
**Plastics — Determination of
tension-tension fatigue crack
propagation — Linear elastic fracture
mechanics (LEFM) approach**

*Plastiques — Détermination de la propagation de fissure par fatigue en
traction — Approche de la mécanique linéaire élastique de la rupture
(LEFM)*



PDF disclaimer

This PDF file may contain embedded typefaces. In accordance with Adobe's licensing policy, this file may be printed or viewed but shall not be edited unless the typefaces which are embedded are licensed to and installed on the computer performing the editing. In downloading this file, parties accept therein the responsibility of not infringing Adobe's licensing policy. The ISO Central Secretariat accepts no liability in this area.

Adobe is a trademark of Adobe Systems Incorporated.

Details of the software products used to create this PDF file can be found in the General Info relative to the file; the PDF-creation parameters were optimized for printing. Every care has been taken to ensure that the file is suitable for use by ISO member bodies. In the unlikely event that a problem relating to it is found, please inform the Central Secretariat at the address given below.

STANDARDSISO.COM : Click to view the full PDF of ISO 15850:2002

© ISO 2002

All rights reserved. Unless otherwise specified, no part of this publication may be reproduced or utilized in any form or by any means, electronic or mechanical, including photocopying and microfilm, without permission in writing from either ISO at the address below or ISO's member body in the country of the requester.

ISO copyright office
Case postale 56 • CH-1211 Geneva 20
Tel. + 41 22 749 01 11
Fax + 41 22 749 09 47
E-mail copyright@iso.ch
Web www.iso.ch

Printed in Switzerland

Contents

Page

Foreword.....	iv
1 Scope	1
2 Normative references	1
3 Terms and definitions	1
4 Principle.....	4
5 Significance and use	4
6 Test specimens	5
7 Apparatus	9
8 Test procedure	14
9 Calculation and interpretation of results	14
10 Test report	16
Bibliography	17

Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

International Standards are drafted in accordance with the rules given in the ISO/IEC Directives, Part 3.

The main task of technical committees is to prepare International Standards. Draft International Standards adopted by the technical committees are circulated to the member bodies for voting. Publication as an International Standard requires approval by at least 75 % of the member bodies casting a vote.

Attention is drawn to the possibility that some of the elements of this International Standard may be the subject of patent rights. ISO shall not be held responsible for identifying any or all such patent rights.

ISO 15850 was prepared by Technical Committee ISO/TC 61, *Plastics*, Subcommittee SC 2, *Mechanical properties*.

STANDARDSISO.COM : Click to view the full PDF of ISO 15850:2002

Plastics — Determination of tension-tension fatigue crack propagation — Linear elastic fracture mechanics (LEFM) approach

1 Scope

This International Standard specifies a method for measuring the propagation of a crack in a notched specimen subjected to a cyclic tensile load varying between a constant positive minimum and a constant positive maximum value. The test results include the crack length as a function of the number of load cycles and the crack length increase rate as a function of the stress intensity factor and energy release rate at the crack tip. The possible occurrence of discontinuities in crack propagation is detected and reported.

The method is suitable for use with the following range of materials:

- rigid and semi-rigid thermoplastic moulding and extrusion materials (including filled and short-fibre-reinforced compounds) plus rigid and semi-rigid thermoplastic sheets;
- rigid and semi-rigid thermosetting materials (including filled and short-fibre-reinforced compounds) plus rigid and semi-rigid thermosetting sheets.

2 Normative references

The following normative documents contain provisions which, through reference in this text, constitute provisions of this International Standard. For dated references, subsequent amendments to, or revisions of, any of these publications do not apply. However, parties to agreements based on this International Standard are encouraged to investigate the possibility of applying the most recent editions of the normative documents indicated below. For undated references, the latest edition of the normative document referred to applies. Members of ISO and IEC maintain registers of currently valid International Standards.

ISO 291, *Plastics — Standard atmospheres for conditioning and testing*

ISO 527 (all parts), *Plastics — Determination of tensile properties*

ISO 2818, *Plastics — Preparation of test specimens by machining*

ISO 13586, *Plastics — Determination of fracture toughness (G_{IC} and K_{IC}) — Linear elastic fracture mechanics (LEFM) approach*

3 Terms and definitions

For the purposes of this International Standard, the following terms and definitions apply.

3.1 cycle

smallest segment of a load-time or stress-time function which is repeated periodically

NOTE The terms fatigue cycle, load cycle and stress cycle are also commonly used.

3.2

number of cycles completed

N

number of load cycles since the beginning of a test

3.3

waveform

shape of the load-time curve within a single cycle

3.4

maximum load

$P_{\max}$

highest value of the load during a cycle

NOTE 1 It is expressed in newtons.

NOTE 2 Only positive, i.e. tensile, loads are used in this test method.

3.5

minimum load

$P_{\min}$

lowest value of the load during a cycle

NOTE 1 It is expressed in newtons.

NOTE 2 Only positive, i.e. tensile, loads are used in this test method.

3.6

load range

ΔP

difference between the maximum and the minimum loads in one cycle, given by:

$$\Delta P = P_{\max} - P_{\min}$$

3.7

load ratio

stress ratio

R

ratio of the minimum to the maximum load in one cycle, i.e.:

$$R = P_{\min}/P_{\max}$$

3.8

stress intensity factor

K

limiting value of the product of the stress $\sigma(r)$ perpendicular to the crack area at a distance r from the crack tip and of the square root of $2\pi r$, as r tends to zero:

$$K = \lim_{r \rightarrow 0} \sigma(r) \sqrt{2\pi r}$$

NOTE 1 It is expressed in pascal root metres ($\text{Pa} \cdot \text{m}^{1/2}$).

NOTE 2 The term factor is used here because it is in common usage, even though the quantity has dimensions.

[ISO 13586]

3.9

maximum stress intensity factor

$K_{\max}$

highest value of the stress intensity factor in one cycle

3.10**minimum stress intensity factor** $K_{\min}$

lowest value of the stress intensity factor in one cycle

3.11**stress intensity factor range** ΔK

difference between the maximum and minimum stress intensity factors in one cycle, given by:

$$\Delta K = K_{\max} - K_{\min}$$

3.12**energy release rate** G difference between the external work δU_{ext} done on a body to enlarge a cracked area by an amount δA and the corresponding change in strain energy δU_{S} :

$$G = \frac{\delta U_{\text{ext}}}{\delta A} - \frac{\delta U_{\text{S}}}{\delta A}$$

NOTE 1 It is expressed in joules per square metre.

NOTE 2 Assuming linear elastic behaviour, the following relationship between the stress intensity factor K and the energy release rate G holds:

$$G = \frac{K^2}{E'}$$

where

$$E' = E \text{ for plane stress, and } E' = \frac{E}{1 - \nu^2} \text{ for plane strain conditions;}$$

 E and ν are the tensile modulus and Poisson's ratio respectively.**3.13****maximum energy release rate** $G_{\max}$

highest value of the energy release rate in one cycle

3.14**minimum energy release rate** $G_{\min}$

lowest value of the energy release rate in one cycle

3.15**energy release rate range** ΔG

difference between the maximum and minimum energy release rates in one cycle, given by:

$$\Delta G = G_{\max} - G_{\min}$$

3.16**notch**

sharp indentation made in the specimen, generally using a razor blade or a similar sharp tool, before a test and intended as the starting point of a fatigue-induced crack

3.17

initial crack length

a_0

length of the notch (3.16)

NOTE 1 It is expressed in metres.

NOTE 2 For compact tensile (CT) specimens, it is measured from the line joining the load-application points (i.e. the line through the centres of the loading-pin holes) to the notch tip (see Figure 2). For single-edge-notched tensile (SENT) specimens, it is measured from the edge of the specimen to the notch tip. Details of the measurement procedure are given in 7.3.

3.18

crack length

a

total crack length at any time during a test, given by the initial crack length a_0 plus the crack length increment due to fatigue loading

NOTE It is expressed in metres.

3.19

fatigue crack growth rate

da/dN

rate of crack extension caused by fatigue loading and expressed in terms of average crack extension per cycle

NOTE It is expressed in metres per cycle.

3.20

stress intensity calibration

mathematical expression, based on empirical or analytical results, that relates the stress intensity factor to load and crack length for a specific specimen geometry

3.21

gauge length

L_0

(single-edge-notched tensile (SENT) specimen) free distance between the upper and lower grips after the specimen has been mounted in the test machine

NOTE It is expressed in metres.

4 Principle

A constant-amplitude cyclic tensile load is imposed on a specimen under suitable test conditions (specimen shape and size, notching, maximum and minimum loads, load cycle frequency, etc.), causing a crack to start from the notch and propagate.

The crack length a is monitored during the test and recorded as a function of the number N of load cycles completed.

Numerical differentiation of the experimental function $a(N)$ provides the fatigue crack growth rate da/dN which is reported as a function of stress intensity factor and energy release rate at the crack tip.

5 Significance and use

Fatigue crack propagation, particularly when expressed as the fatigue crack growth rate da/dN as a function of crack-tip stress intensity factor range ΔK or energy release rate range ΔG characterizes a material's resistance to stable crack extension under cyclic loading. Background information on the fatigue behaviour of plastics and on the fracture mechanics approach to fatigue for these materials is given in [1] and [2] (see the Bibliography).

Expressing da/dN as a function of ΔK or ΔG provides results that are independent of specimen geometry, thus enabling exchange and comparison of data obtained with a variety of specimen configurations and loading conditions. Moreover, this feature enables da/dN versus ΔK or ΔG data to be utilized in the design and evaluation of engineering structures. The concept of similitude is assumed, which implies that cracks of differing lengths subjected to the same nominal ΔK or ΔG will advance by equal increments of crack extension per cycle.

Fatigue crack propagation data are not geometry-independent in the strict sense since thickness effects generally occur. The potential effects of specimen thickness have to be considered when generating data for research or design.

Anisotropy in the molecular orientation or in the structure of the material, and the presence of residual stresses, can have an influence on fatigue crack propagation behaviour. The effect can be significant when test specimens are removed from semi-finished products (e.g. extruded sheets) or finished products. Irregular crack propagation, namely excessive crack front curvature or out-of-plane crack growth, generally indicates that anisotropy or residual stresses are affecting the test results.

This test method can serve the following purposes:

- a) to establish the influence of fatigue crack propagation on the lifetime of components subjected to cyclic loading, provided data are generated under representative conditions and combined with appropriate fracture toughness data (see ISO 13586) and stress analysis information;
- b) to establish material-selection criteria and inspection requirements for damage-tolerant applications;
- c) to establish, in quantitative terms, the individual and combined effects of the material's structure, the processing conditions and the loading variables on fatigue crack propagation.

6 Test specimens

6.1 Shape and size

6.1.1 Standard specimens

Two different types of specimen can be used: single-edge-notched tensile (SENT) and compact tensile (CT). Figures 1 and 2 describe their geometrical characteristics.

6.1.2 Thickness and width

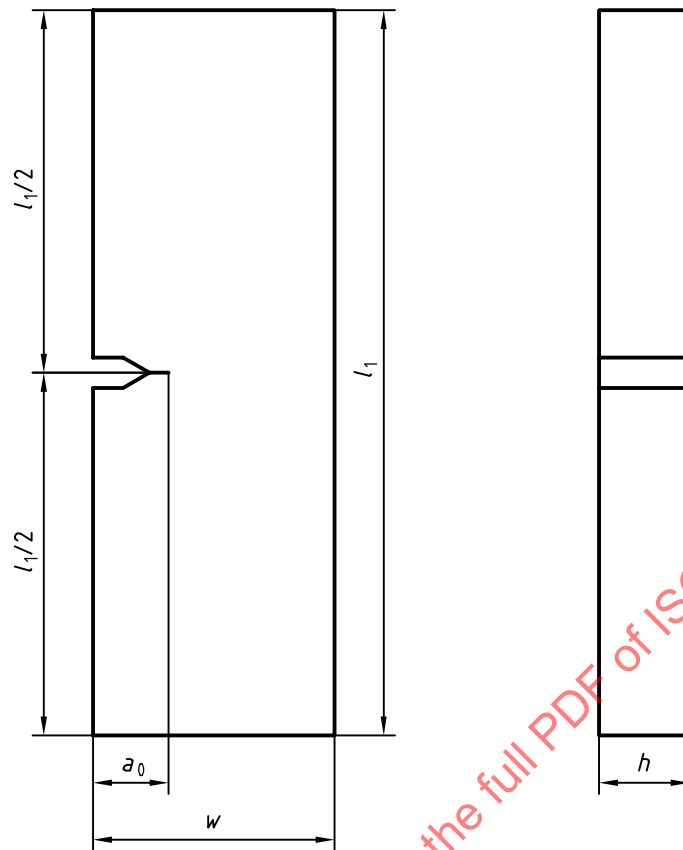
When the specimen thickness h is too small compared to the width w , it is difficult to avoid lateral deflections or out-of-plane bending of the specimen. Conversely, with very thick specimens, through-thickness crack curvature corrections are often necessary and difficulties may be encountered in meeting the through-thickness straightness requirement of 8.1.

On the basis of these considerations, the following limits are recommended for h and w :

- a) for CT specimens, $w/10 \leq h \leq w/2$;
- b) for SENT specimens, $w/20 \leq h \leq w/4$.

It should be noted that the test results are in general thickness-dependent: specimens obtained from the same material but having different thicknesses are likely to give different responses.

It is usually convenient to make the thickness h of specimens equal to the thickness of the sheet sample from which the specimens are cut.

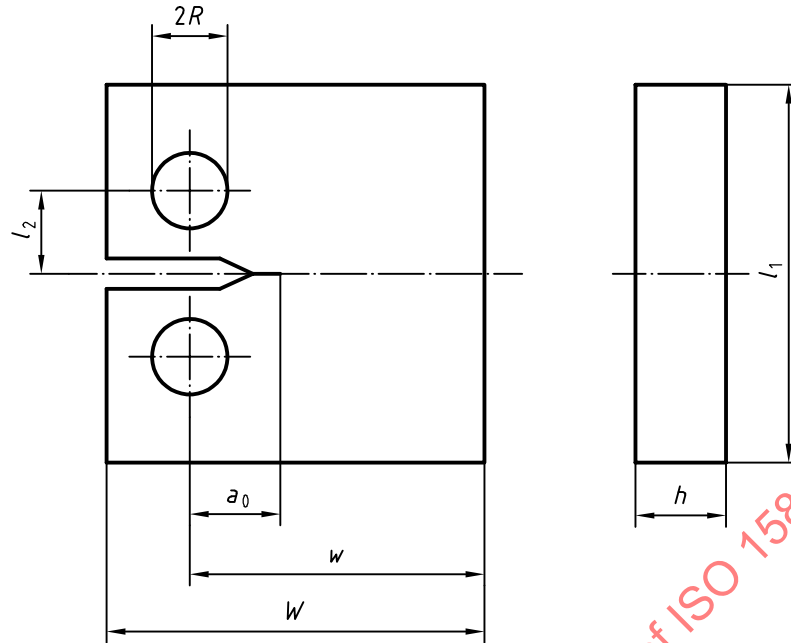


Key

w	Width	$w/20 \leq h \leq w/4$ (recommended)
l_1	Length	$l_1 > 2,5w$
h	Thickness	
a_0	Initial crack length	

The notch shall be within $\pm 0,01w$ of the specimen centreline.

Figure 1 — Standard single-edge-notched tensile (SENT) specimen for fatigue crack propagation testing

**Key**

w	Effective width	$w/10 \leq h \leq w/2$ (recommended)
W	Overall width	$W = 1,25w \pm 0,01w$
l_1	Length	$l_1 = 1,2w \pm 0,01w$
l_2	Distance between centres of loading-pin holes located symmetrically to the crack plane to within $\pm 0,005w$	$l_2 = 0,55w \pm 0,005w$
R	Radius of loading-pin hole	$R = 0,125w \pm 0,005w$
h	Thickness	
a_0	Initial crack length	$a_0 \geq 0,2w$

The notch shall be within $\pm 0,01w$ of the specimen centreline.

Figure 2 — Standard compact tensile (CT) specimen for fatigue crack propagation testing

6.1.3 Size requirements

In order for the results obtained by this test method to be valid, it is required that the material behaviour be predominantly linear elastic at all values of applied load and crack length. Deviations may arise from either viscoelastic behaviour of the material or large-scale plasticity ahead of the crack tip. The former may result in significant non-linearity of the mechanical behaviour, possibly aggravated by a progressive rise of the specimen temperature during the test. The test procedure outlined in this International Standard is therefore recommended only for materials exhibiting very limited viscoelasticity under the loading frequency used and for the expected test duration. Large-scale plasticity of the ligament can be avoided by ensuring that the plastic zone around the crack tip is small compared with the size of the uncracked ligament ($w - a$). On the basis of previous experience with metallic materials^[3], it is required that the following size limits be satisfied in order for the test results to be valid:

$$(w - a) \geq (4/\pi) (K_{\max}/\sigma_y)^2 \quad (1)$$

where

$w - a$ is the uncracked-specimen ligament width;

σ_y is the tensile-yield stress measured in accordance with the relevant part of ISO 527.

The same size limits are expressed in graphical form in Figure 3, where the dimensionless quantities $K_{\max}/(\sigma_y \sqrt{w})$ and a/w are plotted against each other. All combinations of specimen size, crack length, material yield stress and stress intensity factor which lie below the curve in Figure 3 satisfy the specimen size requirements of this test method.

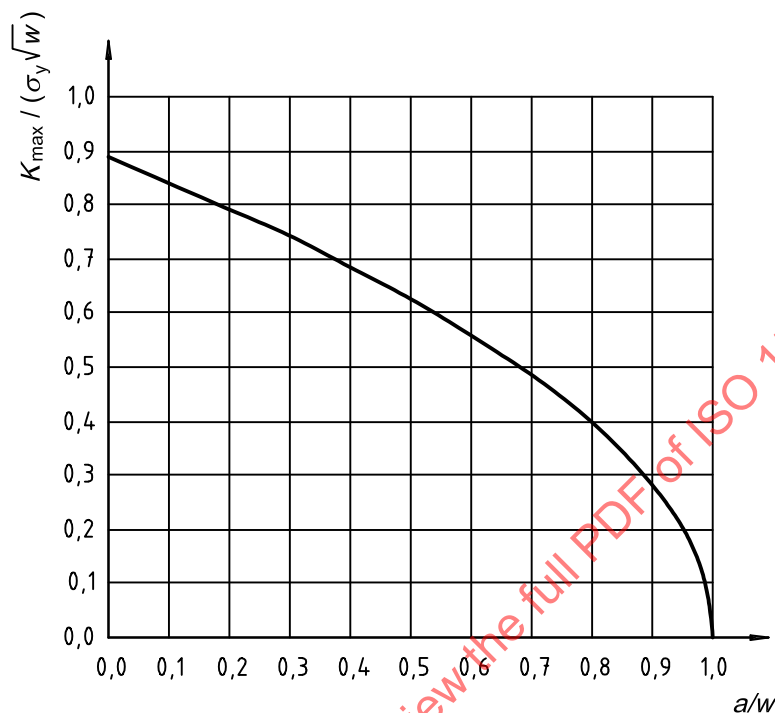


Figure 3 — Size requirements for standard fatigue crack propagation specimens
(Values which lie below the curve satisfy the specimen size requirements of this method)

6.2 Preparation

Prepare specimens in accordance with the relevant materials specification and in accordance with ISO 2818. In the case of anisotropic materials, take care to indicate the reference direction on each specimen.

6.3 Notching

Produce a sharp notch or, when feasible, a natural crack, intended as the starting point of the fatigue-induced crack, in the specimen at the locations depicted in Figures 1 and 2, either in a single step or by sharpening the tip of a blunt slot or notch made by machining.

It is required that the initial crack length a_0 in the CT specimen be at least $0,2w$ so that K -calibration is not influenced by small variations in the location and dimensions of the loading-pin holes. The notch length in CT specimens shall be chosen accordingly (see 7.3 for details of measurement of initial crack length a_0).

The notch in both the CT and SENT specimens shall be within $\pm 0,01w$ of the specimen centreline.

When sharpening a blunt notch produced by machining, the length of the sharp notch shall be more than four times the blunt notch tip radius. Method a), b), c) or d) can be used to create a natural crack or a sharp notch:

- a) Machine a sharp notch in the specimen and then generate a natural crack by tapping on a new razor blade placed in the notch (it is essential to practice this since, in brittle specimens, a natural crack can be generated by this process but some skill is required in avoiding too long a crack or local damage).

- b) If control is difficult or repeatability problems are experienced with method a), it is possible with some brittle specimens to generate a sharp notch by simply pressing the razor blade against the specimen at a temperature close to, but lower than, the glass-transition temperature of the material. With this notching procedure, proper handling of the specimen and correct choice of temperature are essential to avoid deformation of, or damage to, the specimen. Use a new razor blade for each specimen.
- c) If a natural crack cannot be generated, as in tough specimens, then sharpen the notch by sliding a razor blade across the notch. Use a new razor blade for each specimen.
- d) With tough materials, cooling the specimen and then tapping with a razor blade is sometimes successful.

It may be useful to check the effectiveness of the notching procedure by performing preliminary tests at a constant displacement or constant loading rate on specimens notched using different methods. The best notching method is the one which gives the lowest K -value at crack initiation.

6.4 Side grooves

Specimens may need side grooves to avoid the crack path deviating from the plane of symmetry (see 8.4), and to promote straighter crack fronts. Side grooves may also, in some cases, improve the visibility of the crack tip when using visual methods for crack length measurement.

The side grooves shall be equal in depth, have an included angle of $45^\circ \pm 5^\circ$ and have a root radius of $0,25 \text{ mm} \pm 0,05 \text{ mm}$.

The total reduction in specimen thickness due to side grooving shall not exceed $0,2h$.

When using side grooves, the specimen thickness h shall be taken as the distance between the roots of the side grooves.

6.5 Conditioning

After notching, condition specimens as specified in the International Standard for the material tested. In the absence of this information, select the most appropriate conditions from ISO 291, unless otherwise agreed upon by the interested parties.

7 Apparatus

7.1 Test machine

7.1.1 General

The test machine shall be capable of imposing a prescribed load on the specimen (i.e. of operating in the "load control" mode), and of varying the load with time in accordance with a specified waveform. The load distribution shall be symmetrical to the specimen notch. Hydraulically driven test machines with electronic control are generally suitable for this purpose. Mechanically driven machines can also be used, but are less versatile as regards the cycle types and frequency range available.

7.1.2 Load-cycle waveform

The most commonly employed waveform is a sine wave, but other types, e.g. triangular or square waves, may be used when simulating service conditions or investigating the effects of the waveform itself. Two important test variables, namely maximum load $P_{\max}$ and load ratio R , characterize the load-cycle waveform and significantly affect the test results. Load as a function of time shall be controlled with an accuracy of $\pm 1 \%$, and the maximum and minimum load values shall be constant, during the entire test, to within 1% .

7.1.3 Load-cycle frequency

The frequency of the load cycle is a test parameter that may be adjusted according to different criteria, such as the simulation of service conditions or the investigation of the effects of the frequency on the test results. High frequency values (> 5 Hz) are likely to induce significant heating: this shall be taken into account when evaluating the test results. The frequency of the load cycle shall be determined, before the test, with an accuracy of 1 %.

7.1.4 Cycle counter

The test machine shall be equipped with a cycle counter displaying the number of load cycles completed at any given time during the test.

7.2 Grips

Conventional grips for tensile testing (see ISO 527) are suitable for use with SENT specimens, provided they can accommodate these specimens, which are usually larger than standard tensile specimens.

Compact tensile (CT) specimens are loaded by two loading pins which pass through holes in the specimen (see Figure 2). The pin diameter shall be $0,250w \pm 0,005w$, where w is the effective specimen width. The pins shall be free to rotate in their holes during the test.

Careful alignment of the gripping fixtures and of the whole loading train shall be ensured to avoid out-of-plane displacements of the specimen.

7.3 Crack length measurement

7.3.1 General

Determination of the length of a razor-sharpened notch may be difficult on the unloaded specimens before testing. The initial crack length a_0 shall therefore be measured after completion of the test, on the newly created fracture surfaces. Different surface textures usually allow a clear distinction to be made between the razor-sharpened notch and the fatigue crack initiated from the notch. Any visual technique may be used for this measurement, provided a resolution of at least 0,1 mm or $0,002w$ (whichever represents the better resolution) is obtained.

Use the a_0 value thus obtained to correct the initial fatigue crack length reading recorded at the beginning of the test (see below).

If measurement of the razor-sharpened notch length is not possible on the fracture surfaces, take the first fatigue crack length reading recorded after the beginning of the test, but before any measurable increase in crack length, as the initial crack length a_0 .

All fatigue crack length measurements made during the test shall be made with a resolution of at least 0,1 mm or $0,002w$, whichever represents the better resolution. Take crack length readings at fixed crack length increments Δa . The minimum increment $\Delta a_{\min}$ shall be greater than 0,5 mm or five times the crack length measurement resolution, whichever is greater. Make at least 20 crack length measurements between the initial crack length a_0 and the final crack length at the end of the test a_f so that the maximum increment value $\Delta a_{\max}$ will be $\leq (a_f - a_0)/20$. If the above requirements cannot be satisfied (i.e. if $\Delta a_{\max} < \Delta a_{\min}$), the specimen dimensions are not suitable for this test and larger specimens will have to be employed.

At each crack length increment, also record the number of cycles N completed since the beginning of test.

Make all crack length measurements without interrupting the test, using one or more of the techniques specified in 7.3.2 to 7.3.5.

7.3.2 Travelling microscope

A low-power (approximately $\times 15$ to $\times 30$) travelling microscope can be used for crack length measurements. Record each crack length, and the corresponding reading of the number of cycles completed, in accordance with 7.3.1.

It is recommended that, prior to testing, reference marks be made on the specimen surface at precisely determined locations in the direction of cracking. Using such reference marks eliminates potential errors due to accidental movement of the travelling microscope.

If the specimen surface is marked, along the expected crack path, with a grid or scale complying with the resolution requirements given in 7.3.1, the crack length can then be determined directly with any magnifying device of suitable power.

Marks made on the specimen surface shall not affect crack initiation or propagation.

7.3.3 Video recording

The crack length can be monitored automatically during the test by means of a video camera equipped with a low-magnification (approximately $\times 15$ to $\times 30$) lens and connected to a video recorder.

The video recorder shall be synchronized with the cycle counter of the test machine (7.1.4) in order that the number of completed load cycles corresponding to each recorded image can be determined.

When using the video recording technique, accurate calibration of the scale used to read the crack length off the recorded video images shall be carried out before the test in order to ensure that the resolution requirements of 7.3.1 are fulfilled.

Alternatively, the specimen surface may be marked, along the expected crack path, with a grid or scale complying with the resolution requirements given in 7.3.1, allowing the crack length to be read directly from the recorded video images.

Marks made on the specimen surface shall not affect crack initiation or propagation.

7.3.4 Specimen compliance

When using the CT specimen, crack length can be measured by monitoring the specimen compliance.

Specimen compliance is defined as the slope of the linear plot of displacement V versus the load P applied during a load cycle. This can be determined simply by monitoring the peak value of the displacement, on account of the fact that the peak load is constant during the test. Such a procedure may, however, lead to an incorrect value of the specimen compliance due to non-linearities in the load-displacement curve. A more accurate value is obtained by recording the load and displacement signals within a single loading cycle in sufficient detail to recognize possible non-linear portions of the curve and to exclude them from a linear fit. If this procedure is used, it is recommended that either the loading or the unloading portion of the load cycle be consistently used for calculations throughout the test.

After measuring V and P , the normalized compliance C_N is obtained from the following equation:

$$C_N = \frac{h \times E \times V}{P} \quad (2)$$

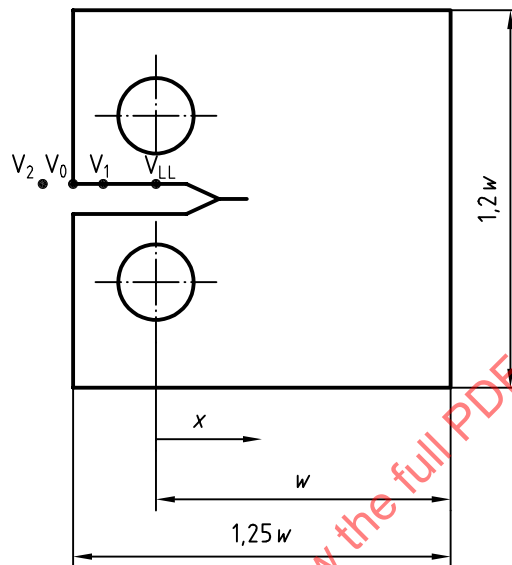
where

h is the specimen thickness;

E is the modulus of elasticity measured in accordance with the relevant part of ISO 527.

The modulus of elasticity of plastic specimens can be affected by processing-induced anisotropy. It is therefore recommended that tensile specimens for modulus determination be as similar as possible, with respect to the processing conditions and specimen orientation, to the fatigue specimens. Usually fatigue specimens are machined out of sheets or flat moulded parts: tensile specimens can then be machined from the same piece, taking care that the orientation is the same (the longitudinal axis of the tensile specimen has to be parallel to the line joining the two loading-pin holes in the CT specimen).

Four different locations shall be used to measure the displacement in the CT specimen. These are defined in Figure 4.



Key

x	Distance from load line (measured away from front face of specimen)
V_{LL}	Load-line compliance $x/w = 0$
V_1	Compliance at location 1 $x/w = -0,157 6$
V_0	Compliance at front face of specimen $x/w = -0,25$
V_2	Compliance at location 2 $x/w = -0,345$

Figure 4 — Locations for measurement of compliance of CT specimens

Selection of displacement measurement gauges, attachment points and methods of attachment are dependent on the test conditions and on the material to be tested. The gauges used shall have a linear response over the range of displacements to be measured, and shall have adequate resolution and a sufficiently short response time. It shall be possible for the attachment points to be accurately and repeatedly placed on the specimen, and they shall not be liable to wear during the fatigue cycling.

A polynomial expression describing the normalized crack length a/w as a function of the normalized compliance of the CT specimen, measured at the locations defined in Figure 4, has been established for metallic materials and has been proved to be valid for polymeric materials as well:

$$a/w = C_0 + C_1 U_x + C_2 (U_x)^2 + C_3 (U_x)^3 + C_4 (U_x)^4 + C_5 (U_x)^5 \quad (3)$$

where

$$U_x = \frac{1}{\left(\frac{h \times E \times V_x}{P} \right)^{1/2} + 1} \quad (4)$$

the coefficients $C_0, C_1, \dots, C_5$ take the values given in Table 1 at the four measurement locations:

Table 1

Measurement location	C_0	C_1	C_2	C_3	C_4	C_5
V_2	1,001 2	−4,916 5	23,057	−323,91	1 798,3	−3 513,2
V_0	1,001 0	−4,669 5	18,460	−236,82	1 214,9	−2 143,6
V_1	1,000 8	−4,447 3	15,400	−180,55	870,92	−1 411,3
V_{LL}	1,000 2	−4,063 2	11,242	−106,04	464,33	−650,68

The number of compliance measurements performed during the test and their spacing in time shall ensure that the crack length measurement requirements given in 7.3.1 are satisfied. The compliance method of crack length measurement lends itself to automatic data acquisition, and a large number of readings is commonly obtained.

At least two visual crack length readings shall be taken, at crack-tip positions at least $0,2w$ apart, during the test. Correct these visual readings for curvature, using the procedure outlined in 9.2, to obtain the actual crack lengths. Use any difference between the actual and compliance crack lengths to adjust all the compliance crack lengths. This is accomplished by calculating an effective modulus of elasticity E^* and using this in equation (4) to correct all the crack length calculations. If the effective modulus E^* differs from the modulus of elasticity E by more than 20 %, then the test equipment is improperly set up and data generated by this method are invalid.

At present, the specimen compliance method is not recommended for use with SENT specimens.

7.3.5 Crack gauges

Crack gauges for crack growth measurement are commercially available and commonly used in fatigue testing. They generally consist of thin, electrically conductive foils which are bonded to the specimen surface over the expected crack path and which are progressively split into two parts as the crack propagates. The electrical resistivity measured across the crack path changes from a minimum value corresponding to the uncracked foil to increasingly greater values as the crack grows. The electrical resistance can thus be used as an indirect measure of the crack length.

The adhesive used to bond the crack gauge to the specimen surface shall ensure that the length of the crack in the crack gauge is exactly equal to the length of the crack in the specimen surface. The adhesive shall not affect the fatigue response of the specimen.

Calibration of crack gauges shall be performed by taking at least two visual crack length readings at crack-tip positions at least $0,2w$ apart.

7.4 Test atmosphere

Conduct the test in the same atmosphere as used for conditioning, unless otherwise agreed upon by the interested parties, e.g. for testing at elevated or low temperatures. As the test duration may be long, particular attention shall be given to the constancy of the various parameters characterizing the test atmosphere (temperature, humidity, etc.).