
**Ships and marine technology —
Marine evacuation systems — Load
calculations and testing**

*Navires et technologie maritime — Systèmes d'évacuation en mer —
Calculs de charge et essais*

STANDARDSISO.COM : Click to view the full PDF of ISO 16706:2016



STANDARDSISO.COM : Click to view the full PDF of ISO 16706:2016



COPYRIGHT PROTECTED DOCUMENT

© ISO 2016, Published in Switzerland

All rights reserved. Unless otherwise specified, no part of this publication may be reproduced or utilized otherwise in any form or by any means, electronic or mechanical, including photocopying, or posting on the internet or an intranet, without prior written permission. Permission can be requested from either ISO at the address below or ISO's member body in the country of the requester.

ISO copyright office
Ch. de Blandonnet 8 • CP 401
CH-1214 Vernier, Geneva, Switzerland
Tel. +41 22 749 01 11
Fax +41 22 749 09 47
copyright@iso.org
www.iso.org

Contents

	Page
Foreword	iv
Introduction	v
1 Scope	1
2 Normative references	1
3 Terms and definitions	1
4 Load calculations	2
4.1 Load calculation	2
4.2 Additional loads	2
4.3 Load distribution	2
5 Load testing	2
5.1 Static load testing	2
5.2 Load test acceptance criteria	2
Annex A (normative) Calculation method of maximum load	3
Bibliography	7

Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

The procedures used to develop this document and those intended for its further maintenance are described in the ISO/IEC Directives, Part 1. In particular the different approval criteria needed for the different types of ISO documents should be noted. This document was drafted in accordance with the editorial rules of the ISO/IEC Directives, Part 2 (see www.iso.org/directives).

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. ISO shall not be held responsible for identifying any or all such patent rights. Details of any patent rights identified during the development of the document will be in the Introduction and/or on the ISO list of patent declarations received (see www.iso.org/patents).

Any trade name used in this document is information given for the convenience of users and does not constitute an endorsement.

For an explanation on the meaning of ISO specific terms and expressions related to conformity assessment, as well as information about ISO's adherence to the World Trade Organization (WTO) principles in the Technical Barriers to Trade (TBT) see the following URL: www.iso.org/iso/foreword.html.

The committee responsible for this document is ISO/TC 8, *Ships and marine technology*, Subcommittee SC 1, *Lifesaving and fire protection*.

Introduction

The International Convention for the Safety of Life at Sea (SOLAS), 1974 requires all life-saving appliances and arrangements to comply with the requirements of the LSA Code and to be tested in accordance with the recommendations of the IMO. The revised recommendation on testing of life-saving appliances, as adopted by IMO Resolution MSC.81(70), prescribes in paragraph 12.2.2 and 12.3.2.2 the execution of a static load test to the structural attachment to the ship of a marine evacuation system. However, this resolution does not refer to any specific calculation method for this test. This document is intended to provide specifications for an appropriate calculation method for this test in order to facilitate consistent implementation by maritime administrations when approving marine evacuation systems.

STANDARDSISO.COM : Click to view the full PDF of ISO 16706:2016

STANDARDSISO.COM : Click to view the full PDF of ISO 16706:2016

Ships and marine technology — Marine evacuation systems — Load calculations and testing

1 Scope

This document specifies a calculation method for the application of a static load test to the structural attachment of marine evacuation systems to ships.

2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

International Maritime Organization, *The International Convention for the Safety of Life at Sea (SOLAS)*, 1974, as amended

International Maritime Organization, *The International Life-Saving Appliance (LSA) Code*, as adopted by IMO Resolution MSC 48(66) as amended

International Maritime Organization, *The Revised recommendation on testing of life-saving appliances*, as adopted by IMO Resolution MSC.81(70) as amended

International Maritime Organization, *International Code on Intact Stability, 2008 (2008 IS Code)*, as adopted by IMO Resolution MSC.267(85) as amended

3 Terms and definitions

For the purposes of this document, the following terms and definitions apply.

ISO and IEC maintain terminological databases for use in standardization at the following addresses:

- IEC Electropedia: available at <http://www.electropedia.org/>
- ISO Online browsing platform: available at <http://www.iso.org/obp>

3.1 marine evacuation system MES

appliance for the rapid transfer of persons from the embarkation deck of a ship to a *floating platform* (3.3) or survival craft by means of a *passage* (3.2)

3.2 passage

integral component of a *marine evacuation system* (3.1) to provide safe descent of persons from the embarkation station to the *floating platform* (3.3) or survival craft

Note 1 to entry: The passage can be an inflatable or rigid slide, a vertical passage or any other arrangement providing the same function.

3.3 floating platform

inflatable structure which may be fitted to the bottom of the *passage* (3.2) to hold evacuees awaiting entry to survival craft

3.4

stowage container

arrangement providing means for stowing a *marine evacuation system* (3.1) and so constructed as to withstand heavy conditions encountered at sea

3.5

structural attachment

attachment of a *marine evacuation system* (3.1) to the ship structure designed to withstand loads calculated in accordance with this document

Note 1 to entry: Such attachments may include blocks, falls, pad eyes, links, fastenings and all other fittings used for restraining the *floating platform* (3.3), if fitted, and survival craft(s) to the ships side during evacuation.

4 Load calculations

4.1 Load calculation

The load imposed by the maximum number and size of fully loaded liferafts for which the system is designed, attached to the loaded floating platform, if fitted, with the ship moving through the water at 3 kn against a head wind of force 10 on the Beaufort scale shall be calculated in accordance with the method in [Annex A](#).

4.2 Additional loads

Where significant gravitational and moment loads of the passage, floating platform, if fitted, or survival craft(s) are imposed to the structural attachments in the fully deployed condition of the marine evacuation system, these loads shall be added when performing the static load tests required.

4.3 Load distribution

Where the loads calculated in [4.1](#) and [4.2](#) are shared by more than one structural attachment, the calculated load for load testing of individual structural attachments may be reduced, taking into consideration the distribution of loads in the scenario described in [4.1](#).

5 Load testing

5.1 Static load testing

All structural attachments of the MES shall be subjected to a static load of 2,2 times the maximum load calculated in accordance with [Clause 4](#). The load shall be applied to the structural attachments for a period of no less than 30 min and in the same direction as the load is applied during service. The structural attachments may be tested with or without the MES in place.

5.2 Load test acceptance criteria

On completion of this test, there shall be no evidence of significant deformation, signs of any fracture, stranding to its connections or any other damage as a result of this factory test.

Annex A (normative)

Calculation method of maximum load

A.1 Maximum calculated load formula

$$F = F_W + R \quad (\text{A.1})$$

where

F is the maximum calculated load (N);

F_W is the sum of wind forces on the slide or passage, floating platform and fully loaded liferafts with the maximum specification or quantity at a wind of force 10 on the Beaufort scale (N);

R is the drag on the floating platform and fully loaded liferafts with the maximum specification or quantity when they are dragged in water at a speed of 3 kn (N).

A.2 Calculation of wind force

A.2.1 General

The sum of wind forces, F_W , shall be calculated as the wind pressure, P , multiplied by the sum of exposed areas, A , of the marine evacuation system in the fully deployed condition.

$$F_W = P \cdot A \quad (\text{A.2})$$

where

P is the wind pressure;

A is the exposed area.

A.2.2 Wind pressure

As specified in the 2008 IS Code, the unit calculated wind pressure shall be taken as 504 N/m² as equivalent to the maximum wind speed of 28,4 m/s for a wind force of 10 on the Beaufort scale.

For the floating platform, if fitted, and survival craft(s) alternatively, the values of wind pressure may be taken from [Table A.1](#):

Table A.1 — Alternative wind pressures

6	h (m)	7	1	8	2	9	3	10	4	11	5	12	6 and over
13	P (N/m ²)	14	316	15	386	16	429	17	460	18	485	19	504
where h is the vertical distance from the centre of the projected vertical area of the floating platform and/or survival craft(s) above the waterline, to the waterline; P is the wind pressure associated with the height, h.													

A.2.3 Calculation of wind area

$$A = (A1 \cdot \alpha) + (A2 \cdot \beta) + (A3 \cdot \theta) + (A4 \cdot \theta) + (A5 \cdot \theta) \quad (\text{A.3})$$

where

A is the sum of the above wind areas (m^2);

$A1$ is the projected slide or passage area (aft) (m^2);

$A2$ is the projected area of the part of a floating platform above water (aft) (m^2);

$A3$ is the projected area of the part of a fully loaded liferaft above water (aft) (m^2);

$A4$ is the projected area of the part of the second fully loaded liferaft above water (m^2);

$A5$ is the projected area of the part of the third fully loaded liferaft above water (m^2);

α is the drag coefficient of the projected slide or passage area;

β is the drag coefficient of the projected area of the part of a floating platform above water;

θ is the drag coefficient of the projected area of the part of a full-load liferaft above water.

NOTE α, β, θ are generally taken as 0,8 to 1,0, dependent on different products.

A.3 Calculation of drag

A.3.1 General

The total drag, R , shall be calculated as follows:

$$R = R_p + R_f \quad (\text{A.4})$$

where

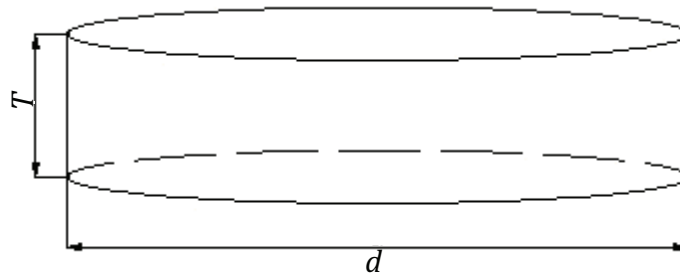
R_p is the pressure drag;

R_f is the friction drag.

A.3.2 Drag composition model

Based on the estimation formula of cylinder drag coefficient proposed by Kirkman,^[1] the drag on a round section liferaft with draught, T , and diameter, d , under the impact of flow at 90° angle of attack is analysed as follows.

- The drag mainly consists of pressure drag, R_p , which accounts for the majority, and friction drag, R_f .
- The part of a fully loaded liferaft below water is simplified as the model in [Figure A.1](#).

**Key**

d maximum diameter of a floating platform or liferaft

T draught of a fully loaded liferaft

Figure A.1 — Composition of drag — simplified model

A.3.3 Reynolds number

Reynolds number, Rn , shall be calculated as:

$$Rn = \frac{v}{\nu} \cdot d \quad (\text{A.5})$$

where

v is the relative flow velocity of 3 kn equal to 1,543 m/s;

ν is the dynamic viscosity equal to $1,1892 \times 10^{-6} \text{ m}^2/\text{s}$ at 15 °C; [2]

$$Rn = \frac{1,543 \text{ m/s}}{1,1892 \cdot 10^{-6} \text{ m}^2/\text{s}} \cdot d \approx 1,3 \cdot 10^6 \text{ m}^{-1} \cdot d.$$

A.3.4 Pressure drag

Pressure drag, R_p , shall be calculated as:

$$R_p = A \cdot C_p \cdot \frac{1}{2} \cdot \rho \cdot v^2 \quad (\text{A.6})$$

where

A is the projected area, i.e. $A = T \cdot d$;

T is the draught of a fully loaded liferaft;

ρ is the density of the seawater equal to $1,03 \times 10^3 \text{ kg/m}^3$;

C_p is the pressure drag coefficient equal to 0,60.

For values of d within the range of liferaft dimensions, Reynolds number $> 5 \times 10^5$, for which the pressure drag coefficient, C_p , may be estimated as $C_p = 0,60$ according to the Kirkman [1] estimation.