{\text{PAEC},222_{\text{Rn}}}^{\#}$, is calculated as given in [Formula \(11\)](#) [see ISO 11929 (all parts)]:

$$E_{\text{PAEC},222_{\text{Rn}}}^{\#} = a + \sqrt{a^2 + (k_{1-\beta}^2 - k_{1-\alpha}^2) \cdot \tilde{u}^2(\tilde{E}_{\text{PAEC}} = 0)} = a + \sqrt{a^2 + (k_{1-\beta}^2 - k_{1-\alpha}^2) \cdot \tilde{u}^2(0)} \quad (11)$$

with

$$a = k_{1-\alpha} \cdot \tilde{u}(0) + \frac{1}{2} \cdot \left(\frac{k_{1-\beta}^2}{E_{\text{PAEC}}} \right) \cdot [u^2(E_{\text{PAEC}}) - \tilde{u}^2(0)] \quad (12)$$

If $\alpha = \beta$, then it follows that $E_{\text{PAEC}}^{\#} = 2 \cdot a$.

$\alpha = \beta = 0,05$ with $k_{1-\alpha} = k_{1-\beta} = 1,65$ is often chosen by default.

9.6 Limits of the confidence interval

The lower, $E_{\text{PAEC},222_{\text{Rn}}}^{\triangleleft}$, and upper, $E_{\text{PAEC},222_{\text{Rn}}}^{\triangleright}$, limits of the confidence interval shall be calculated using [Formulae \(13\)](#) and [\(14\)](#) [see ISO 11929 (all parts)]:

$$E_{\text{PAEC},222_{\text{Rn}}}^{\triangleleft} = E_{\text{PAEC},222_{\text{Rn}}} - k_p \cdot u(E_{\text{PAEC},222_{\text{Rn}}}); \quad p = \omega \cdot (1 - \gamma/2) \quad (13)$$

$$E_{\text{PAEC},222_{\text{Rn}}}^{\triangleright} = E_{\text{PAEC},222_{\text{Rn}}} + k_q \cdot u(E_{\text{PAEC},222_{\text{Rn}}}); \quad q = 1 - \omega \cdot \gamma/2 \quad (14)$$

where

$\omega = \Phi[y/u(y)]$, Φ being the distribution function of the standardized normal distribution;

$\omega = 1$ may be set if $E_{\text{PAEC},222_{\text{Rn}}} \geq 4 \cdot u(E_{\text{PAEC},222_{\text{Rn}}})$, in which case:

$$E_{\text{PAEC},222_{\text{Rn}}}^{\triangleleft \triangleright} = E_{\text{PAEC},222_{\text{Rn}}} \pm k_{1-\gamma/2} \cdot u(E_{\text{PAEC},222_{\text{Rn}}}) \quad (15)$$

$\gamma = 0,05$ with $k_{1-\gamma/2} = 1,96$ are often chosen by default.

10 Test report

10.1 The test report shall be in accordance with the requirements of ISO/IEC 17025 and shall contain the following information:

- a reference to this document, i.e. ISO 11665-3:2020;
- measurement method (spot);
- identification of the sample;
- sampling characteristic (active);
- start time of sampling (date, hour and minutes);
- end time of sampling (date, hour and minutes);
- duration of sampling;

- h) sampling location;
- i) units in which the results are expressed;
- j) test result, $E_{\text{PAEC},222_{\text{Rn}}} \pm u(E_{\text{PAEC},222_{\text{Rn}}})$ or $E_{\text{PAEC},222_{\text{Rn}}} \pm U$, with the associated k value.

10.2 Complementary information may be provided, such as the following:

- a) purpose of the measurement;
- b) probabilities α , β and $(1-\gamma)$;
- c) the decision threshold and the detection limit; depending on the customer request, there are different ways to present the result:
 - 1) when the potential alpha energy concentration of the short-lived radon-222 decay products is compared with the decision threshold [see ISO 11929 (all parts)], the result of the measurement shall be expressed as $\leq E_{\text{PAEC},222_{\text{Rn}}}^*$ if the result is below the decision threshold;
 - 2) when the potential alpha energy concentration of the short-lived radon-222 decay products is compared with the detection limit, the result of the measurement shall be expressed as $\leq E_{\text{PAEC},222_{\text{Rn}}}^{\#}$ if the result is below the detection limit or, if the detection limit exceeds the guideline value, it shall be documented that the method is not suitable for the measurement purpose;
- d) any relevant information likely to affect the results:
 - 1) weather conditions at the time of sampling;
 - 2) ventilation conditions for indoor measurement (mechanical ventilation system, doors and windows open or shut, etc.).

10.3 The results can be expressed in a similar format to that shown in ISO 11665-1:2019, Annex C.

Annex A

(informative)

Examples of gross alpha counting protocols

There are several gross alpha counting protocols associated with spot measurement methods for the potential alpha energy concentration of short-lived radon-222 decay products described in this document

Some of them, that are suitable for the purposes of this document, are listed in [Table A.1](#).

Table A.1 — Examples of gross alpha counting protocols

Method	Duration of the different phases s						
	Sampling	Standby	1st count	Standby	2 nd count	Standby	3 rd count
Thomas ^[10]	300	120	180	60	840	60	540
Thomas ^[10] + Hartley ^{[11][12]}	Variable						
Markov ^[13]	300	60	180	180	180		
Nazaroff ^[14]	300	60	600	600	1 140		
Miller ^{[15][16]}	120	30	120				
Kusnetz ^[17]	300 to 600	2 400 to 5 400					
Rolle ^[18]	120	480	120				

Annex B (informative)

Calculation of the coefficients $k_{218\text{Po},j}$, $k_{214\text{Pb},j}$ and $k_{214\text{Bi},j}$

B.1 General

This annex deals with the method of determination for the coefficients $k_{218\text{Po},j}$, $k_{214\text{Pb},j}$ and $k_{214\text{Bi},j}$.

NOTE For definitions of the symbols used in this annex, see [Clause 3](#).

B.2 Determination method

B.2.1 Determination of the number of alpha disintegrations

After sampling is completed, the expected number of alpha disintegrations, n_α , during the time interval $t_{cj} - t_j$ is given by [Formula \(B.1\)](#):

$$\begin{aligned}
 n_\alpha = & \left[N_{218\text{Po}} + \frac{\lambda_{214\text{Pb}} \cdot \lambda_{214\text{Bi}} \cdot N_{218\text{Po}}}{(\lambda_{214\text{Bi}} - \lambda_{218\text{Po}}) \cdot (\lambda_{214\text{Pb}} - \lambda_{218\text{Po}})} \right] \cdot (e^{-\lambda_{218\text{Po}} \cdot t_j} - e^{-\lambda_{218\text{Po}} \cdot t_{cj}}) \\
 & + \left[\frac{\lambda_{218\text{Po}} \cdot \lambda_{214\text{Bi}} \cdot N_{218\text{Po}}}{(\lambda_{218\text{Po}} - \lambda_{214\text{Pb}}) \cdot (\lambda_{214\text{Bi}} - \lambda_{214\text{Pb}})} + \frac{\lambda_{214\text{Bi}} \cdot N_{214\text{Pb}}}{\lambda_{214\text{Bi}} - \lambda_{214\text{Pb}}} \right] \cdot (e^{-\lambda_{214\text{Pb}} \cdot t_j} - e^{-\lambda_{214\text{Pb}} \cdot t_{cj}}) \\
 & + \left[\frac{\lambda_{218\text{Po}} \cdot \lambda_{214\text{Pb}} \cdot N_{218\text{Po}}}{(\lambda_{218\text{Po}} - \lambda_{214\text{Bi}}) \cdot (\lambda_{214\text{Pb}} - \lambda_{214\text{Bi}})} + \frac{\lambda_{214\text{Pb}} \cdot N_{214\text{Pb}}}{\lambda_{214\text{Pb}} - \lambda_{214\text{Bi}}} + N_{214\text{Bi}} \right] \cdot (e^{-\lambda_{214\text{Bi}} \cdot t_j} - e^{-\lambda_{214\text{Bi}} \cdot t_{cj}})
 \end{aligned} \quad (\text{B.1})$$

where $N_{218\text{Po}}$, $N_{214\text{Pb}}$ et $N_{214\text{Bi}}$ are the number of atoms for ^{218}Po , ^{214}Pb and ^{214}Bi , collected on the membrane filter at the end of sampling.

To determine this number of alpha disintegrations, counting has to be performed once between t_j and t_{cj} .

The number of countings that it is necessary to perform depends on the gross alpha counting protocol used (see [Annex A](#)). From these counting results, $I_j - I_{0,j}$, the number of atoms of each radon decay product collected on the filter at the end of sampling ($N_{218\text{Po}}$, $N_{214\text{Pb}}$ and $N_{214\text{Bi}}$) can be deduced.

B.2.2 Determination of the activity concentration of each radon decay product

The activity concentration of each radon decay product is obtained from [Formula \(3\)](#) (see [9.2](#)). This yields [Formulae \(B.2\)](#), [\(B.3\)](#) and [\(B.4\)](#):

$$C_{218\text{Po}} = \frac{1}{\varepsilon_c \cdot Q} \cdot \sum_{j=1}^n k_{218\text{Po},j} \cdot (I_j - I_{0,j}) \quad (\text{B.2})$$

$$C_{214\text{Pb}} = \frac{1}{\varepsilon_c \cdot Q} \cdot \sum_{j=1}^n k_{214\text{Pb},j} \cdot (I_j - I_{0,j}) \quad (\text{B.3})$$

$$C_{214\text{Bi}} = \frac{1}{\varepsilon_c \cdot Q} \cdot \sum_{j=1}^n k_{214\text{Bi},j} \cdot (I_j - I_{0,j}) \quad (\text{B.4})$$

The activity concentration of each radon decay product is also calculated, for a sampling duration t_s , as given by [Formulae \(B.5\)](#), [\(B.6\)](#) and [\(B.7\)](#):

$$C_{218\text{Po}} = \frac{\lambda_{218\text{Po}}^2}{1 - e^{-\lambda_{218\text{Po}} \cdot t_s}} \cdot \frac{N_{218\text{Po}}}{Q} \quad (\text{B.5})$$

$$C_{214\text{Pb}} = \frac{\lambda_{214\text{Pb}}^2}{1 - e^{-\lambda_{214\text{Pb}} \cdot t_s}} \cdot \frac{N_{214\text{Pb}}}{Q} - \left(\frac{\lambda_{214\text{Pb}} \cdot \lambda_{218\text{Po}}}{1 - e^{-\lambda_{218\text{Po}} \cdot t_s}} \right) \quad (\text{B.6})$$

$$\cdot \left(1 + \frac{\lambda_{214\text{Pb}}}{\lambda_{214\text{Pb}} - \lambda_{218\text{Po}}} \cdot \frac{e^{-\lambda_{214\text{Pb}} \cdot t_s} - e^{-\lambda_{218\text{Po}} \cdot t_s}}{1 - e^{-\lambda_{214\text{Pb}} \cdot t_s}} \right) \cdot \frac{N_{218\text{Po}}}{Q}$$

$$C_{214\text{Bi}} = \frac{\lambda_{214\text{Bi}}^2}{1 - e^{-\lambda_{214\text{Bi}} \cdot t_s}} \cdot \frac{N_{214\text{Bi}}}{Q} - \left(\frac{\lambda_{214\text{Bi}} \cdot \lambda_{214\text{Pb}}}{1 - e^{-\lambda_{214\text{Pb}} \cdot t_s}} \right) \cdot \left(1 + \frac{\lambda_{214\text{Bi}}}{\lambda_{214\text{Bi}} - \lambda_{214\text{Pb}}} \cdot \frac{e^{-\lambda_{214\text{Bi}} \cdot t_s} - e^{-\lambda_{214\text{Pb}} \cdot t_s}}{1 - e^{-\lambda_{214\text{Bi}} \cdot t_s}} \right)$$

$$\cdot \frac{N_{214\text{Pb}}}{Q} - \left[\frac{\lambda_{214\text{Bi}} \cdot \lambda_{214\text{Pb}} \cdot \lambda_{218\text{Po}}}{(\lambda_{218\text{Po}} - \lambda_{214\text{Pb}}) \cdot (1 - e^{-\lambda_{218\text{Po}} \cdot t_s})} \right] \cdot \left[\frac{e^{-\lambda_{214\text{Pb}} \cdot t_s} - e^{-\lambda_{218\text{Po}} \cdot t_s}}{1 - e^{-\lambda_{214\text{Pb}} \cdot t_s}} + \frac{\lambda_{214\text{Bi}}}{\lambda_{218\text{Po}} - \lambda_{214\text{Bi}}} \cdot \frac{e^{-\lambda_{214\text{Bi}} \cdot t_s} - e^{-\lambda_{218\text{Po}} \cdot t_s}}{1 - e^{-\lambda_{214\text{Bi}} \cdot t_s}} \right] \cdot \frac{N_{218\text{Po}}}{Q} \\ + \frac{\lambda_{214\text{Bi}}}{\lambda_{214\text{Bi}} - \lambda_{214\text{Pb}}} \cdot \frac{e^{-\lambda_{214\text{Bi}} \cdot t_s} - e^{-\lambda_{214\text{Pb}} \cdot t_s}}{1 - e^{-\lambda_{214\text{Bi}} \cdot t_s}} \cdot \left(1 + \frac{e^{-\lambda_{214\text{Pb}} \cdot t_s} - e^{-\lambda_{218\text{Po}} \cdot t_s}}{1 - e^{-\lambda_{214\text{Pb}} \cdot t_s}} \right) \cdot \frac{N_{218\text{Po}}}{Q} \quad (\text{B.7})$$

B.2.3 Determination of the coefficients $k_{218\text{Po},j}$, $k_{214\text{Pb},j}$ and $k_{214\text{Bi},j}$

Using [Formulae \(B.2\)](#) to [\(B.7\)](#), along with the determination of $N_{218\text{Po}}$, $N_{214\text{Pb}}$ and $N_{214\text{Bi}}$, the values of $k_{218\text{Po},j}$, $k_{214\text{Pb},j}$ and $k_{214\text{Bi},j}$ can be obtained for each measurement method.

B.3 Application to the Thomas protocol

B.3.1 Measurement procedure

For the Thomas protocol^[10], the sampling takes place over exactly $t_s = 300$ s, to the second.

After the sampling phase, the number of alpha disintegrations of the collected decay products is measured.

The steps are as follows:

- determine the background number of counts. Before performing the sampling, the virgin membrane is measured by means of three gross alpha countings with counting durations $t_{c1} - t_1 = 180$ s, $t_{c2} - t_2 = 840$ s, $t_{c3} - t_3 = 540$ s. The non-contamination of the detector when fitted with a virgin membrane is checked by a counting of at least 1 min prior to each measurement;
- carry out sampling;

- c) position the filtering membrane opposite the detector after the sampling process has been halted;
- d) perform three gross alpha countings of the membrane with specific durations according to the Thomas protocol:

- 1) $t = 0$ s to $t_1 = 120$ s standby, there is no count;
- 2) $t_1 = 120$ s to $t_{c1} = 300$ s count I_1 is performed;
- 3) $t_{c1} = 300$ s to $t_2 = 360$ s standby, there is no count;
- 4) $t_2 = 360$ s to $t_{c2} = 1\,200$ s count I_2 is performed;
- 5) $t_{c2} = 1\,200$ s to $t_3 = 1\,260$ s standby, there is no count;
- 6) $t_3 = 1\,260$ s to $t_{c3} = 1\,800$ s count I_3 is performed.

B.3.2 Determination of the coefficients $k_{218\text{Po},j}$, $k_{214\text{Pb},j}$ and $k_{214\text{Bi},j}$

If the sampling duration is known, the activity concentration of each radon decay product can be obtained from [Formulae \(B.5\)](#), [\(B.6\)](#) and [\(B.7\)](#). This yields [Formulae \(B.8\)](#), [\(B.9\)](#) and [\(B.10\)](#):

$$C_{218\text{Po}} = 2,112\,91 \times 10^{-5} \cdot \frac{N_{218\text{Po}}}{Q} \quad (\text{B.8})$$

$$C_{214\text{Pb}} = 1,531\,78 \times 10^{-6} \cdot \frac{N_{214\text{Pb}}}{Q} - 9,849\,24 \times 10^{-7} \cdot \frac{N_{218\text{Po}}}{Q} \quad (\text{B.9})$$

$$C_{214\text{Bi}} = 2,131\,71 \times 10^{-6} \cdot \frac{N_{214\text{Bi}}}{Q} - 1,328\,16 \times 10^{-7} \cdot \frac{N_{214\text{Pb}}}{Q} + 2,327\,55 \times 10^{-8} \cdot \frac{N_{218\text{Po}}}{Q} \quad (\text{B.10})$$

From all times (start and end counting times) selected in the counting protocol and using [Formula \(B.1\)](#), the counting results can be expressed as given by [Formulae \(B.11\)](#), [\(B.12\)](#) and [\(B.13\)](#):

$$I_1 - I_{0,1} = \varepsilon_c \cdot (0,316\,57 \cdot N_{218\text{Po}} + 0,085\,3 \cdot N_{214\text{Pb}} + 0,093\,37 \cdot N_{214\text{Bi}}) \quad (\text{B.11})$$

$$I_2 - I_{0,2} = \varepsilon_c \cdot (0,324\,93 \cdot N_{218\text{Po}} + 0,108\,01 \cdot N_{214\text{Pb}} + 0,314\,93 \cdot N_{214\text{Bi}}) \quad (\text{B.12})$$

$$I_3 - I_{0,3} = \varepsilon_c \cdot (0,095\,77 \cdot N_{218\text{Po}} + 0,095\,65 \cdot N_{214\text{Pb}} + 0,129\,65 \cdot N_{214\text{Bi}}) \quad (\text{B.13})$$

From these counting results, the number of atoms of the radon decay products collected on the filter at the end of sampling ($N_{218\text{Po}}$, $N_{214\text{Pb}}$ and $N_{214\text{Bi}}$) can be deduced using, for example, the Cramer's rule:

$$N_{218\text{Po}} = \frac{1}{\varepsilon_c} \cdot [4,930\,77 \cdot (I_1 - I_{0,1}) - 2,393\,32 \cdot (I_2 - I_{0,2}) + 2,262\,79 \cdot (I_3 - I_{0,3})] \quad (\text{B.14})$$

$$N_{214\text{Pb}} = \frac{1}{\varepsilon_c} \cdot [4,930\,77 \cdot (I_1 - I_{0,1}) - 2,393\,32 \cdot (I_2 - I_{0,2}) + 2,262\,79 \cdot (I_3 - I_{0,3})] \quad (\text{B.15})$$