
**Plain bearings — Hydrostatic plain
journal bearings with drainage
grooves under steady-state
conditions —**

**Part 1:
Calculation of oil-lubricated plain
journal bearings with drainage
grooves**

*Paliers lisses — Paliers lisses radiaux hydrostatiques avec rainures
d'écoulement fonctionnant en régime stationnaire —*

*Partie 1: Calcul pour la lubrification des paliers lisses radiaux avec
rainures d'écoulement*



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ISO copyright office
CP 401 • Ch. de Blandonnet 8
CH-1214 Vernier, Geneva
Phone: +41 22 749 01 11
Email: copyright@iso.org
Website: www.iso.org

Published in Switzerland

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Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

The procedures used to develop this document and those intended for its further maintenance are described in the ISO/IEC Directives, Part 1. In particular, the different approval criteria needed for the different types of ISO document should be noted. This document was drafted in accordance with the editorial rules of the ISO/IEC Directives, Part 2 (see www.iso.org/directives).

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For an explanation of the voluntary nature of standards, the meaning of ISO specific terms and expressions related to conformity assessment, as well as information about ISO's adherence to the World Trade Organization (WTO) principles in the Technical Barriers to Trade (TBT), see www.iso.org/iso/foreword.html.

The committee responsible for this document is ISO/TC 123, *Plain bearings*, Subcommittee SC 8, *Calculation methods for plain bearings and their applications*.

This third edition cancels and replaces the second edition (ISO 12167-1:2016), which has been technically revised.

The main changes are as follows:

- subclause titles have been added;
- symbols have been corrected and added in [Table 1](#);
- calculation values in [Annex B](#) have been corrected;
- adjustments have been made according to ISO/IEC Directives, Part 2:2021;
- typographical errors have been corrected.

A list of all parts in the ISO 12167 series can be found on the ISO website.

Any feedback or questions on this document should be directed to the user's national standards body. A complete listing of these bodies can be found at www.iso.org/members.html.

Introduction

Hydrostatic bearings use external lubrication to support pressure on the bearings; thus, they are less prone to wear and tear, run quietly, and have a wide useable speed, as well as high stiffness and damping capacity. These properties also demonstrate the special importance of plain journal bearings in different fields of application such as in machine tools.

Basic calculations described in this document may be applied to bearings with different numbers of recesses and different width/diameter ratios for identical recess geometry.

Oil is fed to each bearing recess by means of a common pump with a constant pumping pressure (system $p_{\text{en}} = \text{constant}$) and through preceding linear restrictors, e.g. capillaries.

In this document, only bearings with oil drainage grooves between the recesses are taken into account. As compared to bearings without oil drainage grooves, this type needs higher power with the same stiffness behaviour.

Equivalent calculation procedures that enable operating conditions to be estimated and checked against acceptable conditions may also be used.

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Plain bearings — Hydrostatic plain journal bearings with drainage grooves under steady-state conditions —

Part 1: Calculation of oil-lubricated plain journal bearings with drainage grooves

1 Scope

This document specifies the calculation procedures to calculate and assess a given bearing design, as well as to design a bearing as a function of some optional parameters. This document contains the design of the required lubrication system including the calculation of the restrictor data.

This document applies to hydrostatic plain journal bearings under steady-state conditions.

2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 12167-2:2021, *Plain bearings — Hydrostatic plain journal bearings with drainage grooves under steady-state conditions — Part 2: Characteristic values for the calculation of oil-lubricated plain journal bearings with drainage grooves*

3 Terms and definitions

No terms and definitions are listed in this document.

ISO and IEC maintain terminology databases for use in standardization at the following addresses:

- ISO Online browsing platform: available at <https://www.iso.org/obp>
- IEC Electropedia: available at <https://www.electropedia.org/>

4 Symbols

Symbols and units are defined in [Table 1](#).

Table 1 — Symbols

Symbol	Term	Unit
a	Inertia factor	1
A_{lan}	Land area	m ²
A_{lan}^*	Relative land area	1
A_p	Recess area	m ²
b	Width perpendicular to the direction of flow	m

Table 1 (continued)

Symbol	Term	Unit
b_{ax}	Width of axial outlet $\left[b_{ax} = \frac{\pi \times D}{Z} - (l_c + b_G) \right]$	m
b_c	Width of circumferential outlet ($b_c = B - l_{ax}$)	m
b_G	Width of drainage groove	m
B	Bearing width	m
c	Stiffness coefficient	N/m
c_p	Specific heat capacity of the lubricant (p is a constant)	J/kg·K
C_R	Radial clearance	m
d_{cp}	Diameter of capillaries	m
D	Bearing diameter (D_J : shaft; D_B : bearing; $D \approx D_J \approx D_B$)	m
e	Eccentricity (shaft displacement)	m
f	Relative film thickness [$f = h/C_R$]	1
$f_{en,i}$	Relative film thickness at $\varphi = \varphi'_{1,i}$	1
$f_{ex,i}$	Relative film thickness at $\varphi = \varphi'_{2,i}$	1
F	Load-carrying capacity (load)	N
F_i	Radial force in recess i	N
F_h	Horizontal component of the resultant force of recesses	N
F_v	Vertical component of the resultant force of recesses	N
F^*	Characteristic value of load-carrying capacity	1
F_{eff}^*	Characteristic value of effective load-carrying capacity	1
$F_{eff,0}^*$	Characteristic value of effective load-carrying capacity for $N = 0$	1
h	Local lubricant film thickness (clearance gap height)	m
h_{en}	Oil film thickness at entrance edge of recess	m
h_{ex}	Oil film thickness at exit edge of recess	m
h_{min}	Minimum lubricant film thickness (minimum clearance gap height)	m
h_p	Depth of recess	m
i (index)	Consecutive number	1
k	Exponent	1
K_{rot}	Speed-dependent parameter	1
$K_{rot,nom}$	Normalized speed-dependent parameter	1
l	Length in the direction of flow	m
l_{ax}	Axial land length	m
l_c	Circumferential land length	m
l_{cp}	Length of capillaries	m
N	Rotational frequency (speed)	s ⁻¹
opt (index)	optimum	1
p	Recess pressure, general	Pa
$\bar{p}$	Specific bearing load [$\bar{p} = F/(B \times D)$]	Pa
p_{en}	Feed pressure (pumping pressure)	Pa
p_i	Pressure in recess i	Pa
p_i^*	Pressure ratio in recess i	1
$p_{i,0}$	Pressure in recess i , when $\varepsilon = 0$	Pa

Table 1 (continued)

Symbol	Term	Unit
$p_{\max}$	Maximum pressure in recess	Pa
$p_{\min}$	Minimum pressure in recess	Pa
P^*	Power ratio	1
P_f	Frictional power	W
$P_{f,\text{lan}}$	Frictional power in land area	W
$P_{f,p}$	Frictional power in recess area	W
P_f^*	Characteristic value for the frictional power	1
$P_{f,\text{lan}}^*$	Characteristic value for the frictional power in land area	1
$P_{f,p}^*$	Characteristic value for the frictional power in recess area	1
P_p	Pumping power	W
P_{tot}	Total power	W
P_{tot}^*	Characteristic value of total power	1
Q	Lubricant flow rate (for complete bearing)	m ³ /s
Q^*	Lubricant flow rate parameter	1
Q_{ax}	Lubricant flow rate from recess in the axial direction	m ³ /s
$Q_{\text{cp}, i}$	Lubricant flow rate from capillary into recess i	m ³ /s
Q_{en}	Inlet lubricant flow rate into recess in the circumferential direction	m ³ /s
Q_{ex}	Outlet lubricant flow rate from recess in the circumferential direction	m ³ /s
R_{cp}	Flow resistance of capillaries	Pa·s/m ³
$R_{\text{lan}, \text{ax}}$	Flow resistance of one axial land $\left(R_{\text{lan}, \text{ax}} = \frac{12 \times \eta \times l_{\text{ax}}}{b_{\text{ax}} \times C_{\text{R}}^3} \right)$	Pa·s/m ³
$R_{\text{lan}, c}$	Flow resistance of one circumferential land $\left(R_{\text{lan}, c} = \frac{12 \times \eta \times l_c}{b_c \times C_{\text{R}}^3} \right)$	Pa·s/m ³
$R_{p, 0}$	Flow resistance of one recess, when $\varepsilon = 0$	Pa·s/m ³
Re	Reynolds number	1
Re_{cp}	Reynolds number in capillaries	1
Re_p	Reynolds number in recess	1
So	Sommerfeld number	1
T	Temperature	°C
T_B	Mean temperature in the bearings; see Formula (15)	°C
T_{cp}	Temperature in capillaries	°C
T_{en}	Inlet temperature	°C
u	Flow velocity	m/s
U	Circumferential speed	m/s
$\bar{w}$	Average velocity in restrictor	m/s
Z	Number of recesses	1
α	Position of first recess related to recess centre measured from load direction; see Figure A.3	rad
β	Attitude angle of shaft	°
γ	Exponent in viscosity formula	1
Δp_{lan}	Pressure difference in land area	Pa
ΔT	Temperature difference	K

Table 1 (continued)

Symbol	Term	Unit
ΔT_B	Mean temperature difference in the bearings	K
ΔT_{cp}	Temperature difference in capillaries	K
ε	Relative eccentricity	1
η	Dynamic viscosity	Pa·s
η_B	Dynamic viscosity for $T = T_B$	Pa·s
η_{cp}	Dynamic viscosity in capillaries	Pa·s
η_{40}	Dynamic viscosity at 40 °C	Pa·s
κ	Resistance ratio	1
ξ	Restrictor ratio	1
π_f	Relative frictional pressure	1
$\pi_{f,opt}$	Optimum relative frictional pressure	1
ρ	Density	kg/m ³
τ	Shearing stress	N/m ²
φ	Angular coordinate measured from radius opposite to eccentricity, e ; see Figure A.3	rad
φ_F	Angle of resultant force of recesses	rad
φ_G	Angle between the centre of land and the centre of drainage groove	rad
ψ	Relative bearing clearance	1
ψ_{opt}	Optimum relative bearing clearance	1
ω	Angular velocity ($\omega = 2 \times \pi \times N$)	s ⁻¹

5 Bases of calculation and boundary conditions

Calculation in accordance with this document is the mathematical determination of the operational parameters of hydrostatic plain journal bearings as a function of operating conditions, bearing geometry and lubrication data. This means the determination of eccentricities, load-carrying capacity, stiffness, required feed pressure, oil flow rate, frictional and pumping power, and temperature rise. Besides the hydrostatic pressure build up, the influence of hydrodynamic effects is also approximated.

Reynolds equation furnishes the theoretical basis for the calculation of hydrostatic bearings. In most practical cases of application, it is, however, possible to arrive at sufficiently exact results by approximation.

The approximation used in this document is based on two basic formulae intended to describe the flow through the bearing lands, which can be derived from Reynolds equation when special boundary conditions are observed. The Hagen-Poiseuille law describes the pressure flow in a parallel clearance gap and the Couette formula the drag flow in the bearing clearance gap caused by shaft rotation. A detailed presentation of the theoretical background of the calculation procedure is included in [Annex A](#). An example of the calculation procedure is given in [Annex B](#).

The following important premises are applicable to the calculation procedures described in this document:

- all lubricant flows in the lubrication clearance gap are laminar;
- the lubricant adheres completely to the sliding surfaces;
- the lubricant is an incompressible Newtonian fluid;
- in the whole lubrication clearance gap, as well as in the preceding restrictors, the lubricant is partially isoviscous;

- e) a lubrication clearance gap completely filled with lubricant is the basis of frictional behaviour;
- f) fluctuations of pressure in the lubricant film normal to the sliding surfaces do not take place;
- g) bearing and journal have completely rigid surfaces;
- h) the radii of curvature of the surfaces in relative motion to each other are large in comparison to the lubricant film thickness;
- i) the clearance gap height in the axial direction is constant (axial parallel clearance gap);
- j) the pressure over the recess area is constant;
- k) there is no motion normal to the sliding surfaces.

The bearing consists of Z cylindrical segments and rectangular recess of the same size and is supplied with oil through restrictors of the same flow characteristics. Each segment consists of a circumferential part between two centre lines of axial drainage grooves. With the aid of the above-mentioned approximation formulae, all parameters required for the design or calculation of bearings can be determined. The application of the similarity principle results in dimensionless similarity values for load-carrying capacity, stiffness, oil flow rate, friction, recess pressures, etc.

The results indicated in this document in the form of tables and diagrams are restricted to operating ranges common in practice for hydrostatic bearings. Thus, the range of the bearing eccentricity (displacement under load) is limited to $\varepsilon = 0$ to $0,5$.

Limitation to this eccentricity range means a considerable simplification of the calculation procedure as the load-carrying capacity is a nearly linear function of the eccentricity. However, the applicability of this procedure is hardly restricted as in practice eccentricities $\varepsilon > 0,5$ are mostly undesirable for reasons of operational safety. A further assumption for the calculations is the approximated optimum restrictor ratio^[2] $\xi = 1$ for the stiffness behaviour.

As for the outside dimensions of the bearing, this document is restricted to the range bearing width/bearing diameter $B/D = 0,3$ to 1 , which is common in practical cases of application. The recess depth is larger than the clearance gap height by a factor of 10 to 100 . When calculating the friction losses, the friction loss over the recess in relation to the friction over the bearing lands can generally be neglected on account of the above premises. However, this does not apply when the bearing shall be optimized with regard to its total power losses.

To take into account the load direction of a bearing, it is necessary to distinguish between the two extreme cases, load in the direction of recess centre and load in the direction of land centre.

Apart from the aforementioned boundary conditions, some other requirements are to be mentioned for the design of hydrostatic bearings in order to ensure their functioning under all operating conditions. In general, a bearing shall be designed in such a manner that a clearance gap height of at least 50% to 60% of the initial clearance gap height is ensured when the maximum possible load is applied. With this in mind, particular attention shall be paid to misalignments of the shaft in the bearing due to shaft deflection which may result in contact between shaft and bearing edge and thus in damage of the bearing. In addition, the parallel clearance gap required for the calculation is no longer present in such a case.

In the case where the shaft is in contact with the bearing lands when the hydrostatic pressure is switched off, it can be necessary to check the contact zones with regard to rising surface pressures.

It shall be ensured that the heat originating in the bearing does not lead to a non-permissible rise in the temperature of the oil.

If necessary, a means of cooling the oil shall be provided. Furthermore, the oil shall be filtered in order to avoid choking of the capillaries and damage to the sliding surfaces.

Low pressure in the relieved recess shall also be avoided, as this leads to air being drawn in from the environment and this would lead to a decrease in stiffness (see [6.7](#)).

6 Method of calculation

6.1 General

This document covers the calculation, as well as the design, of hydrostatic plain journal bearings. In this case, calculation is understood to be the verification of the operational parameters of a hydrostatic bearing with known geometrical and lubrication data. In the case of a design calculation, with the given methods of calculation, it is possible to determine the missing data for the required bearing geometry, the lubrication data and the operational parameters on the basis of a few initial data (e.g. required load-carrying capacity, stiffness, rotational frequency).

In both cases, the calculations are carried out according to an approximation method based on the Hagen-Poiseuille and the Couette formulae, mentioned in [Clause 5](#), see also [A.2.2](#) and [A.2.3](#). The bearing parameters calculated according to this method are given as relative values in the form of tables and diagrams as a function of different parameters. The procedure for the calculation or design of bearings is described in [6.2](#) to [6.7](#). This includes the determination of different bearing parameters with the aid of the given calculation formulae or the tables and diagrams. The following calculation items are explained in detail:

- a) determination of load-carrying capacity with and without taking into account shaft rotation;
- b) calculation of lubricant flow rate and pumping power;
- c) determination of frictional power with and without consideration of losses in the bearing recesses;
- d) procedure for bearing optimization with regard to minimum total power loss.

For all calculations, it is necessary to check whether the important premise of laminar flow in the bearing clearance gap, in the bearing recess and in the capillary is met. This is checked by determining the Reynolds numbers. Furthermore, the portion of the inertia factor in the pressure differences shall be kept low at the capillary (see [A.3.1](#)).

If the boundary conditions defined in [Clause 5](#) are observed, this method of calculation yields results with deviations which can be neglected for the requirements of practice, in comparison with an exact calculation by solving the Reynolds equation.

6.2 Load-carrying capacity

Unless indicated otherwise, it is assumed in the following that capillaries with a linear characteristic are used as restrictors and that the restrictor ratio is $\xi = 1$. Furthermore, the difference is only made between the two cases, "load in direction of recess centre" and "load in direction of land centre". For this reason, it is no longer mentioned in each individual case that the characteristic values are a function of the three parameters, "restrictor type", "restrictor ratio" and "load direction relative to the bearing".

Even under the abovementioned premises, the characteristic value of load carrying capacity [[Formula \(1\)](#)]

$$F^* = \frac{F}{B \times D \times p_{\text{en}}} = \frac{\bar{p}}{p_{\text{en}}} \quad (1)$$

still depends on the following parameters:

- number of recesses, Z ;
- width/diameter ratio, B/D ;
- relative axial land width, l_{ax}/B ;
- relative land width in circumferential direction, l_c/D ;
- relative groove width, b_G/D ;

- relative journal eccentricity, ε ;
- relative frictional pressure when the difference is only made between the two cases, “load on recess centre” and “load on land centre”:

$$\pi_f = \frac{\eta_B \times \omega}{p_{en} \times \psi^2} \quad (2)$$

NOTE The Sommerfeld number, So , common with hydrodynamic plain journal bearings can be set up as follows:

$$So = \frac{\bar{p} \times \psi^2}{\eta_B \times \omega} = \frac{F^*}{\pi_f}$$

In ISO 12167-2:2021, Figures 1 and 2, the functions $F^*(\varepsilon, \pi_f)$ and $\beta(\varepsilon, \pi_f)$ are represented for $Z = 4$, $\xi = 1$, $B/D = 1$, $l_{ax}/B = 0,1$, $l_c/D = 0,1$, $b_G/D = 0,05$, i.e. restriction by means of capillaries, load in direction of centre of bearing recess.

ISO 12167-2:2021, Figures 1 and 2 show the influence of rotation on the characteristic value of load-carrying capacity and the attitude angle.

For the calculation of a geometrically similar bearing, it is possible to determine the minimum lubricant film thickness when values are given, e.g. for F , B , D , p_{en} , ω , ψ , and η_B (determination of η_B according to 6.6, if applicable).

All parameters are given for the determination of F^* according to Formula (1) and π_f according to Formula (2). For this geometry, the relevant values for ε and β can be taken from ISO 12167-2:2021, Figures 1 and 2 and thus, $h_{min} = C_R(1 - \varepsilon)$.

According to the approximation method described in Annex A, it transpires that the characteristic value of effective load-carrying capacity is no longer a function of the ratio B/D .

$$F_{eff}^* = \frac{F}{b_c \times Z \times b_{ax} \times p_{en}} = \frac{F^*}{\frac{b_c}{D} \times \frac{Z \times b_{ax}}{B}} \quad (3)$$

If the resistance ratio

$$k = \frac{R_{lan, ax}}{R_{lan, c}} = \frac{l_{ax} \times b_c}{l_c \times b_{ax}} \quad (4)$$

and the speed dependent parameter

$$K_{rot} = \frac{\xi \times k \times \pi_f \times l_c}{D}$$

$$K_{rot, nom} = \frac{K_{rot}}{1 + k} \quad (5)$$

are introduced, there remains a dependence on the following parameters:

$$F_{eff}^*(Z, \varphi_G, k, K_{rot}, \varepsilon)$$

If, in addition, advantage is taken of the fact that the function $F_{eff}^*(\varepsilon)$ is nearly linear for $\varepsilon \leq 0,5$, then it is practically sufficient to know that the function $F_{eff}^*(\varepsilon = 0,4) = f(Z, \varphi_G, k, K_{rot})$ for the calculation of the load carrying capacity.

For $K_{\text{rot}} = 0$, i.e. for the stationary shaft, the characteristic value of effective load-carrying capacity for $\varepsilon = 0,4$ only depends on three parameters:

$$F_{\text{eff}}^* (\varepsilon = 0,4) = f(Z, \varphi_G, k)$$

Thus, in ISO 12167-2:2021, Figure 3, $F_{\text{eff},0}^* (\varepsilon = 0,4)$ for $Z = 4$ and 6 can be given via κ for different φ_G values.

The influence of the rotational movement on the characteristic value of load-carrying capacity is taken into account by the ratio $\frac{F_{\text{eff}}^*}{F_{\text{eff},0}^*} = f(Z, \varphi_G, k, K_{\text{rot}})$.

For $Z = 4$, the ratio $F_{\text{eff}}^* / F_{\text{eff},0}^*$ is shown in ISO 12167-2:2021, Figure 4. The hydrodynamically conditioned increase of the load-carrying capacity can be easily recognized when presented in such a manner.

If, for example, Z and all parameters are given for the determination of F_{eff}^* according to [Formula \(3\)](#), κ according to [Formula \(4\)](#) and K_{rot} according to [Formula \(5\)](#), then the minimum lubricant film thickness developing during operation can be determined.

After having calculated φ_G , κ and $K_{\text{rot, nom}}$, the value for $F_{\text{eff},0}^* (\varepsilon = 0,4)$ is taken from ISO 12167-2:2021, Figure 3 and the value for $F_{\text{eff}}^* / F_{\text{eff},0}^* (\varepsilon = 0,4)$ from ISO 12167-2:2021, Figure 4, F_{eff}^* is calculated according to [Formula \(3\)](#) and then the relative eccentricity is obtained as follows:

$$\varepsilon = \frac{0,4 \times F_{\text{eff}}^*}{\frac{F_{\text{eff}}^*}{F_{\text{eff},0}^*} (\varepsilon = 0,4) \times F_{\text{eff},0}^* (\varepsilon = 0,4)}$$

and the minimum lubricant film thickness is $h_{\text{min}} = C_R \times (1 - \varepsilon)$.

6.3 Lubricant flow rate and pumping power

The characteristic value for the lubricant flow rate is given by

$$Q^* = \frac{Q \times \eta_B}{C_R^3 \times p_{\text{en}}} \quad (6)$$

It depends only slightly on the relative journal eccentricity ε , the load direction relative to the bearing and the relative frictional pressure π_f , or the speed dependent parameter K_{rot} .

By approximation, the lubricant flow rate can be calculated as follows (see also [A.3.4](#)):

$$Q^* (\varepsilon \leq 0,5) \approx Q^* (\varepsilon = 0) = \frac{Z}{6(1+\xi)} \times \frac{B}{D} \times \frac{1 - \frac{l_{\text{ax}}}{B}}{\frac{l_c}{D}} \times \frac{k+1}{k} \quad (7)$$

$$\frac{1}{1+\xi} = \frac{P_p}{p_{en}} (\varepsilon=0) \text{ with } \xi = \frac{R_{cp}}{R_{p,0}} \text{ and } R_{p,0} = \frac{6 \times \eta_B \times l_{ax}}{b_{ax} \times C_R^3 (1+k)}$$

The flow resistance of the capillaries according to [A.3.2.2](#) is given by

$$R_{cp} = \frac{128 \times \eta_{cp} \times l_{cp}}{\pi \times d_{cp}^4} \times (1+a)$$

with the non-linear portion (inertia factor)

$$a = \frac{1,08}{32} \times \frac{4 \times Q \times \rho}{\eta_{cp} \times l_{cp} \times \pi \times Z}$$

By converting [Formula \(6\)](#), the lubricant flow rate can be calculated when the parameters η_B , C_R , p_{en} , ξ , B/D , and l_{ax}/B are given.

For optimized bearings, Q^* shall be taken from ISO 12167-2:2021, Table 1. The pumping power, without considering the pump efficiency, is given by

$$P_p = Q \times p_{en} = Q^* \times \frac{p_{en}^2 \times C_R^3}{\eta_B} \quad (8)$$

According to the approximation method, Q^* is again determined according to [Formula \(7\)](#), thus it is the characteristic value of both flow rate and pumping power.

6.4 Frictional power

The characteristic value for the frictional power is given by

$$P_f^* = \frac{P_f \times C_R}{\eta_B \times U^2 \times B \times D} \quad (9)$$

Friction generates in the lands as well as in the recess area. The land area related to the total surface of the bearing $\pi \times B \times D$ is given by

$$A_{lan}^* = \frac{A_{lan}}{\pi \times B \times D} = \frac{2}{\pi} \times \left[\frac{l_{ax}}{B} \times \pi + Z \times \frac{l_c}{D} \times \left(1 - 2 \times \frac{l_{ax}}{B} \right) - Z \times \frac{l_{ax}}{B} \times \frac{b_G}{D} \right]$$

According to the approximation method, the characteristic value for the frictional power in the land area is given by

$$P_{f,lan}^* = \frac{\pi}{\sqrt{1-\varepsilon^2}} \times A_{lan}^*$$

and in the recess area

$$P_{f,p}^* = \pi \times 4 \times \frac{C_R}{h_p} \times (1 - A_{lan}^*)$$

Thus, the characteristic value for the total amount of friction is given by

$$P_f^* = \pi \times A_{lan}^* \times \left[\frac{1}{\sqrt{1-\varepsilon^2}} + \frac{4 \times C_R}{h_p} \times \left(\frac{1}{A_{lan}^*} - 1 \right) \right] \quad (10)$$

The actual frictional power is obtained by converting [Formula \(9\)](#):

$$P_f = P_f^* \times \frac{\eta_B \times U^2 \times B \times D}{C_R}$$

6.5 Optimization

When optimizing according to the power consumption, the total power loss, i.e. the sum of pumping and frictional power, is minimized. According to 6.3 and 6.4, the total power is given by

$$P_{\text{tot}} = P_p + P_f = Q^* \times \frac{p_{\text{en}}^2 \times C_R^3}{\eta_B} + P_f^* \times \frac{\eta_B \times U^2 \times B \times D}{C_R}$$

With Formulae (8) and (9), this can be written as follows:

$$P_{\text{tot}} = F \times \omega \times C_R \times \frac{Q^*}{4 \times \frac{B}{D} \times F^* \times \pi_f} \times \left(1 + \frac{P_f}{P_p} \right) \quad (11)$$

Following a proposal of Vermeulen,^[3] the ratio of frictional power to pumping power is introduced as an optional parameter and designated with P^* . Thus, the characteristic value for the total power loss is given by

$$P_{\text{tot}}^* = \frac{P_{\text{tot}}}{F \times \omega \times C_R} = \frac{Q^* \times (1 + P^*)}{4 \times \frac{B}{D} \times F^* \times \pi_f} \quad (12)$$

Serial calculations have shown that the power minimum which can be obtained in the relatively wide range, $P^* = 1$ to 3, depends only slightly on the chosen power ratio, P^* . An approximated optimization with the mean value $P^* = 2$ may be carried out.

The relative frictional pressure in Formula (12) cannot be chosen freely, as it is linked to the chosen power ratio, P^* :

$$P^* = \frac{P_f}{P_p} = \pi_f^2 \times 4 \times \frac{B}{D} \times \frac{P_f^*}{Q^*} \quad \text{or} \quad \pi_f = \frac{1}{2} \times \sqrt{\frac{P^* \times Q^*}{P_f^* \times \frac{B}{D}}} \quad (13)$$

When P^* , B/D , ε , η_B/C_R and ξ are given, the characteristic value of total power according to Formula (12) to be minimized remains only a function of Z , l_{ax}/B , l_c/D and b_G/D .

In ISO 12167-2:2021, Figures 5 to 12, P_{tot}^* for $P^* = 2$, $b_G/D = 0,05$, $\xi = 1$, $\varepsilon = 0,4$ is presented for different B/D and Z as a function of l_{ax}/B , l_c/D and l_c/B respectively, taking into account the friction in the recesses. The land widths, l_{ax}/B and l_c/B [$l_c/D = (l_c/B) \times (B/D)$], where the total power is reduced to a minimum, result from these figures.

The optimum land widths and the associated values for $B/D = 1$ to 0,3, as well as the numbers of recesses $Z = 4$ to 10 obtained by this, are given in ISO 12167-2:2021, Table 1.

With decreasing width, P_{tot}^* and thus, the total need of power increases. For high rotational frequencies and a given diameter, it may, however, be advantageous to use a plain bearing with smaller bearing width.

In the case where the shaft is at a standstill or rotating very slowly, the optimization method with $P^* = 1$ to 3 can no longer be applied; see Reference [3]. In this case, the pumping power has to be minimized and thus, relatively wide lands are obtained. Therefore, the approximation method also fails and the Reynolds equation has to be solved by means of a finite method.

For a bearing with $Z = 4$, $B/D = 1$ the following land widths are recommended as being optimal $l_{\text{ax}}/B = l_c/B = 0,25$.

For $\varepsilon = 0,4$, the following values can be used for the calculation, $F^* = 0,174$ and $Q^* = 1,48$.

6.6 Temperatures and viscosities

With $\varepsilon = 0$, heating in the capillaries due to dissipation is calculated as follows (heat exchange between lubricant and environment is not considered here):

$$\Delta T_{cp} = \frac{p_{en} - p}{c_p \times \rho} = \frac{p_{en}}{c_p \times \rho} \times \frac{\xi}{1 + \xi}$$

and heating in the bearing, again with $\varepsilon = 0$, as follows:

$$\Delta T_B = \frac{p}{c_p \times \rho} + \frac{P_f}{c_p \times \rho \times Q} = \frac{p_{en}}{c_p \times \rho} \times \left(\frac{1}{1 + \xi} + P^* \right)$$

Thus the mean temperature in the capillaries is given by

$$T_{cp} = T_{en} + \frac{1}{2} \times \Delta T_{cp} \quad (14)$$

and the mean temperature in the bearing

$$T_B = T_{en} + \Delta T_{cp} + \frac{1}{2} \times \Delta T_B \quad (15)$$

It is assumed for the effective viscosities in the capillaries and bearing that $\eta_{cp} = \eta(T_{cp})$ and $\eta_B = \eta(T_B)$.

If the dependence of the viscosity on temperature is not completely known, the viscosities, η_{cp} and η_B , can be approximated, following the statement of Reynolds. A precondition is that two viscosities, η_1 and η_2 , are known at two temperatures, T_1 and T_2 , which should be close to the estimated temperatures, T_{cp} and T_B .

$$\eta_{cp} = \eta_1 \times \exp[-\gamma \times (T_{cp} - T_1)]; \quad \eta_B = \eta_1 \times \exp[-\gamma \times (T_B - T_1)] \quad (16)$$

with $\gamma = \frac{1}{T_2 - T_1} \times \ln \frac{\eta_1}{\eta_2}$

If only the viscosity class in accordance with ISO 3448 is known, then the course of viscosity for common lubrication oils having a viscosity index of about 100 can be calculated only on the basis of the nominal viscosity, η_{40} (dynamic viscosity at 40 °C):

$$\eta(T) = \eta_{40} \times \exp \left[160 \times \ln \left(\frac{\eta_{40}}{0,18 \times 10^{-3}} \right) \times \left(\frac{1}{T + 95} - \frac{1}{135} \right) \right] \quad (17)$$

The dynamic viscosity, η_{40} , is obtained by multiplying the kinematic viscosity, η_{40} , based on the viscosity classes, by the density, ρ . If this value is not exactly known, it can be calculated by approximation with $\rho = 900 \text{ kg/m}^3$.

[Formula \(17\)](#) is based on the statement of Vogel and empirically determined constants of Cameron and Rost and was transposed by Rodermund^[4] to the nominal viscosity at 40 °C.

6.7 Minimum pressure in recesses

With high rotational frequencies and high K_{rot} values according to [Formula \(5\)](#), the pressure in the recess, p_{min} , on the no-load side of the plain bearing may decrease to zero. Whereas, the recess

pressure, $p_{\max}$, on the load side may become greater than p_{en} . The minimum recess pressure, as well as F^* , depends on several variables. For the ratio applies

$$\frac{p_{\min}}{p_{\text{en}}}(Z, \varphi_G, k, K_{\text{rot}})$$

In ISO 12167-2:2021, Figure 13, the minimum relative recess pressure over $K_{\text{rot, nom}}$ is shown for $Z = 4$, $\varepsilon = 0,4$, $\kappa = 1$ to 2 and two φ_G values.

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Annex A (informative)

Description of the approximation method for the calculation of hydrostatic plain journal bearings

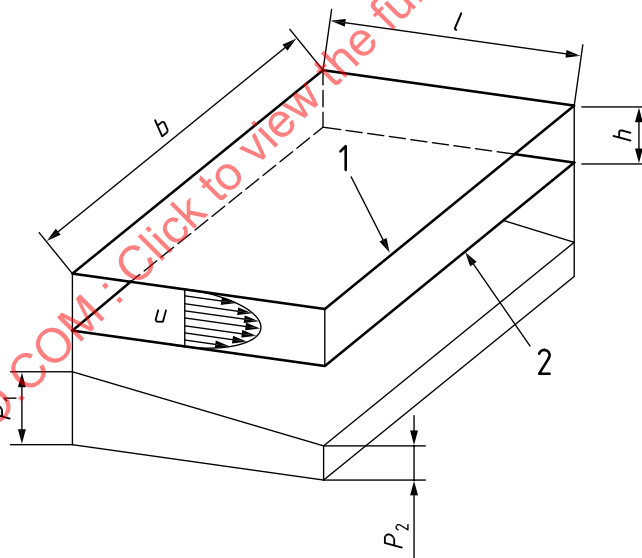
A.1 General

The calculation is based on an approximation method leading to an almost exact result, especially in cases where small lands are provided (e.g. shaft rotating at high speed). In the case of wider lands, the Reynolds equation shall be solved by means of differential formulae.

A.2 Fundamentals

A.2.1 General

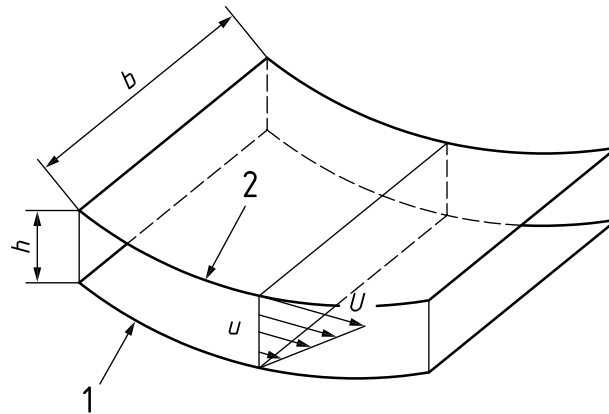
The approximation method assumes laminar flow, free of inertia, and uses two basic formulae for the flows via the lands (see [Figures A.1](#) and [A.2](#)).



Key

- 1 bearing
- 2 shaft

Figure A.1 — Pressure flow between parallel plates



Key

- 1 bearing
- 2 shaft

Figure A.2 — Drag flow due to shaft rotation

A.2.2 Hagen-Poiseuille formula

Pressure flow between parallel plates: ($b \gg h$)

$$Q = \frac{(p_2 - p_1) \times b \times h^3}{12 \times \eta \times l}$$

A.2.3 Couette formula

Drag flow due to shaft rotation:

$$Q = b \times \frac{U \times h}{2}$$

A.2.4 Further assumptions

- a) The pressure is constant over the recess area.
- b) The viscosity in the bearing and in the restrictors is constant.
- c) Shaft and bearing are rigid, their axes always parallel.
- d) For the calculation of the lubricant flow rates, it is assumed that the outlet width extends up to the centre of the adjacent lands and that the pressure drop over the outlet length is linear.
- e) For the calculation of the load effects, it is assumed that the pressure in the recesses spreads up to the centre of the adjacent lands.

A.3 Calculations

A.3.1 General

At first, the pressures in the recesses are calculated with the aid of the continuity formula for a certain shaft position, defined by ε, β where $\varepsilon = e/C_R$.

All other parameters are derived from the pressures in the recesses.

The calculation is iterative as the attitude angle β is not known in the beginning. This angle is to be varied until the result of the pressures in the recesses and the load has the same direction (see [Figure A.3](#)).

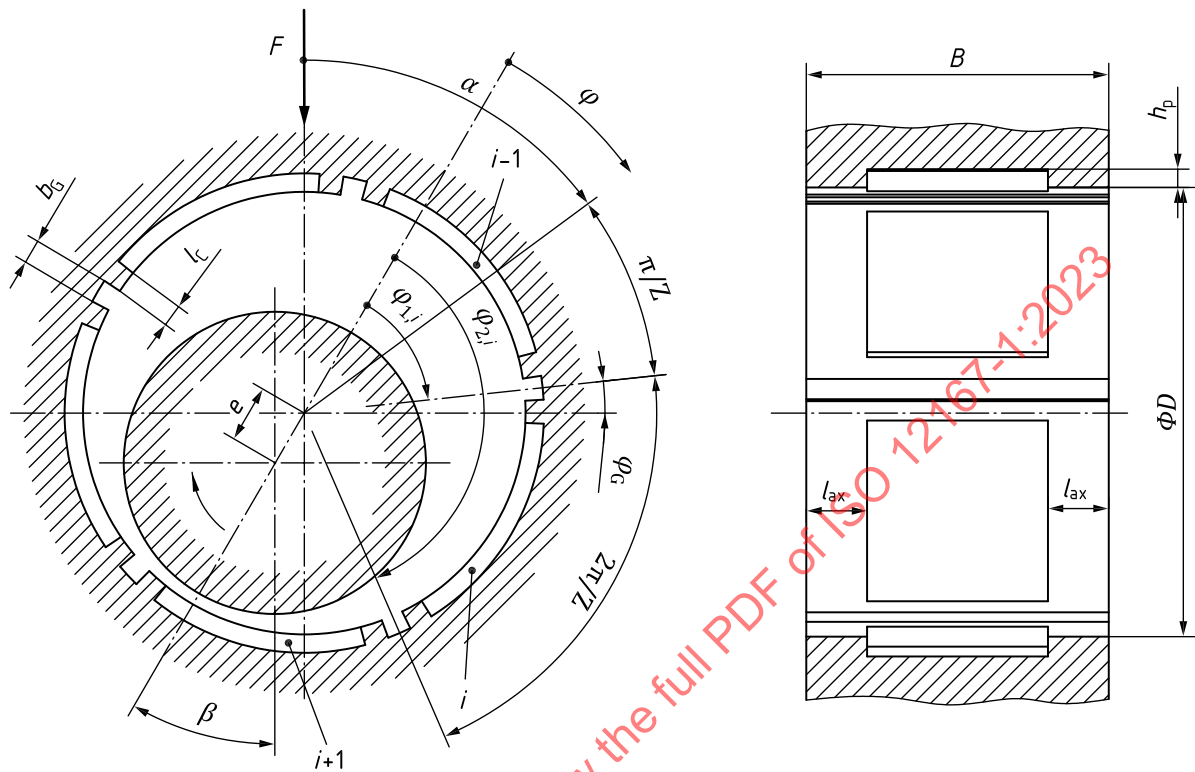


Figure A.3 — Bearing geometry

In principle, a vertical load is assumed for the calculation. However, this is no restriction as it can be assumed that the bearing is to be mounted appropriately for other directions of load.

The segment, i ($i = 1, 2, \dots, Z$), starts at the angle $\varphi_{1,i}$ (centre of drainage groove) and ends at the angle $\varphi_{2,i}$ (centre of next drainage groove), as shown in [Figure A.3](#). Angles φ , $\varphi_{1,i}$, and $\varphi_{2,i}$ are measured from radius opposite to eccentricity, e , as shown in [Figure A.3](#).

The centre of the first recess is situated at α . The initial angle and the end angle are

$$\varphi_{1,i} = \alpha - \beta + \frac{2 \times \pi}{Z} \times \left(i - \frac{3}{2} \right)$$

$$\varphi_{2,i} = \alpha - \beta + \frac{2 \times \pi}{Z} \times \left(i - \frac{1}{2} \right)$$

The film thickness, h , changes in the land area according to $h = C_R(1 + \varepsilon \times \cos \varphi)$.

A.3.2 Pressures in the recesses

A.3.2.1 General

The continuity principle is used for each recess. The separate recesses are decoupled by axial grooves so that the determination of pressure in the recesses does not depend on the pressure of the adjacent recesses. The grooves themselves are pressureless.

A.3.2.2 Lubricant flow rate via preresistance

The lubricant flow rate via preresistance ($\varepsilon = 0$) is given by

$$\frac{Q}{Z} = \frac{(p_{en} - p)^k}{R_{cp}}$$

where $k = 1$ corresponds to a linear resistance law.

Example of capillary with laminar flow:

$$Re_{cp} = \frac{\bar{w} \times d_{cp} \times \rho}{\eta_{cp}} < 2\,300$$

and with negligible portion of the term of inertia $\frac{\rho}{2} \times \bar{w}^2$.

$k = \frac{1}{2}$ corresponds to a square-law dependency, for example, of an orifice, the flow coefficient of which can be regarded as independent of the Reynolds number.

When dimensioning a capillary, the portion of the term of inertia shall be kept low and, if applicable, be taken into account. According to the theory of Schiller given in Reference [5], the pressure drop necessary to generate the velocity, $\bar{w} = \frac{4 \times Q}{Z \times \pi \times d_{cp}^2}$, at a properly rounded inlet (rounding off radius

$> 0,3 \times d_{cp}$), is $\Delta p_{en} = 2,16 \times \frac{\rho}{2} \times \bar{w}^2$.

The flow resistance of the capillaries is then

$$R_{cp} = \frac{p_{en} - p_i}{\frac{Q}{Z}} = \frac{\Delta p_{lan}}{\frac{Q}{Z}} + \frac{\Delta p_{en}}{\frac{Q}{Z}} = \frac{128 \times \eta_{cp} \times l_{cp}}{\pi \times d_{cp}^4} + \frac{2,16 \times \frac{\rho}{2} \times \bar{w}^2}{\bar{w} \times \frac{\pi}{4} \times d_{cp}^2}$$

$$R_{cp} = \frac{128 \times \eta_{cp} \times l_{cp}}{\pi \times d_{cp}^4} \times (1 + a)$$

where $Re_{cp} = \frac{4 \times Q \times \rho}{Z \times \pi \times d_{cp} \times \eta_{cp}}$

and $a = \frac{1,08}{32} \times Re_{cp} \times \frac{d_{cp}}{l_{cp}} = \frac{1,08}{32} \times \frac{4 \times Q \times \rho}{Z \times \pi \times l_{cp} \times \eta_{cp}}$

The portion of the non-linear term, a (inertia factor), has the effect that the exponent $k < 1$ in the abovementioned formula for Q/Z . Exponent k can be calculated by approximation as follows:

$$k = \frac{1 + a}{1 + 2 \times a}$$

Without greater errors, it is permitted to take $a = 0,1$ to $0,2$ and to calculate with exponent $k = 1$. With regard to the different lubricant flow rates in the particular recesses ($\varepsilon \neq 0$), a Reynolds number of $Re_{cp} = 1\,000$ to $1\,500$ shall not be exceeded.

A.3.2.3 Axial lubricant flow rate

The volume flow from recess i in the axial direction is

$$Q_{ax,i} = 2 \times \int_{\varphi_{1,i} + \varphi_G}^{\varphi_{2,i} - \varphi_G} \frac{h^3}{12 \times \eta_B} \times \frac{p_i}{l_{ax}} \times \frac{D}{2} \times d\varphi$$

where $\varphi_G = \frac{l_c + b_G}{D}$

h is not constant due to the shaft eccentricity.

If, for the initial angle $\varphi'_{1,i} = \varphi_{1,i} + \varphi_G$ or for the end angle $\varphi'_{2,i} = \varphi_{2,i} - \varphi_G$ and

$$\begin{aligned} \alpha_i &= \int_{\varphi'_{1,i}}^{\varphi'_{2,i}} \frac{h^3}{C_R^3} d\varphi = \int_{\varphi'_{1,i}}^{\varphi'_{2,i}} (1 + \varepsilon \cos \varphi)^3 \times d\varphi \\ &= \left[(\varphi'_2 - \varphi'_1) \times \left(1 + \frac{3}{2} \times \varepsilon^2 \right) + (\sin \varphi'_2 - \sin \varphi'_1) \times (3\varepsilon + \varepsilon^3) + \frac{3}{4} \times \varepsilon^2 \times (\sin 2\varphi'_2 - \sin 2\varphi'_1) \right. \\ &\quad \left. - \frac{\varepsilon^3}{3} \times (\sin^3 \varphi'_2 - \sin^3 \varphi'_1) \right]_i \end{aligned}$$

then

$$Q_{ax,i} = \frac{C_R^3 \times D}{12 \times \eta_B \times l_{ax}} \times \alpha_i \times p_i$$

A.3.2.4 Circumferential lubricant flow rate

When the volume flow rate in the circumferential direction is calculated, a flow between parallel plates with film thicknesses of $h_{en,i} = h(\varphi'_{1,i})$ or $h_{ex,i} = h(\varphi'_{2,i})$ is assumed as an approximation.

In the circumferential direction, for the volume flow flowing in:

$$Q_{en,i} = b_c \times \left(\frac{U \times h_{en,i}}{2} - \frac{p_i \times h_{en,i}^3}{12 \times \eta_B \times l_c} \right)$$

and by analogy, the following applies to the volume flow flowing out:

$$Q_{ex,i} = b_c \times \left(\frac{U \times h_{ex,i}}{2} + \frac{p_i \times h_{ex,i}^3}{12 \times \eta_B \times l_c} \right)$$

A.3.2.5 Lubricant flow from the capillary restrictor

According to [Figure A.4](#), the continuity equation for recess i results in

$$Q_{cp,i} = Q_{ax,i} + Q_{ex,i} - Q_{en,i}$$

$Q_{cp,i}$ is the rate of lubricant flow from the capillary restrictor into the recess i and is given by Hagen-Poiseuille law as follows:

$$Q_{cp,i} = \frac{(p_{en} - p_i)}{R_{cp}}$$

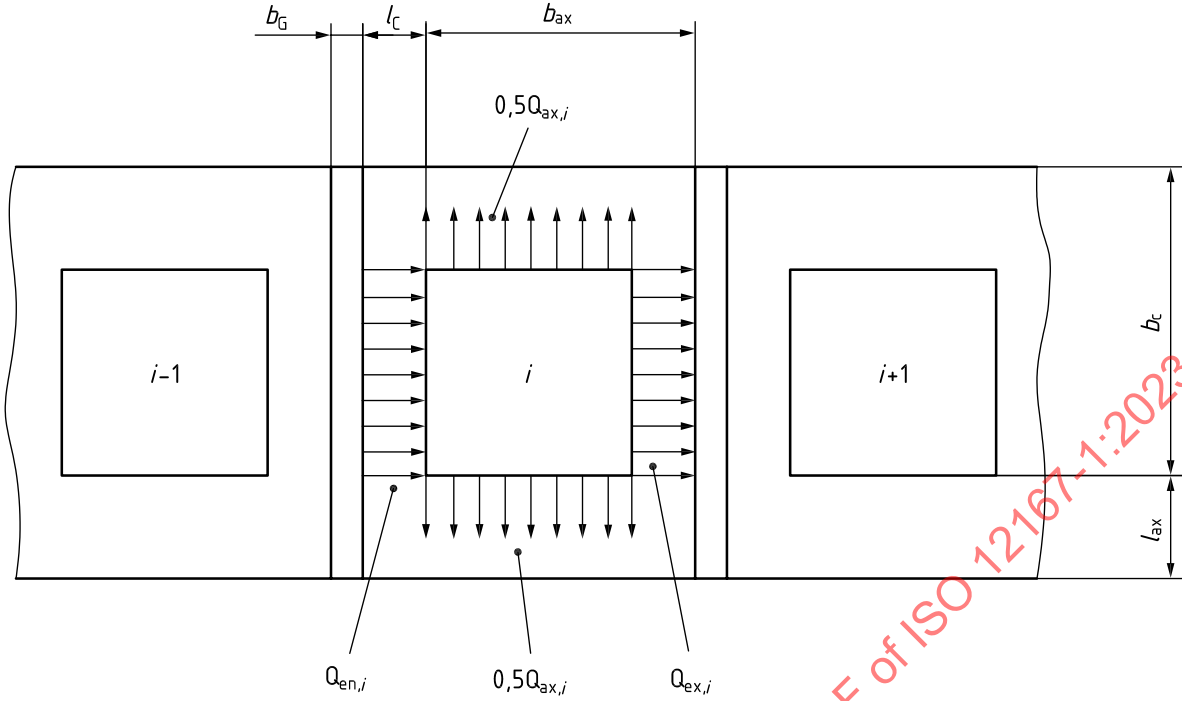


Figure A.4 — Volume flows for one recess (figure represented in flattened for sliding surface)

If $f_{en,i} = 1 + \varepsilon \times \cos \varphi'_{1,i}$ and $f_{ex,i} = 1 + \varepsilon \times \cos \varphi'_{2,i}$

$$\omega = 2 \times \pi \times N = \frac{2 \times U}{D}$$

$$P_i^* = \frac{p_i}{p_{en}}$$

The speed dependent parameter is

$$K_{rot} = \frac{\eta_B \times \omega \times \xi \times k \times l_c}{p_{en} \times \psi^2 \times D}$$

where the relative bearing clearance is $\psi = \frac{2 \times C_R}{D}$,

the resistance ratio is $k = \frac{R_{p,ax}}{R_{p,c}} = \frac{l_{ax} \times b_c}{l_c \times b_{ax}}$,

the flow resistance of one recess at $\varepsilon = 0$ is $R_{p,0} = \frac{R_{p,ax}}{2(1+k)} = \frac{R_{p,c} \times k}{2(1+k)}$

and the restrictor ratio is $\xi = \frac{R_{cp}}{R_{p,0}} = \frac{R_{cp} \times b_{ax} \times C_R^3}{6 \times \eta_B \times l_{ax}} \times (1+k)$.

Then the pressure p_i^* in the recess i results from

$$p_i^* = \frac{p_i}{p_{\text{en}}} = \frac{1 - \frac{6 \times K_{\text{rot}}}{1+k} (f_{\text{ex},i} - f_{\text{en},i})}{1 + \frac{a_i \times \xi}{2(1+k) \left(\frac{\pi}{Z} - \varphi_G \right)} + \frac{k \times \xi \times (f_{\text{en},i}^3 + f_{\text{ex},i}^3)}{2(1+k)}}$$

Thus, the relative pressures in the recesses and all further bearing parameters are determined by:

- a) restrictor ratio, ξ ;
- b) bearing geometry:
 - number of recesses, Z ,
 - form and position of recesses, (κ, α) ,
 - position of journal, (ε, β) ;
- c) speed dependent parameter, K_{rot} .

The angle β is determined iteratively in the course of the calculation.

A.3.3 Load F , attitude angle β , stiffness c

The radial load effect on recess i in accordance with [Figure A.5](#) is given by

$$F_i = b_c \times \int_{-\frac{\pi}{Z} - \varphi_G}^{\frac{\pi}{Z} - \varphi_G} p_i \cos \delta \times \frac{D}{2} \times d\delta = D \times b_c \times p_i \sin \left(\frac{\pi}{Z} - \varphi_G \right)$$

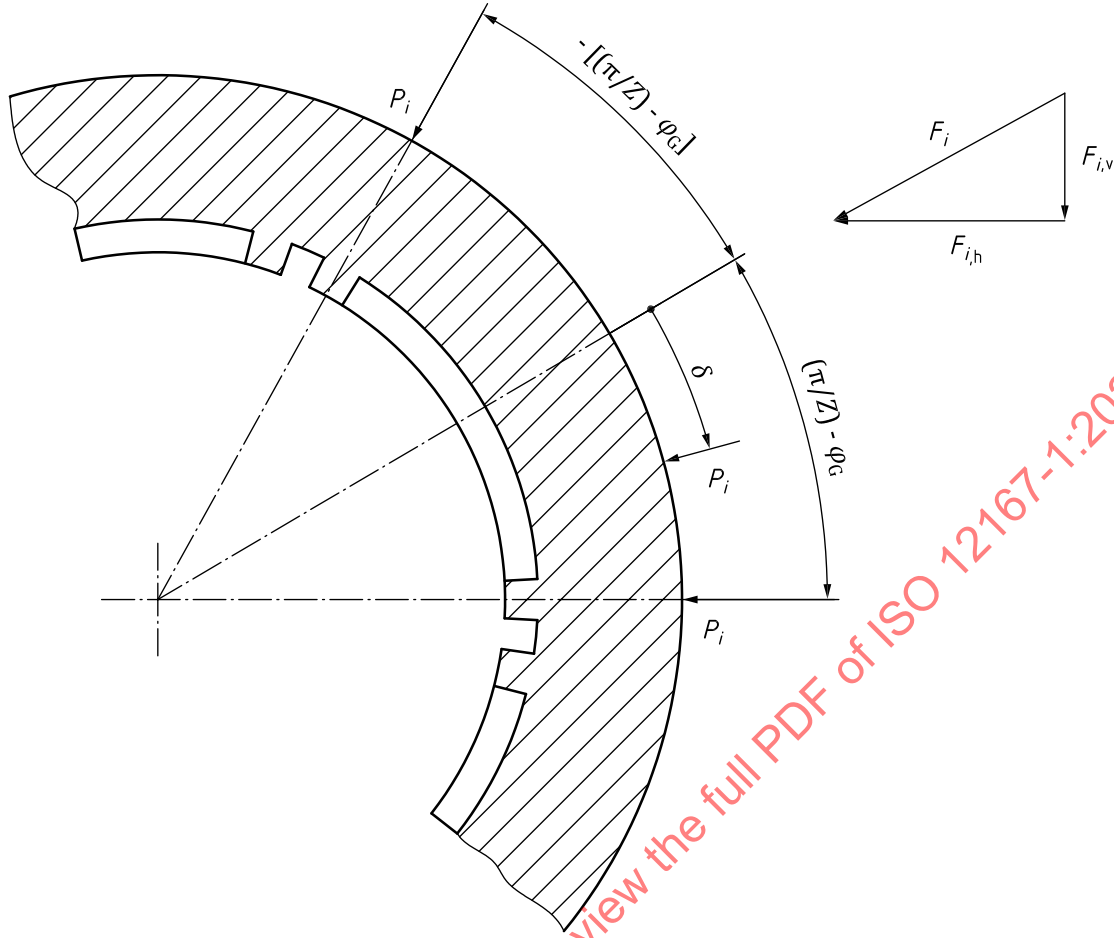


Figure A.5 — Application of load to one recess

The direction of F_i is given by

$$\bar{\varphi}_i = \frac{\varphi_{en,i} + \varphi_{ex,i}}{2}$$

The horizontal component is the sum of all horizontal projections of F_i is given by

$$F_h = b_c \times D \times \sin\left(\frac{\pi}{Z} - \varphi_G\right) \times \sum_{i=1}^Z p_i \times \sin(\bar{\varphi}_i + \beta)$$

Correspondingly, for the vertical component

$$F_v = b_c \times D \times \sin\left(\frac{\pi}{Z} - \varphi_G\right) \times \sum_{i=1}^Z p_i \times \cos(\bar{\varphi}_i + \beta)$$

where

$$\bar{\varphi}_i + \beta = \alpha + \frac{2\pi}{Z} \times (i-1)$$

The total load is $F = \sqrt{F_h^2 + F_v^2}$

Angle of the resulting force $\varphi_F = \arctan \frac{F_h}{F_v}$

In case of vertical load, the attitude angle for each ε should be modified in such a way that $\varphi_F = 0$. If the load-carrying capacity F is not applied vertically but at an angle φ_F to a perpendicular line, then the results for vertical direction of load can be applied when mounting the plain bearing at the angle φ_F .

The stiffness c can generally be defined in different ways.

Here, the following definition is used:

$$c = \frac{F}{e} = \frac{F}{\varepsilon \times C_R}$$

A.3.4 Lubricant flow rate and pumping power

The total lubricant flow rate can be calculated on the basis of the sum of the flow rates through the restrictors, $Q_{cp,i}$:

$$Q = \sum_{i=1}^Z Q_{cp,i} = \frac{Z \times p_{en} - \sum p_i}{R_{cp}}$$

The lubricant flow rate can also be approximated according to [Formula \(7\)](#).

Pumping power, $P_p = Q \times p_{en}$

A.3.5 Frictional power

The frictional power is composed of

- a) friction in the land area, and
- b) friction in the recesses due to secondary flow.

The land area is given by

$$A_{lan} = 2 \times \pi \times l_{ax} \times D + 2 \times Z \times l_c \times (B - 2 \times l_{ax}) - 2 \times Z \times b_G \times l_{ax}$$

$$A_{lan}^* = \frac{A_{lan}}{\pi \times B \times D} = \frac{2}{\pi} \times \left\{ \frac{l_{ax}}{B} \times \pi + Z \times \frac{l_c}{D} \times \left(1 - 2 \times \frac{l_{ax}}{B} \right) - Z \times \frac{b_G}{D} \times \frac{l_{ax}}{B} \right\}$$

The shearing stress at the shaft surface is, in general, given by

$$\tau = \eta_B \left(\frac{\partial u}{\partial y} \right)_{y=h} = \frac{1}{2} \times \frac{\partial p}{\partial x} \times h + \frac{U}{h} \times \eta_B$$

As an approximation, the shearing stress τ is calculated as follows without taking into account the pressure flow rate.

$$\tau = \frac{U}{h} \times \eta_B$$

The result for the land friction is finally given by

$$P_{f,lan} = \int_{A_{lan}} \tau \times U \times dA = \frac{\eta \times U^2}{C_R} \times \int_{A_{lan}} \frac{dA}{1 + \varepsilon \times \cos \varphi}$$

If it is assumed that the lands are uniformly distributed over the periphery, it can be simplified as follows:

$$P_{f,lan} = \frac{\eta \times U^2}{C_R} \times \frac{A_{lan}}{\sqrt{1 - \varepsilon^2}}$$

Although the depth of recess $h_p \gg h$ according to Shinkle and Hornung,^[6] the friction due to the secondary flow in the recesses shall be included in the calculation for shafts running at high speed. This applies especially to wide recesses and small lands.

When the flow in the recesses is still laminar, i.e.

$$Re_p = \frac{U \times h_p \times \rho}{\eta_B} < 1\,000$$

then the friction in the recesses is calculated as follows:

$$P_{f,p} = 4 \times \frac{\eta \times U^2}{h_p} \times A_p$$

where

$$A_p = \pi \times B \times D - A_{lan}$$

When $Re_p > 1\,000$, then the flow is turbulent and the friction increases correspondingly. In that case, the preceding formula for τ can no longer be used.

A.3.6 Formulae for dimensioning

The following formulae can be used to determine the dimensions when stiffness c is given:

$$C_R = \frac{F}{\varepsilon \times c}$$

$$D^2 \times p_{en} = \frac{F}{\frac{B}{D} \times F^*}$$

$$\frac{p_{en}^2}{\eta_B} = \frac{F \times \omega}{C_R^2} \times \frac{1}{4 \times \frac{B}{D} \times F^* \times \pi_f}$$

Annex B (informative)

Example of calculation according to the method given in [Annex A](#)

B.1 Example 1 — Calculation of a hydrostatic journal bearing

B.1.1 General

A bearing with four recesses with given dimensions and operational data are to be examined. The lubricant oil, ISO VG 46, and the temperature in front of the bearing are also stated. The amount of oil, power, stiffness, film thickness, etc. are to be calculated. The following parameters are given.

B.1.2 Dimensions

- Bearing diameter, $D = 0,12$ m
- Bearing width, $B = 0,12$ m
- Width of circumferential outlet, $b_c = 0,108$ m
- Axial land length, $l_{ax} = 0,012$ m
- Circumferential land length, $l_c = 0,012$ m
- Width of drainage groove, $b_G = 0,006$ m
- Depth of recess, $h_p = 40 C_R$ m
- Number of recesses, $Z = 4$
- Diameter of capillaries, $d_{cp} = 0,003\ 25$ m
- Length of capillaries, $l_{cp} = 1,14$ m
- Relative bearing clearance, $\psi = 1,5 \times 10^{-3}$
- Radial clearance, $C_R = \psi \times \frac{D}{2} = 90 \times 10^{-6}$ m

B.1.3 Operational data

- Load-carrying capacity (load), $F = 20\ 000$ N
- Rotational frequency (speed), $N = 16,66\ s^{-1}$ ($\omega = 2 \times \pi \times N \cong 104,7\ s^{-1}$)
- Inlet temperature, $T_{en} = 45\ ^\circ\text{C}$
- Feed pressure, $p_{en} = 60\ \text{bar} = 6 \times 10^6\ \text{Pa}$

B.1.4 Lubricant data

[Table B.1](#) is given the lubricant data for ISO VG 46.

Table B.1 — Temperature dependence for ISO VG 46

T °C	η Pa·s
40	0,041 40
50	0,026 58
60	0,018 07

— Volume specific heat, $c_p \cdot \rho = 1,75 \times 10^6 \text{ J/m}^3 \cdot \text{K}$

— Density, $\rho = 900 \text{ kg/m}^3$

Exponent, calculated on the basis of the lubricant data, $\gamma = \frac{1}{10} \times \ln \frac{\eta_{40}}{\eta_{50}} \cong \frac{1}{10} \times \ln \frac{0,041\,40}{0,026\,58} \cong 0,044\,3$

These data are used to calculate the parameters listed in [B.1.5](#) to [B.1.18](#).

B.1.5 Temperatures and dynamic viscosities

The frictional power is not yet known from the first calculation. It is therefore approximated as follows with ($\xi = 1$, $P^* = 0$).

$$\Delta T_{cp} = \frac{p_{en}}{c_p \times \rho} \times \left(\frac{\xi}{1 + \xi} \right) = \frac{6 \times 10^6}{1,75 \times 10^6} \times \left(\frac{1}{1 + 1} \right) \cong 1,7 \text{ K}$$

$$\Delta T_B = \frac{p_{en}}{c_p \times \rho} \times \left(\frac{1}{1 + \xi} + P^* \right) = \frac{6 \times 10^6}{1,75 \times 10^6} \times \left(\frac{1}{1 + 1} + 0 \right) \cong 1,7 \text{ K}$$

$$T_{cp} = T_{en} + \frac{\Delta T_{cp}}{2} \cong 45 + \frac{1,7}{2} \cong 45,85 \text{ °C}$$

$$T_B = T_{en} + \Delta T_{cp} + \frac{\Delta T_B}{2} \cong 45 + 1,71 + \frac{1,7}{2} \cong 47,55 \text{ °C}$$

The dynamic viscosities are then given by

$$\eta_{cp} = \eta_{40} \times \exp[-\gamma \times (T_{cp} - 40)] \cong 0,041\,4 \times \exp[-0,044\,3 \times (45,85 - 40)] \cong 0,031\,9 \text{ Pa} \cdot \text{s}$$

$$\eta_B = \eta_{40} \times \exp[-\gamma \times (T_B - 40)] \cong 0,041\,4 \times \exp[-0,044\,3 \times (47,55 - 40)] \cong 0,029\,6 \text{ Pa} \cdot \text{s}$$

B.1.6 Flow resistances

$$R_{cp} = \frac{128 \times \eta_{cp} \times l_{cp}}{\pi \times d_{cp}^4} \times (1 + a) \cong \frac{128 \times 0,031\,9 \times 1,14}{\pi \times 0,003\,25^4} \times (1 + 0,2) \cong 1,594 \times 10^{10} \text{ Pa} \cdot \text{s/m}^3$$

The inertia factor a cannot yet be calculated in this place, as the oil flow rate is not known. Therefore, it should be started with an estimated value and the exact value of a determined iteratively. Here, the value has been taken from the following calculation.

$$R_{p,0} = \frac{R_{lan,ax}}{2 \times (1 + k)} = \frac{6 \times \eta_B}{C_R^3} \times \frac{\frac{l_c}{D}}{\frac{b_c}{B}} \times \frac{D}{B} \times \frac{k}{1 + k} \cong \frac{6 \times 0,029\,6 \times 0,1 \times 1 \times 1,43}{(90 \times 10^{-6})^3 \times 0,9 \times 2,43} \cong 1,593 \times 10^{10} \text{ Pa} \cdot \text{s/m}^3$$

κ is calculated in [B.1.9](#).