

---

---

**Statistical methods in process  
management — Capability and  
performance —**

**Part 4:  
Process capability estimates and  
performance measures**

*Méthodes statistiques dans la gestion de processus — Aptitude et  
performance —*

*Partie 4: Estimations de l'aptitude de processus et mesures de  
performance*



STANDARDSISO.COM : Click to view the full PDF of ISO 22514-4:2016



**COPYRIGHT PROTECTED DOCUMENT**

© ISO 2016, Published in Switzerland

All rights reserved. Unless otherwise specified, no part of this publication may be reproduced or utilized otherwise in any form or by any means, electronic or mechanical, including photocopying, or posting on the internet or an intranet, without prior written permission. Permission can be requested from either ISO at the address below or ISO's member body in the country of the requester.

ISO copyright office  
Ch. de Blandonnet 8 • CP 401  
CH-1214 Vernier, Geneva, Switzerland  
Tel. +41 22 749 01 11  
Fax +41 22 749 09 47  
copyright@iso.org  
www.iso.org

# Contents

Page

|                                                                                                       |           |
|-------------------------------------------------------------------------------------------------------|-----------|
| <b>Foreword</b>                                                                                       | <b>v</b>  |
| <b>Introduction</b>                                                                                   | <b>vi</b> |
| <b>1 Scope</b>                                                                                        | <b>1</b>  |
| <b>2 Symbols and abbreviated terms</b>                                                                | <b>1</b>  |
| 2.1 Symbols                                                                                           | 1         |
| 2.2 Abbreviated terms                                                                                 | 3         |
| <b>3 Basic concepts used for process capability and performance</b>                                   | <b>3</b>  |
| 3.1 General                                                                                           | 3         |
| 3.2 Location                                                                                          | 3         |
| 3.3 Dispersion                                                                                        | 3         |
| 3.3.1 Inherent dispersion                                                                             | 3         |
| 3.3.2 Total dispersion                                                                                | 3         |
| 3.3.3 Short-term dispersion                                                                           | 3         |
| 3.4 Mean square error (MSE)                                                                           | 4         |
| 3.5 Reference limits                                                                                  | 4         |
| 3.6 Reference interval (also known as process spread)                                                 | 4         |
| <b>4 Capability</b>                                                                                   | <b>4</b>  |
| 4.1 General                                                                                           | 4         |
| 4.2 Process capability                                                                                | 6         |
| 4.2.1 Normal distribution                                                                             | 6         |
| 4.2.2 Non-normal distribution                                                                         | 7         |
| 4.3 Process location                                                                                  | 7         |
| 4.4 Process capability indices for measured data                                                      | 8         |
| 4.4.1 General                                                                                         | 8         |
| 4.4.2 $C_p$ index (for the normal distribution)                                                       | 9         |
| 4.4.3 $C_{pk}$ index (for the normal distribution)                                                    | 10        |
| 4.4.4 $C_{pk}$ index for unilateral tolerances                                                        | 10        |
| 4.5 Process capability indices for measured data (non-normal)                                         | 10        |
| 4.5.1 General                                                                                         | 10        |
| 4.5.2 Probability paper method                                                                        | 11        |
| 4.5.3 Pearson curves method                                                                           | 11        |
| 4.5.4 Distribution identification method                                                              | 12        |
| 4.6 Alternative method for describing and calculating process capability estimates                    | 12        |
| 4.7 Other capability measures for continuous data                                                     | 13        |
| 4.7.1 Process capability fraction (PCF)                                                               | 13        |
| 4.7.2 Indices when the specification limit is one-sided or no specification limit is given            | 13        |
| 4.8 Assessment of proportion out-of-specification (normal distribution)                               | 15        |
| <b>5 Performance</b>                                                                                  | <b>16</b> |
| 5.1 General                                                                                           | 16        |
| 5.2 Process performance indices for measured data (normal distribution)                               | 16        |
| 5.2.1 $P_p$ index                                                                                     | 16        |
| 5.2.2 $P_{pk}$ index                                                                                  | 17        |
| 5.3 Process performance indices for measured data (non-normal distribution)                           | 17        |
| 5.3.1 General                                                                                         | 17        |
| 5.3.2 Probability paper method                                                                        | 17        |
| 5.3.3 Pearson curves method                                                                           | 18        |
| 5.3.4 Distribution identification method                                                              | 18        |
| 5.4 Other performance indices for measured data                                                       | 18        |
| 5.5 Assessment of proportion out-of-specification for a normal distribution of the total distribution | 18        |
| <b>6 Reporting process capability and performance indices</b>                                         | <b>19</b> |

|                                                                                                                          |           |
|--------------------------------------------------------------------------------------------------------------------------|-----------|
| <b>Annex A (informative) Estimating standard deviations</b>                                                              | <b>21</b> |
| <b>Annex B (informative) Estimating capability and performance measures using Pearson curves — Procedure and example</b> | <b>23</b> |
| <b>Annex C (informative) Distribution identification</b>                                                                 | <b>37</b> |
| <b>Annex D (informative) Confidence intervals</b>                                                                        | <b>42</b> |
| <b>Bibliography</b>                                                                                                      | <b>44</b> |

STANDARDSISO.COM : Click to view the full PDF of ISO 22514-4:2016

## Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

The procedures used to develop this document and those intended for its further maintenance are described in the ISO/IEC Directives, Part 1. In particular the different approval criteria needed for the different types of ISO documents should be noted. This document was drafted in accordance with the editorial rules of the ISO/IEC Directives, Part 2 (see [www.iso.org/directives](http://www.iso.org/directives)).

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. ISO shall not be held responsible for identifying any or all such patent rights. Details of any patent rights identified during the development of the document will be in the Introduction and/or on the ISO list of patent declarations received (see [www.iso.org/patents](http://www.iso.org/patents)).

Any trade name used in this document is information given for the convenience of users and does not constitute an endorsement.

For an explanation on the meaning of ISO specific terms and expressions related to conformity assessment, as well as information about ISO's adherence to the WTO principles in the Technical Barriers to Trade (TBT) see the following URL: [Foreword - Supplementary information](#).

The committee responsible for this document is Technical Committee ISO/TC 69, *Applications of statistical methods*, Subcommittee SC 4, *Applications of statistical methods in process management*.

This first edition of ISO 22514-4 cancels and replaces ISO/TR 22514-4:2007, which has been technically revised.

ISO 22514 consists of the following parts, under the general title *Statistical methods in process management — Capability and performance*:

- *Part 1: General principles and concepts*
- *Part 2: Process capability and performance of time-dependent process models*
- *Part 3: Machine performance studies for measured data on discrete parts*
- *Part 4: Process capability estimates and performance measures*
- *Part 5: Process capability estimates and performance for attributive characteristics*
- *Part 6: Process capability statistics for characteristics following a multivariate normal distribution*
- *Part 7: Capability of measurement processes*
- *Part 8: Machine performance of a multi-state production process*

## Introduction

Many organizations have embarked upon a continuous improvement strategy. To comply with such a strategy, any organization will need to evaluate the capability and performance of its key processes. The methods described in this part of ISO 22514 are intended to assist any management in this respect. These evaluations need to be constantly reviewed by the management so that actions compatible with continuous improvement can be taken when required.

The content of this part of ISO 22514 has been subject to large shifts of opinion during recent times. The most fundamental shift has been to philosophically separate what is named in this part of ISO 22514 as capability conditions from performance conditions, the primary difference being whether statistical stability has been obtained (capability) or not (performance). This naturally leads onto the two sets of indices that are to be found in their relevant clauses. It has become necessary to draw a firm distinction between these since it has been observed in the industry that companies have been deceived about their true capability position due to inappropriate indices being calculated and published.

The progression of this part of ISO 22514 is from the general condition to the specific and this approach leads to general formulae being presented before their more usual, but specific manifestations.

There exist numerous references that describe the importance of understanding the processes at work within any organization, be it a manufacturing process or an information handling process. As organizations compete for sales with each other, it has become increasingly apparent that it is not only the price paid for a product or service that matters so much, but also what costs will be incurred by the purchaser from using such a product or service. The objective for any supplier is to continually reduce variability and not to just satisfy specification.

Continual improvement leads to reductions in the costs of failure and assists in the drive for survival in an increasingly more competitive world. There will also be savings in appraisal costs for as variation is reduced, the need to inspect product might disappear or the frequency of sampling might be reduced.

Process capability and performance evaluations are necessary to enable organizations to assess the capability and performance of their suppliers. Those organizations will find the indices contained within this part of ISO 22514 useful in this endeavour.

Quantifying the variation present within a process enables judgement of its suitability and ability to meet some given requirement. The following paragraphs and clauses provide an outline of the philosophy required to be understood to determine the capability or performance of any process.

All processes will be subject to certain inherent variability. This part of ISO 22514 does not attempt to explain what is meant by inherent variation, why it exists, where it comes from nor how it affects a process. This part of ISO 22514 starts from the premise that it exists and is stable.

Process owners should endeavour to understand the sources of variation in their processes. Methods such as flowcharting the process and identifying the inputs and outputs from a process assist in identification of these variations together with the appropriate use of cause and effect (fishbone) diagrams.

It is important for the user of this part of ISO 22514 to appreciate that variations exist that will be of a short-term nature, as well as those that will be of a long-term nature and that capability determinations using only the short-term variation might be greatly different to those which have used the long-term variability.

When considering short-term variation, a study that uses only the shortest-term variation, sometimes known as a machine study and described in ISO 22514-3, might be carried out. The method required to carry out such a study will be outside the scope of this part of ISO 22514; however, it should be noted that such studies are important and useful.

It should be noted that where the capability indices given in this part of ISO 22514 are computed, they only form point estimates of their true values. It is therefore recommended that, wherever possible, the

indices' confidence intervals are computed and reported. This part of ISO 22514 describes methods by which these can be computed.

STANDARDSISO.COM : Click to view the full PDF of ISO 22514-4:2016

STANDARDSISO.COM : Click to view the full PDF of ISO 22514-4:2016

# Statistical methods in process management — Capability and performance —

## Part 4: Process capability estimates and performance measures

### 1 Scope

This part of ISO 22514 describes process capability and performance measures that are commonly used.

### 2 Symbols and abbreviated terms

#### 2.1 Symbols

In addition to the symbols listed below, some symbols are defined where they are used within the text.

|            |                                                                                 |
|------------|---------------------------------------------------------------------------------|
| $\alpha$   | fraction or proportion                                                          |
| $\beta$    | shape parameter in a Weibull distribution                                       |
| $\beta_2$  | coefficient of kurtosis                                                         |
| $c_4$      | constant based on subgroup size, $n$ (see ISO 7870-2)                           |
| $C_p$      | process capability index                                                        |
| $C_{pk}$   | minimum process capability index                                                |
| $C_{pk_L}$ | lower process capability index                                                  |
| $C_{pk_U}$ | upper process capability index                                                  |
| $C_{pm}$   | alternative process capability index                                            |
| $C_R$      | process capability fraction (PCF)                                               |
| $d_2$      | constant based on subgroup size, $n$ (see ISO 7870-2)                           |
| $e$        | Eulers's number (approximately 2,718), mathematical constant                    |
| $\Phi$     | distribution function of the standard normal distribution                       |
| $\gamma$   | location parameter in a Weibull distribution                                    |
| $\gamma_1$ | coefficient of skewness                                                         |
| $m$        | number of subgroups                                                             |
| $K_l, K_u$ | multipliers for estimating the confidence limits for a process capability index |
| $L$        | lower specification limit                                                       |

|                  |                                                                    |
|------------------|--------------------------------------------------------------------|
| $P_{0,135} \%$   | lower 0,135 % percentile                                           |
| $\mu$            | location of the process; population mean value                     |
| $N$              | total sample size                                                  |
| $n$              | number of values or subgroup size (for a control chart)            |
| $P_{\alpha} \%$  | $\alpha$ percentile                                                |
| $p_L$            | lower fraction nonconforming                                       |
| $P_p$            | process performance index                                          |
| $P_{pk}$         | minimum process performance index                                  |
| $P_{pk_L}$       | lower process performance index                                    |
| $P_{pk_U}$       | upper process performance index                                    |
| $p_t$            | total fraction nonconforming                                       |
| $p_U$            | upper fraction nonconforming                                       |
| $P_{99,865} \%$  | upper 99,865 % percentile                                          |
| $\pi$            | geometric constant                                                 |
| $Q_k$            | process variation index                                            |
| $\theta$         | parameter required for the Rayleigh distribution                   |
| $\bar{R}$        | average subgroup range                                             |
| $S$              | standard deviation, sample statistic                               |
| $S_t$            | standard deviation, with the subscript 't' indicating total        |
| $\bar{S}$        | average sample standard deviation                                  |
| $S_j$            | observed sample standard deviation of the $j^{\text{th}}$ subgroup |
| $\sigma$         | standard deviation, population                                     |
| $\hat{\sigma}_t$ | estimated standard deviation, total                                |
| $T$              | target value                                                       |
| $U$              | upper specification limit                                          |
| $X_{\alpha} \%$  | $\alpha$ % percentile                                              |
| $X_i$            | $i^{\text{th}}$ value in a sample                                  |
| $\bar{X}$        | arithmetic mean value, sample                                      |
| $\bar{\bar{X}}$  | arithmetic mean, of a number of sample arithmetic means            |

|            |                                                                             |
|------------|-----------------------------------------------------------------------------|
| $\xi$      | scale parameter in a Weibull distribution                                   |
| $Y_1, Y_2$ | values read from a graph                                                    |
| $z_\alpha$ | quantile of the standardized normal distribution from $-\infty$ to $\alpha$ |

## 2.2 Abbreviated terms

|     |                             |
|-----|-----------------------------|
| MSE | mean square error           |
| PCF | process capability fraction |
| PCI | process capability index    |

## 3 Basic concepts used for process capability and performance

### 3.1 General

The measures referred to in [4.2](#) to [4.6](#) refer only to measured data. They are unsuitable for count or attributes data and information concerning the expression of measures for such data will be found in ISO 22514-5.

### 3.2 Location

The characterization of location is the mean,  $\mu$ , or the median,  $X_{50} \%$ . Although for symmetric distributions the mean is the most natural selection, with non-symmetric distributions the median is the preferred selection.

### 3.3 Dispersion

#### 3.3.1 Inherent dispersion

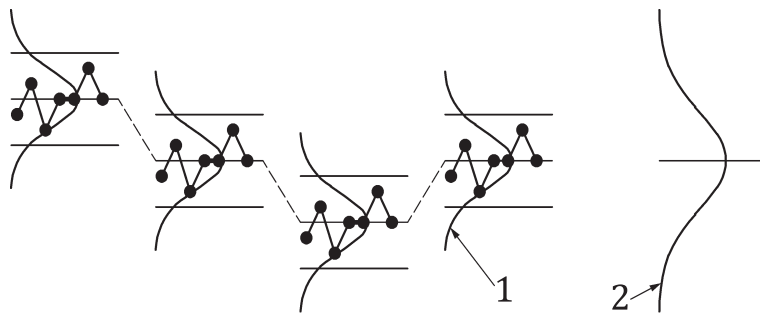
The preferred selection to quantify inherent dispersion is the standard deviation  $\sigma$ . This is often estimated from the mean range value,  $\bar{R}$ , taken from a range ( $R$ ) chart or  $\bar{S}$  from a standard deviation ( $S$ ) chart when the process is stable and in a state of statistical control as indicated in [4.1](#). Methods used to estimate the process standard deviation are given in [Annex A](#).

#### 3.3.2 Total dispersion

It is necessary to differentiate between a standard deviation that measures only short-term variation and that which measures longer-term variation. The total dispersion is the dispersion that is inherent in the long-term variation. Methods of calculating the standard deviations representing these variations are given in [Annex A](#). Very often, when data are gathered over a long period of time, the standard deviation is made larger by the effects of fluctuations in the process,  $\sigma_t$ .

#### 3.3.3 Short-term dispersion

A process may have a short-term dispersion effect that is a part of the total dispersion. [Figure 1](#) illustrates this. The short-term dispersion includes the inherent dispersion and can also include some short-term instability effect.

**Key**

- 1 short-term dispersion
- 2 overall dispersion

**Figure 1 — Short-term dispersion and its relationship to the total dispersion**

The total dispersion can be any shape and not necessarily normal as illustrated here.

### 3.4 Mean square error (MSE)

When minimizing variation, some practitioners use the mean square error as the preferred measure. It is compatible with the methods used in off-line quality techniques.

### 3.5 Reference limits

The lower and upper reference limits are respectively defined as the 0,135 % and the 99,865 % percentiles of the distribution that describe the output of the process characteristic. They are written as  $X_{0,135\%}$  and  $X_{99,865\%}$ .

### 3.6 Reference interval (also known as process spread)

The reference interval is the interval between the upper and the lower reference limits. The reference interval includes 99,73 % of the individuals in the population from a process that is in a state of statistical control.

## 4 Capability

### 4.1 General

Process capability is a measure of inherent process variability. The variability that is inherent in a process when operating in a state of statistical control is known as the inherent process variability. It represents the variation that remains after all known removable *assignable causes* have been eliminated. If the process is monitored using a control chart, the control chart will show an *in control* state.

Capability is often regarded as being related to the proportion of output that will occur within the product specification tolerances. Since a process in statistical control should be described by a predictable distribution, the proportion of out-of-specification outputs can be estimated. As long as the process remains in statistical control, it will continue to produce the same proportion out-of-specification.

Management actions to reduce the variation from *random causes* are required to improve the process' ability to consistently meet the specification requirements.

In short, the following will be necessary:

- define the process and its operating conditions. If there is a change to those conditions, it will necessitate a new process study;
- assess the short-term and long-term measurement variabilities as percentages of the total variability and minimize them;
- preserve the process stability and maintain its statistical control;
- estimate the remaining inherent variation;
- select an appropriate measure of capability.

The following are the conditions that will apply for capability:

- all technical conditions, e.g. temperature and humidity, shall be clearly stated;
- the uncertainty of the measurement system shall be estimated and judged appropriate (see ISO 22514-7);
- multi-factor, multi-level aspects of the process should be allowed;
- the duration over which the data has been gathered shall be recorded;
- the frequency of sampling and sample size shall be specified and the start and finish dates of data collection;
- the process shall be controlled with a control chart;
- the process shall be in a state of statistical control.

It is necessary to check the control chart from which the data have been taken for statistical control and to examine a histogram of the data with any specification limits superimposed upon it. A valid test for normality should be used in assessing the data such as the Anderson-Darling test<sup>[15]</sup> or any other suitable method. This test is powerful in detecting departures from normality in the tails of the distribution and is suggested here as this is the region of interest for capability and performance indices. Additionally, a normal probability plot can be used to look for the following:

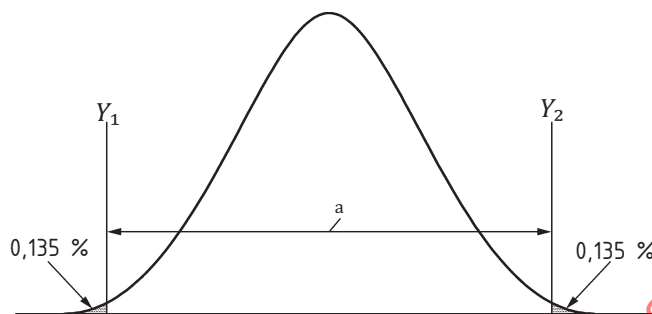
- a) verification of normality;
- b) outliers;
- c) data beyond any specification limit;
- d) whether the data are well inside the specification limit(s);
- e) evidence of asymmetry (i.e. skewness);
- f) evidence of “long tails” in the data (i.e. kurtosis);
- g) off-centre distribution;
- h) any unusual patterns.

Explanations of anomalies should be sought in relation to these mentioned features and appropriate action taken on the data prior to the calculation of any measure. It would be inappropriate to just discard data that do not appear to fit any preconceived pattern. Such departures might be very revealing about the process' behaviour and should be thoroughly investigated.

## 4.2 Process capability

### 4.2.1 Normal distribution

Process capability is defined as a statistical measure of inherent process variability for a given characteristic. The conventional method is to take the reference interval that describes 99,73 % of the individual values from a process that is in a state of statistical control with the 0,135 % remaining on each side. This applies even if the population of individual values is not normally distributed. For a normal distribution, this process interval is represented by six standard deviations (see [Figure 2](#)).



#### Key

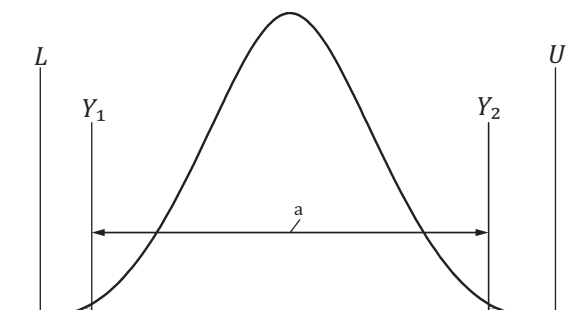
a Reference interval 99,73 %.

**Figure 2 — Normal distribution**

On occasions, process capability is taken to account for extra sources of variation such as a multiple stream process, for example, output from a multi-cavity injection moulding press. Under these circumstances, the distribution of all values from all cavities could still be approximately normal, but with extra variability so that the standard deviation shall represent the total variation,  $\sigma_t$ . It is important to state how the standard deviation has been calculated, as well as the sampling strategy used, sample size and the quantity and variability of output produced between samples as these will, in practice, affect the validity of the capability assessment (see ISO 22514-2 for further information).

Data will usually be taken from a control chart. If the control chart had relaxed control lines or modified control lines, the real process standard deviation will be larger than that estimated from data taken from a control chart with standard control lines. Issues such as these and those given earlier will influence the reference interval and it is important that they are stated in any capability assessment.

“Capable” processes will be those whose reference intervals are less than any specified tolerance by a particular amount. An example of this is shown in [Figure 3](#).



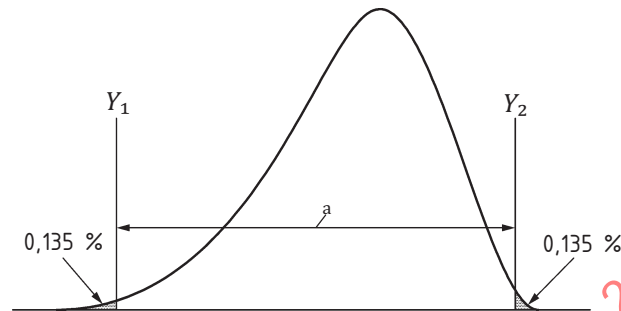
#### Key

a Reference interval 99,73 %.

**Figure 3 — Normal distribution with specification limits**

### 4.2.2 Non-normal distribution

If the distribution of individual values does not form a normal distribution, but is skewed, then the reference interval may appear as in [Figure 4](#). The values  $Y_1$  and  $Y_2$ , which will usually be the 0,135 % and the 99,865 % percentiles, can be estimated using a suitable probability paper (see [Figure 5](#) for an example using an extreme value distribution probability paper) or by the use of suitable computer software. They can also be computed using tabular values (see [Annex B](#)) or using the particular probability function as suggested in [Annex C](#).



**Key**

a Reference interval 99,73 %.

**Figure 4 — Non-normal distribution**

### 4.3 Process location

Even if a process can be deemed capable by the above definition (in [4.2.1](#)), if the process distribution has been poorly centred relative to the specification limits, out-of-specification items might be produced. For this reason, it is necessary to assess the location in addition to the process interval.



#### 4.4.1 General

It is effective to express the capability of a process with the use of an index number. Several indices are given. Care shall be taken when handling non-normal distributions.

The process capability index often used is the ratio of a specified tolerance to the reference interval and is known as  $C_p$ . Thus,

There are other indices that incorporate both the location and the variation. Of these, the most widely used is the  $C_{pk}$  index. If the observed index is less than a specified value, the process is deemed unacceptable and might lead to the shipment of a proportion of items outside of the specification or that function and fit might be compromised.

The  $C_{pk}$  index is the ratio of the difference between a specified tolerance limit and the process location to the difference between the corresponding natural process limit and the process location.

$$C_{pk_U} = \frac{U - X_{50\%}}{X_{99,865\%} - X_{50\%}} \quad (2)$$

and

$$C_{pk_L} = \frac{X_{50\%} - L}{X_{50\%} - X_{0,135\%}}$$

The  $C_{pk}$  index is reported as the smaller value of these.

NOTE Some practitioners report both of the above values (that are also known as CPU and CPL, respectively). This provides information about both sides of the process.

These indices will provide information about whether a process is poorly centred and whether it will possibly produce out-of-specification items. Even if the  $C_p$  index is high, a low value of the  $C_{pk}$  index will reveal a poorly centred process and a high probability of producing out-of-specification items.

#### 4.4.2 $C_p$ index (for the normal distribution)

If the individual values form a normal distribution and come from a statistically stable process, the length of the reference interval is equal to  $6\sigma$ , where  $\sigma$  is the inherent process standard deviation. Therefore, the  $C_p$  index can be expressed as:

$$C_p = \frac{U - L}{6\sigma}$$

An estimate ( $\hat{\sigma}$ ) of the inherent process standard deviation ( $\sigma$ ) is required to obtain an estimate of the  $C_p$  index. When this has been obtained, usually with data from a control chart once the process is shown to be statistically stable (see 4.1), the index is estimated:

$$\hat{C}_p = \frac{U - L}{6\hat{\sigma}}$$

#### 4.4.3 $C_{pk}$ index (for the normal distribution)

When the distribution of individual values forms a normal distribution, the median  $X_{50\%}$  is equal to the mean ( $\mu$ ). Further,  $X_{99,865\%} - X_{50\%}$  and  $X_{50\%} - X_{0,135\%}$  are each equal to  $3\sigma$ . Therefore, the  $C_{pk}$  index can be expressed as the minimum of:

$$C_{pk_U} = \frac{U - \mu}{3\sigma}$$

or

$$C_{pk_L} = \frac{\mu - L}{3\sigma}$$

The estimated  $C_{pk}$ , (using  $\bar{\bar{X}}$  to estimate  $\mu$  instead of  $X_{50\%}$ ) will be the minimum of:

$$\hat{C}_{pk_U} = \frac{U - \bar{\bar{X}}}{3\hat{\sigma}}$$

or

$$\hat{C}_{pk_L} = \frac{\bar{\bar{X}} - L}{3\hat{\sigma}}$$

In computing a capability index, thought has to be given to the measure of the process variation used in the denominator. Here,  $\sigma$  is given to represent the variation when the data comes from a process that is in a state of statistical control.

The data might come from a multiple stream process such as a multi-headed filling machine or a multi-spindle machine where the total output is treated together, where data from all streams are simultaneously considered. The lower the index, the greater the proportion of items produced out-of-specification.

#### 4.4.4 $C_{pk}$ index for unilateral tolerances

When there is only one specification limit given, it is only possible to calculate a  $C_{pk}$  index. The index will be calculated using the appropriate limit, either an  $L$  or a  $U$ .

### 4.5 Process capability indices for measured data (non-normal)

#### 4.5.1 General

If the distribution of individual values is non-normal, the expressions in [Formulae \(1\)](#) and [\(2\)](#) still apply, but the estimation of the indices becomes more complicated. Three approaches to estimate the reference limits are given.

The probability paper method described in [4.5.2](#) is fairly simple and requires little computation, but is somewhat crude. The approach given in [4.5.4](#) is computationally more involved, but is superior to any other method as far as accuracy is concerned.

#### 4.5.2 Probability paper method

From graphs similar to that shown in [Figure 4](#), estimates of the percentiles  $X_{0,135\%}$  and  $X_{99,865\%}$  can be obtained. The estimates are denoted by  $Y_1$  and  $Y_2$ , respectively, and [Formula \(1\)](#) becomes:

$$\hat{C}_p = \frac{U - L}{Y_2 - Y_1}$$

In a similar way, the  $C_{pk}$  formulae become:

$$\hat{C}_{pk_U} = \frac{U - X_{50\%}}{Y_2 - X_{50\%}}$$

or

$$\hat{C}_{pk_L} = \frac{X_{50\%} - L}{X_{50\%} - Y_1}$$

whichever gives the lower value.

If the observed index is less than a specified value, the process is deemed unacceptable and might lead to the shipment of a proportion of items outside of the specification or that function and fit might be compromised. The proportion nonconforming depends upon the distribution and the value of the index. The link between the index and the proportion of nonconforming items produced depends on the class of distributions. Care should be taken not to interpret indices on the basis of cut-off points that have been derived for the normal distribution and, hence, are only applicable for that distribution.

Note that the probability paper method directly estimates fairly extreme percentiles and this can be inaccurate.

#### 4.5.3 Pearson curves method

As an alternative to using probability paper, standardized Pearson curves can be used. The method is described by way of an example (see [Annex B](#)). The index is computed using:

$$\hat{C}_p = \frac{U - L}{\hat{X}_{99,865\%} - \hat{X}_{0,135\%}}$$

where  $\hat{X}_{0,135\%}$  and  $\hat{X}_{99,865\%}$  are the 0,135 % and 99,865 % percentiles estimated from the standardized Pearson curves.

Also, we have the formulae:

$$\hat{C}_{pk_U} = \frac{U - \hat{X}_{50\%}}{\hat{X}_{99,865\%} - \hat{X}_{50\%}}$$

or

$$\hat{C}_{pk_L} = \frac{\hat{X}_{50\%} - L}{\hat{X}_{50\%} - \hat{X}_{0,135\%}}$$

where  $\hat{X}_{50\%}$  is the estimated median.

In order to use this method, it is necessary to establish skewness and kurtosis values in addition to the mean and standard deviation for the data set upon which the index is to be computed.

This method is not preferred, but is presented here for completeness due to its occasional use.

This approach, and a similar one based on Johnson curves, should be regarded with considerable caution, especially when it is a procedure within a “black box” computer program used to analyse large sets of data. Some of the potential difficulties are as follows:

- within a system of distributions, some distributions are more difficult to fit than others. The method of moments can yield unstable or inefficient curve parameters in some cases;
- unless the estimation technique is applied skilfully, it is possible to obtain fitted curves that are meaningless over certain ranges of the data. For example, with the method of moments, an easily made mistake is to fit a Pearson Type III distribution whose estimated threshold is less than the lower bound for the process output, thereby, invalidating the estimates of  $X_{0,135\%}$  and  $C_{pk}$ ;
- the method of moments does not yield estimates of the variability in the estimated indices. Likewise, these methods do not yield confidence intervals for the indices;
- not every data distribution can be described adequately with a Pearson or Johnson curve;
- goodness-of-fit tests are limited to the chi-squared test since more powerful tests are not generally available for the Pearson and Johnson systems;
- the “black box” approach tends to displace basic practices, such as plotting the data and applying simple normalizing transformations, that provide genuine understanding of the process.

#### 4.5.4 Distribution identification method

[Annex C](#) describes certain families of distribution functions (such as the log-normal distribution, the Rayleigh and the Weibull distributions) that are commonly found when investigating process capability. The method is first to identify the appropriate family of distributions, secondly to estimate the parameters of the distribution of the family that best explain the data by some efficient estimation method and, finally, to express the quantiles in terms of the parameters of that distribution.

This is analogous to the procedure adopted in the case of the normal distribution where  $\sigma$  is estimated and  $6\sigma$  is represented by  $(X_{99,865\%} - X_{0,135\%})$ .

Various types of probability paper might be useful to identify the appropriate family of distributions.

#### 4.6 Alternative method for describing and calculating process capability estimates

The bases for this method are the widely used definitions of  $C_p$  and  $C_{pk}$  for the “ideal process” with a normally distributed characteristic,  $X$ , where the expectation,  $\mu$ , and variance,  $\sigma^2$ , are constant with time and the corresponding estimates are  $\bar{X}$  and  $S^2$ .

**Table 1 — Process capability indices and estimates for the normal distribution**

| Index                                | Estimate                                              |
|--------------------------------------|-------------------------------------------------------|
| $C_p = \frac{U - L}{6\sigma}$        | $\hat{C}_p = \frac{U - L}{6S}$                        |
| $C_{pk_U} = \frac{U - \mu}{3\sigma}$ | $\hat{C}_{pk_U} = \frac{U - \bar{X}}{3S}$             |
| $C_{pk_L} = \frac{\mu - L}{3\sigma}$ | $\hat{C}_{pk_L} = \frac{\bar{X} - L}{3S}$             |
| $C_{pk} = \min(C_{pk_L}, C_{pk_U})$  | $\hat{C}_{pk} = \min(\hat{C}_{pk_L}, \hat{C}_{pk_U})$ |

This “ideal process” implies that the long-term standard deviation is equal to the short-term standard deviation.

For the normal distribution, there is an exact relation between the lower fraction nonconforming units and  $C_{pk_L}$  and between the upper fraction nonconforming and  $C_{pk_U}$ . This relation is exploited in [4.8](#) to

calculate the proportion out-of-specification from lower and upper process capability indices. The relationship is displayed in [Table 2](#) for easy reference.

When these measures of process capability have to be extended to characteristics that are not normally distributed, the fraction nonconforming item can be transformed to a capability index using the relationships in [Table 2](#). This method can be applied in particular if the product characteristic is qualitative.

**Table 2 — Process capability indices and estimates for the normal distribution — Equivalent formulae**

| Index                                 | Estimate                                                |
|---------------------------------------|---------------------------------------------------------|
| $C_p = \frac{C_{pk_U} + C_{pk_L}}{2}$ | $\hat{C}_p = \frac{\hat{C}_{pk_U} + \hat{C}_{pk_L}}{2}$ |
| $C_{pk_U} = \frac{z_{1-p_U}}{3}$      | $\hat{C}_{pk_U} = \frac{z_{1-\hat{p}_U}}{3}$            |
| $C_{pk_L} = \frac{z_{1-p_L}}{3}$      | $\hat{C}_{pk_L} = \frac{z_{1-\hat{p}_L}}{3}$            |

where  $p_U$  and  $p_L$  are the fractions nonconforming at the upper and lower specification limits and  $\hat{p}_U$ ,  $\hat{p}_L$  are the corresponding estimates. The formulae in the above table can be applied to any distribution.

It is assumed that the user has knowledge of the shape of the distribution because of what is known about the manufacturing process or by some evaluation of a sample by an appropriate probability paper.

For those distributions that are frequently observed (normal, log-normal, Rayleigh and Weibull), the required relations and formulae are given in [Annex C](#).

## 4.7 Other capability measures for continuous data

### 4.7.1 Process capability fraction (PCF)

The PCF is the inverse of the  $C_p$  index:

$$\frac{6\sigma}{U-L} = \frac{1}{C_p}$$

It can be expressed as a percentage value and occasionally named  $C_R$  (%).

### 4.7.2 Indices when the specification limit is one-sided or no specification limit is given

#### 4.7.2.1 General

Sometimes, a specification is given that has only one limit, e.g. a maximum value. In these circumstances, it will only be possible to compute a  $C_{pk}$  or a  $P_{pk}$  index.

There will also be situations when specification limits are not given or not known. However, if a target or nominal value is given for the product characteristic or process parameter, the following measures might be appropriate. They present a special appeal to those engaged in minimizing process variation around a target value.

#### 4.7.2.2 Mean square error (MSE)

The mean square error provides a measure that involves both location and variation. It is computed as follows:

$$\sigma^2 + (\mu - T)$$

In deriving this measure from data, it is necessary to provide estimates of the process standard deviation and  $\mu$  using sample data from a control chart.

#### 4.7.2.3 $Q_k$ index

This index uses the mean square error given in 4.7.2.2, but expresses the whole value as a coefficient of variation and is computed as follows:

$$Q_k = \frac{100\sqrt{\sigma^2 + (\mu - T)^2}}{T} (\%)$$

for  $T \neq 0$ .

An interesting property of this index is if the process drifts from its target, the index will increase in value and if the process variation increases, it will also increase the value of the index. The smaller this index becomes, the better the process is deemed to have performed.

#### 4.7.2.4 $C_{pm}$ index

The  $C_{pm}$  index, like the  $Q_k$  index, incorporates the target value and the MSE into the calculation.

In its simplest form, the index is:

$$C_{pm} = \frac{U - L}{6\sqrt{\sigma^2 + (\mu - T)^2}}$$

This calculation implies that  $T$  is the midpoint between  $U$  and  $L$  and so a refinement was later introduced that allowed for a non-central  $T$  value:

$$C_{pm}^* = \frac{\min(U - T, T - L)}{3\sqrt{\sigma^2 + (\mu - T)^2}}$$

Compared to the usual indices,  $C_p$  and  $C_{pk}$ , here only one index is needed to describe a situation.

The  $C_{pm}$  index is sometimes referred to as a Taguchi index because of the incorporation of the MSE in the denominator.

#### 4.8 Assessment of proportion out-of-specification (normal distribution)

The proportion of out-of-specification items ( $p_L$  and  $p_U$ ) that fall below  $L$  and above  $U$  can be estimated using properties of the standard normal distribution. Standardized deviates can be calculated as follows:

$$z_{\hat{p}_U} = 3\hat{C}_{pk_U}$$

and

$$z_{\hat{p}_L} = 3\hat{C}_{pk_L}$$

$\hat{p}_U$  and  $\hat{p}_L$  are found as the proportions exceeding  $z_{p_U}$  and  $z_{p_L}$ , respectively, in a standard normal distribution.

Additionally, the process yield can be computed as 100 % minus the total percentage nonconforming in the case of a controlled process.

If a characteristic, in statistical control and stable, has a  $C_{pk_U}$  of 0,86 and a  $C_{pk_L}$  of 0,91, the proportion of out-of-specification can be determined using the method given above as follows.

a) Calculate the “upper” standardized deviate.

$$\begin{aligned} z_{\hat{p}_L} &= 3\hat{C}_{pk_L} \\ &= 3 \times 0,91 \\ &= 2,73 \end{aligned}$$

b) Calculate the “lower” standardized deviate.

$$\begin{aligned} z_{\hat{p}_U} &= 3\hat{C}_{pk_U} \\ &= 3 \times 0,86 \\ &= 2,58 \end{aligned}$$

c) Using the standard normal distribution, look up or calculate the values  $\hat{p}_U$  and  $\hat{p}_L$  for the proportions of the distribution beyond the specification limits  $U$  and  $L$ ,  $z_{p_U}$  and  $z_{p_L}$ , respectively.

For convenience and ease of use, [Table 3](#) gives look-up values for the estimated proportion out-of-specification. [Table 3](#) is indexed by  $C_{pk_U}$  or  $C_{pk_L}$  the process capability indices (PCI). [Table 3](#) should not be used to derive  $C_p$  nor  $C_{pk}$  values for attributes data.

Using the above example of a  $C_{pk_U}$  of 0,86 and a  $C_{pk_L}$  of 0,91, the estimated proportion beyond the specification limits  $U$  and  $L$  can be read directly from [Table 3](#) as 0,004 9 and 0,003 2.

**Table 3 —  $C_{pk_U}$  or  $C_{pk_L}$  (PCI in the table) and proportion of the normal distribution remaining in the tails of the distribution beyond a specification limit**

| PCI | 0,00                  | 0,01                  | 0,02                  | 0,03                  | 0,04                  | 0,05                  | 0,06                  | 0,07                  | 0,08                  | 0,09                  |
|-----|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|
| 1,6 | $7,9 \times 10^{-07}$ | $6,8 \times 10^{-07}$ | $5,9 \times 10^{-07}$ | $5,0 \times 10^{-07}$ | $4,3 \times 10^{-07}$ | $3,7 \times 10^{-07}$ | $3,2 \times 10^{-07}$ | $2,7 \times 10^{-07}$ | $2,3 \times 10^{-07}$ | $2,0 \times 10^{-07}$ |
| 1,5 | $3,4 \times 10^{-06}$ | $3,0 \times 10^{-06}$ | $2,6 \times 10^{-06}$ | $2,2 \times 10^{-06}$ | $1,9 \times 10^{-06}$ | $1,7 \times 10^{-06}$ | $1,4 \times 10^{-06}$ | $1,2 \times 10^{-06}$ | $1,1 \times 10^{-06}$ | $9,2 \times 10^{-07}$ |
| 1,4 | $1,3 \times 10^{-05}$ | $1,2 \times 10^{-05}$ | $1,0 \times 10^{-05}$ | $8,9 \times 10^{-06}$ | $7,8 \times 10^{-06}$ | $6,8 \times 10^{-06}$ | $5,9 \times 10^{-06}$ | $5,2 \times 10^{-06}$ | $4,5 \times 10^{-06}$ | $3,9 \times 10^{-06}$ |
| 1,3 | $4,8 \times 10^{-05}$ | $4,2 \times 10^{-05}$ | $3,7 \times 10^{-05}$ | $3,3 \times 10^{-05}$ | $2,9 \times 10^{-05}$ | $2,6 \times 10^{-05}$ | $2,3 \times 10^{-05}$ | $2,0 \times 10^{-05}$ | $1,7 \times 10^{-05}$ | $1,5 \times 10^{-05}$ |
| 1,2 | 0,000 2               | 0,000 1               | 0,000 1               | 0,000 1               | 0,000 1               | 0,000 1               | 0,000 1               | 0,000 1               | 0,000 1               | 0,000 1               |
| 1,1 | 0,000 5               | 0,000 4               | 0,000 4               | 0,000 3               | 0,000 3               | 0,000 3               | 0,000 3               | 0,000 2               | 0,000 2               | 0,000 2               |

Table 3 (continued)

| PCI | 0,00    | 0,01    | 0,02    | 0,03    | 0,04    | 0,05    | 0,06    | 0,07    | 0,08    | 0,09    |
|-----|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| 1,0 | 0,001 3 | 0,001 2 | 0,001 1 | 0,001 0 | 0,000 9 | 0,000 8 | 0,000 7 | 0,000 7 | 0,000 6 | 0,000 5 |
| 0,9 | 0,003 5 | 0,003 2 | 0,002 9 | 0,002 6 | 0,002 4 | 0,002 2 | 0,002 0 | 0,001 8 | 0,001 6 | 0,001 5 |
| 0,8 | 0,008 2 | 0,007 5 | 0,006 9 | 0,006 4 | 0,005 9 | 0,005 4 | 0,004 9 | 0,004 5 | 0,004 1 | 0,003 8 |
| 0,7 | 0,017 9 | 0,016 6 | 0,015 4 | 0,014 3 | 0,013 2 | 0,012 2 | 0,011 3 | 0,010 4 | 0,009 6 | 0,008 9 |
| 0,6 | 0,035 9 | 0,033 6 | 0,031 4 | 0,029 4 | 0,027 4 | 0,025 6 | 0,023 9 | 0,022 2 | 0,020 7 | 0,019 2 |
| 0,5 | 0,066 8 | 0,063 0 | 0,059 4 | 0,055 9 | 0,052 6 | 0,049 5 | 0,046 5 | 0,043 6 | 0,040 9 | 0,038 4 |
| 0,4 | 0,115 1 | 0,109 3 | 0,103 8 | 0,098 5 | 0,093 4 | 0,088 5 | 0,083 8 | 0,079 3 | 0,074 9 | 0,070 8 |
| 0,3 | 0,184 1 | 0,176 2 | 0,168 5 | 0,161 1 | 0,153 9 | 0,146 9 | 0,140 1 | 0,133 5 | 0,127 1 | 0,121 0 |
| 0,2 | 0,274 3 | 0,264 3 | 0,254 6 | 0,245 1 | 0,235 8 | 0,226 6 | 0,217 7 | 0,209 0 | 0,200 5 | 0,192 2 |
| 0,1 | 0,382 1 | 0,370 7 | 0,359 4 | 0,348 3 | 0,337 2 | 0,326 4 | 0,315 6 | 0,305 0 | 0,294 6 | 0,284 3 |
| 0,0 | 0,500 0 | 0,488 0 | 0,476 1 | 0,464 1 | 0,452 2 | 0,440 4 | 0,428 6 | 0,416 8 | 0,405 2 | 0,393 6 |

## 5 Performance

### 5.1 General

Process performance for a characteristic is the achieved distribution of results. The single important difference between *performance* and *capability* is that for performance, there is no requirement for the process to be in statistical control or for the process to be controlled using a control chart. The following are the conditions that will apply for performance:

- all technical conditions, e.g. temperature and humidity, shall be clearly stated;
- the uncertainty of the measurement system shall be estimated and judged appropriate (see ISO 22514-7);
- multi-factor, multi-level aspects of the process should be allowed;
- the duration over which the data has been gathered shall be recorded;
- the frequency of sampling shall be specified and the start and finish dates of data collection;
- the process need not be controlled with a control chart;
- the process need not be in a state of statistical control, in particular, historical data where the sequence is unknown can be used to evaluate process performance.

Indices are given below to express process performance. Their form is similar to those already given in the clause on capability and the general relationships given in [Formulae \(1\)](#) and [\(2\)](#) for measured data are used, except they are named  $P_p$ ,  $P_{pk_U}$  and  $P_{pk_L}$ , respectively.

## 5.2 Process performance indices for measured data (normal distribution)

### 5.2.1 $P_p$ index

When the individual values form a normal distribution, the length of the reference interval is equal to  $6\sigma_t$  where  $\sigma_t$  is the total standard deviation. Therefore, the  $P_p$  index can be expressed as:

$$P_p = \frac{U - L}{6\sigma_t}$$

An estimate,  $\hat{\sigma}_t$ , of the total standard deviation ( $\sigma_t$ ) is required to obtain an estimate of the  $P_p$  index. In practice,  $\hat{\sigma}_t$  will be the standard deviation ( $S_t$ ) of all of the data. When this has been obtained, the index is estimated.

### 5.2.2 $P_{pk}$ index

When the distribution of individual values forms a normal distribution, the median  $X_{50\%}$  is equal to the mean ( $\mu$ ). Further,  $X_{99,865\%} - X_{50\%}$  and  $X_{50\%} - X_{0,135\%}$  are each equal to  $3\sigma_t$ . Therefore, the  $P_{pk}$  index is the smaller of the two values:

$$P_{pk_U} = \frac{U - \mu}{3\sigma_t}$$

or

$$P_{pk_L} = \frac{\mu - L}{3\sigma_t}$$

where the indices are estimated by:

$$\hat{P}_{pk_U} = \frac{U - \bar{X}}{3\hat{\sigma}_t}$$

or

$$\hat{P}_{pk_L} = \frac{\bar{X} - L}{3\hat{\sigma}_t}$$

A lower index means greater proportion of items produced out-of-specification.

## 5.3 Process performance indices for measured data (non-normal distribution)

### 5.3.1 General

The approaches adopted in this clause for non-normal data is the same as that given earlier in [4.5](#) for capability indices.

### 5.3.2 Probability paper method

From graphs similar to those given in [Figure 5](#), estimates of the percentiles  $X_{0,135} \%$  and  $X_{99,865} \%$  can be obtained. The estimates are denoted by  $Y_1$  and  $Y_2$ , respectively, and the formula becomes:

$$\hat{P}_p = \frac{U - L}{Y_2 - Y_1}$$

In a similar way, the  $P_{pk}$  formulae become:

$$\hat{P}_{pk_U} = \frac{U - \hat{X}_{50\%}}{Y_2 - \hat{X}_{50\%}}$$

or

$$\hat{P}_{pk_L} = \frac{\hat{X}_{50\%} - L}{\hat{X}_{50\%} - Y_1}$$

whichever of them gives the least value.

If the index is less than a given value, the process is deemed to have produced an excessive proportion of items outside of the specification. The proportion nonconforming depends upon the distribution and the value of the index. The link between the index and the proportion of nonconforming items produced depends on the class of distributions. Care should be taken not to interpret indices on the basis of cut-off points that have derived for the normal distribution and, hence, are only applicable for that distribution.

The probability paper method directly estimates fairly extreme percentiles and that this can be inaccurate. Additionally, the estimation method using probability paper, although very simple to use, is nevertheless somewhat crude and computational procedures are preferred (see [Annex C](#)).

### 5.3.3 Pearson curves method

As an alternative to using probability paper, standardized Pearson curves are sometimes used. The method is described by way of an example (see [Annex B](#)). The index is computed using:

$$\hat{P}_p = \frac{U - L}{\hat{X}_{99,865\%} - \hat{X}_{0,135\%}}$$

where  $\hat{X}_{0,135\%}$  and  $\hat{X}_{99,865\%}$  are the estimated 0,135 % and 99,865 % percentiles from the standardized Pearson curves.

Also, we have the formulae:

$$\hat{P}_{pk_U} = \frac{U - \hat{X}_{50\%}}{\hat{X}_{99,865\%} - \hat{X}_{50\%}}$$

and

$$\hat{P}_{pk_L} = \frac{\hat{X}_{50\%} - L}{\hat{X}_{50\%} - \hat{X}_{0,135\%}}$$

where  $\hat{X}_{50\%}$  is the estimated median value.

In order to use this method, the user will need to establish skewness and kurtosis values in addition to the mean and standard deviation for the data set upon which the index is to be computed.

This method is not preferred, but is presented here due to its occasional use for completeness (see 4.5.3 for further comments about the use of this method).

#### 5.3.4 Distribution identification method

See Annex C for a description of certain families of distribution functions such as the log-normal distribution, the Rayleigh and the Weibull distributions that are commonly found when investigating process performance. See also 4.5.4 for further comments about the method.

#### 5.4 Other performance indices for measured data

All of the indices given earlier for capability will have counterparts when considering performance. Any standard deviation will represent the total variation ( $\sigma_t$ ) instead of the inherent variation ( $\sigma$ ).

#### 5.5 Assessment of proportion out-of-specification for a normal distribution of the total distribution

The same method to estimate the proportion of out-of-specification is used here as in 4.8. The reader should substitute  $\hat{P}_{pk_U}$  and  $\hat{P}_{pk_L}$  respectively for  $C_{pk_U}$  and  $C_{pk_L}$ . Table 3 can also be used to determine the proportion out-of-specification and the reader should enter the table with  $\hat{P}_{pk_U}$  or  $\hat{P}_{pk_L}$  instead of  $C_{pk_U}$  or  $C_{pk_L}$ .

### 6 Reporting process capability and performance indices

If process capability (or performance) statistics are used for process qualification, they should be reported in relation to this part of ISO 22514. The calculation method and the number of values used as basis for the calculation shall be stated.

An example is given in Table 4.

**Table 4 — Example of report of calculated process capability indices**

|                                                     |                        |
|-----------------------------------------------------|------------------------|
| Process capability (or performance) index           | $C_p = 2,01$           |
| Minimum process capability (or performance) index   | $C_{pk} = 1,90$        |
| Confidence interval                                 | $1,54 < C_{pk} < 2,26$ |
| Number of values used for the calculation           | 100                    |
| Measurement uncertainty                             | 0,002 mm               |
| Optional:                                           |                        |
| — frequency of sampling;                            | 30 min.                |
| — time and duration of data taking;                 |                        |
| — distribution model;                               | Normal                 |
| — technical conditions (batches, operation, tools). |                        |

Additionally, the study report shall contain the following information:

- the place where the study was performed and the type of process the machine is part of;
- the persons who performed the study and who took the measurements;
- when the study was performed, including the date, times of start and finish, log of any interruptions;
- any machine and process reference numbers;
- the component's name and reference number;

- f) the component characteristic(s) measured;
- g) the specification for the characteristic(s) and what factors were held constant;
- h) ambient conditions;
- i) the raw data;
- j) non-standard conditions.

For each characteristic measured, the following shall be reported (or provided):

- the distribution model estimated;
- the calculated indices.

The following should be reported (or provided):

- a control chart of the data;
- a tally chart or histogram of the data;
- a probability plot of the data;
- the mean value from the data;
- the standard deviation from the data;
- the estimated percentage out of specification;
- the calculated indices' confidence intervals;
- the measurement uncertainty/measurement process capability.

## Annex A (informative)

### Estimating standard deviations

#### A.1 General

It is necessary to estimate the standard deviation in order to calculate the indices referred to in this part of ISO 22514. There are two types of standard deviation to consider. The first is what might be described as the short-term standard deviation or instantaneous (inherent) standard deviation. It is often calculated from statistics taken from a control chart and this is shown in [A.2](#). The other is the estimation of the total standard deviation and this is described in [A.3](#).

If the process has more than one mode or state, the spread should be calculated by following the method given in ISO 22514-2 or ISO 22514-8.

#### A.2 Inherent standard deviation

##### A.2.1 Estimation using the mean range value

The inherent (process) standard deviation (the data will be taken from an “in control” control chart) can be estimated from a range control chart using:

$$\hat{\sigma} = \frac{\bar{R}}{d_2}$$

where  $d_2$  is a factor taken from [Table A.1](#).

**Table A.1 — Factors for the estimation of process standard deviation**

| Subgroup size ( $n$ ) | $d_2$ | $c_4$   |
|-----------------------|-------|---------|
| 2                     | 1,128 | 0,797 9 |
| 3                     | 1,693 | 0,886 2 |
| 4                     | 2,059 | 0,921 3 |
| 5                     | 2,326 | 0,940 0 |
| 6                     | 2,534 | 0,951 5 |
| 7                     | 2,704 | 0,959 4 |
| 8                     | 2,847 | 0,965 0 |
| 9                     | 2,970 | 0,969 3 |
| 10 <sup>a</sup>       | 3,078 | 0,972 7 |

<sup>a</sup> Values for  $d_2$  and  $c_4$  may be found in textbooks for sample sizes greater than 10.

### A.2.2 Estimation using the mean standard deviation value

If a standard deviation control chart has been used to monitor the within subgroup variation, the inherent (process) standard deviation can be estimated using:

$$\hat{\sigma} = \frac{\bar{S}}{c_4}$$

where  $c_4$  is a control chart factor taken from [Table A.1](#).

### A.2.3 Estimation using subgroup standard deviations

If the within subgroup standard deviation is calculated for every subgroup, the inherent (process) standard deviation can be estimated using:

$$\hat{\sigma} = \sqrt{\frac{\sum_{j=1}^m S_j^2}{m}}$$

where there are  $m$  subgroups of  $n$  observations in each.

## A.3 Estimation of total standard deviation

When data are generated from a process which is “out-of-control” or if no control chart has been used, it is inappropriate to compute the standard deviation using the methods of [A.2](#). The following formula should be used instead:

$$\hat{\sigma}_t = S_t = \sqrt{\frac{\sum_{i=1}^N (X_i - \bar{X})^2}{N - 1}}$$

The circumstances that lead to the use of this formula are when fluctuations exist in the process mean caused by assignable causes that might not be removable and this extra variation is to be incorporated with the remaining random cause variation. It is the appropriate measure of variation for use in calculating the performance indices.

When considering multiple stream processes, such as a multiple cavity injection moulding press, it is often desired to treat the data from all the cavities as if they came from a single process. The data from each cavity might form a single normal distribution. However, the reality is often that each cavity produces a slightly different distribution because either the means or the variabilities or both are different. If the data from all of the process streams can be considered to yield a normal distribution, the best estimate of the process variation will be given by this formula.

## Annex B (informative)

### Estimating capability and performance measures using Pearson curves — Procedure and example<sup>1)</sup>

#### B.1 Record specification limits

Upper limit,  $U = 0,30$

Lower limit,  $L = 0,20$

#### B.2 Record process statistics

The process is shown to be statistically “in control”.

Mean,  $\bar{x} = 0,235$

Standard deviation,  $\hat{\sigma} = 0,012\ 2$

Skewness,  $\hat{\gamma}_1 = 0,7$  (rounding to one decimal place)

Kurtosis,  $\hat{\beta}_2 = 3,5$  (rounding to one decimal place)

#### B.3 Look up standardized 0,135 percentile

For positive skewness, use [Table B.1](#). For negative skewness, use [Table B.2](#).

0,135 percentile,  $P_{0,135\ \%} = 3,056$  by interpolation.

#### B.4 Look up standardized 99,865 percentile

For positive skewness, use [Table B.2](#). For negative skewness, use [Table B.1](#).

99,865 percentile,  $P_{99,865\ \%} = 4,656$  by interpolation.

#### B.5 Look up standardized median in [Table B.3](#)

For positive skewness, reverse the sign. For negative skewness, leave positive.

Standardized median,  $P_{50\ \%} = -0,067\ 5$  by interpolation.

#### B.6 Compute estimated 0,135 % percentile

$$\begin{aligned}\hat{X}_{0,135\ \%} &= \bar{x} - \hat{\sigma} P_{0,135\ \%} \\ &= 0,235 - (0,012\ 2 \times 3,056) \\ &= 0,197\ 7\end{aligned}$$

<sup>1)</sup> Procedure based on that in Reference [\[10\]](#).

## B.7 Compute estimated 99,865 % percentile

$$\begin{aligned} X_{99,865 \%} &= \bar{x} + \hat{\sigma} P_{99,865 \%} \\ &= 0,235 + (0,012\ 2 \times 4,656) \\ &= 0,291\ 8 \end{aligned}$$

## B.8 Compute estimated median

$$\begin{aligned} \hat{X}_{50 \%} &= \bar{x} + \hat{\sigma} P_{50 \%} \\ &= 0,235 + (0,012\ 2 \times -0,067\ 5) \\ &= 0,234\ 2 \end{aligned}$$

## B.9 Compute process capability indices

$$\begin{aligned} \hat{C}_p &= \frac{U - L}{\hat{X}_{99,865 \%} - \hat{X}_{0,135 \%}} \\ &= \frac{0,30 - 0,20}{0,291\ 8 - 0,197\ 7} \\ &= 1,06 \end{aligned}$$

$$\begin{aligned} \hat{C}_{pk_U} &= \frac{U - \hat{X}_{50 \%}}{\hat{X}_{99,865 \%} - \hat{X}_{50 \%}} \\ &= \frac{0,30 - 0,234\ 2}{0,291\ 8 - 0,234\ 2} \\ &= 1,14 \end{aligned}$$

$$\begin{aligned} \hat{C}_{pk_L} &= \frac{\hat{X}_{50 \%} - L}{\hat{X}_{50 \%} - \hat{X}_{0,135 \%}} \\ &= \frac{0,234\ 2 - 0,20}{0,234\ 2 - 0,197\ 7} \\ &= 0,94 \end{aligned}$$

STANDARDSISO.COM : Click to view the full PDF of ISO 22514-4:2016

Table B.1

| PEARSON CURVES (STANDARDIZED TAILS)                                                                                                       |                         |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |               |
|-------------------------------------------------------------------------------------------------------------------------------------------|-------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|---------------|
| $P_{0,135} \% (0,135 \text{ percentile}) \text{ for } \gamma_1 > 0, P_{99,865} \% (99,865 \text{ percentile}) \text{ for } \gamma_1 < 0.$ |                         |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |               |
| Kurtosis<br>( $\beta_2$ )                                                                                                                 | Skewness ( $\gamma_1$ ) |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |               |
|                                                                                                                                           | 0,0                     | 0,1   | 0,2   | 0,3   | 0,4   | 0,5   | 0,6   | 0,7   | 0,8   | 0,9   | 1,0   | 1,1   | 1,2   | 1,3   | 1,4   | 1,5   | 1,6   | 1,7   | 1,8   | 1,9   | 2,0   | ( $\beta_2$ ) |
| -1,4                                                                                                                                      | 1,512                   | 1,421 | 1,317 | 1,206 | 1,092 | 0,979 | 0,868 | 0,762 |       |       |       |       |       |       |       |       |       |       |       |       |       | -1,4          |
| -1,2                                                                                                                                      | 1,727                   | 1,619 | 1,496 | 1,364 | 1,230 | 1,100 | 0,975 | 0,858 | 0,747 |       |       |       |       |       |       |       |       |       |       |       |       | -1,2          |
| -1,0                                                                                                                                      | 1,966                   | 1,840 | 1,696 | 1,541 | 1,384 | 1,232 | 1,089 | 0,957 | 0,836 |       |       |       |       |       |       |       |       |       |       |       |       | -1,0          |
| -0,8                                                                                                                                      | 2,210                   | 2,072 | 1,912 | 1,736 | 1,555 | 1,377 | 1,212 | 1,062 | 0,927 | 0,804 | 0,692 |       |       |       |       |       |       |       |       |       |       | -0,8          |
| -0,6                                                                                                                                      | 2,442                   | 2,298 | 2,129 | 1,941 | 1,740 | 1,539 | 1,348 | 1,175 | 1,023 | 0,887 | 0,766 | 0,656 |       |       |       |       |       |       |       |       |       | -0,6          |
| -0,4                                                                                                                                      | 2,653                   | 2,506 | 2,335 | 2,141 | 1,930 | 1,711 | 1,496 | 1,299 | 1,125 | 0,974 | 0,841 | 0,723 | 0,616 |       |       |       |       |       |       |       |       | -0,4          |
| -0,2                                                                                                                                      | 2,839                   | 2,692 | 2,522 | 2,329 | 2,116 | 1,887 | 1,655 | 1,434 | 1,235 | 1,065 | 0,919 | 0,791 | 0,677 | 0,574 |       |       |       |       |       |       |       | -0,2          |
| 0,0                                                                                                                                       | 3,000                   | 2,856 | 2,689 | 2,500 | 2,289 | 2,059 | 1,817 | 1,578 | 1,356 | 1,163 | 1,000 | 0,861 | 0,739 | 0,630 | 0,531 |       |       |       |       |       |       | 0,0           |
| 0,2                                                                                                                                       | 3,140                   | 2,986 | 2,834 | 2,653 | 2,447 | 2,220 | 1,976 | 1,726 | 1,485 | 1,269 | 1,086 | 0,933 | 0,801 | 0,686 | 0,583 |       |       |       |       |       |       | 0,2           |
| 0,4                                                                                                                                       | 3,261                   | 3,088 | 2,952 | 2,785 | 2,589 | 2,368 | 2,127 | 1,873 | 1,619 | 1,382 | 1,178 | 1,008 | 0,865 | 0,742 | 0,634 | 0,536 |       |       |       |       |       | 0,4           |
| 0,6                                                                                                                                       | 3,366                   | 3,164 | 3,045 | 2,896 | 2,714 | 2,502 | 2,267 | 2,015 | 1,754 | 1,502 | 1,277 | 1,087 | 0,931 | 0,799 | 0,685 | 0,583 | 0,489 |       |       |       |       | 0,6           |
| 0,8                                                                                                                                       | 3,458                   | 3,222 | 3,118 | 2,986 | 2,821 | 2,622 | 2,396 | 2,148 | 1,887 | 1,625 | 1,381 | 1,172 | 1,000 | 0,857 | 0,736 | 0,629 | 0,533 |       |       |       |       | 0,8           |
| 1,0                                                                                                                                       | 3,539                   | 3,266 | 3,174 | 3,058 | 2,910 | 2,727 | 2,512 | 2,271 | 2,013 | 1,748 | 1,491 | 1,262 | 1,072 | 0,917 | 0,787 | 0,675 | 0,575 | 0,484 |       |       |       | 1,0           |
| 1,2                                                                                                                                       | 3,611                   | 3,300 | 3,218 | 3,115 | 2,983 | 2,817 | 2,616 | 2,385 | 2,132 | 1,876 | 1,602 | 1,357 | 1,149 | 0,979 | 0,840 | 0,721 | 0,617 | 0,524 |       |       |       | 1,2           |
| 1,4                                                                                                                                       | 3,674                   | 3,327 | 3,254 | 3,161 | 3,043 | 2,893 | 2,708 | 2,488 | 2,243 | 1,981 | 1,713 | 1,456 | 1,230 | 1,045 | 0,894 | 0,768 | 0,659 | 0,562 | 0,475 |       |       | 1,4           |
| 1,6                                                                                                                                       | 3,731                   | 3,349 | 3,282 | 3,199 | 3,092 | 2,957 | 2,787 | 2,581 | 2,345 | 2,089 | 1,821 | 1,556 | 1,316 | 1,113 | 0,950 | 0,815 | 0,701 | 0,600 | 0,510 |       |       | 1,6           |
| 1,8                                                                                                                                       | 3,782                   | 3,367 | 3,306 | 3,229 | 3,133 | 3,011 | 2,855 | 2,664 | 2,438 | 2,189 | 1,925 | 1,664 | 1,404 | 1,185 | 1,008 | 0,863 | 0,743 | 0,638 | 0,546 | 0,461 |       | 1,8           |
| 2,0                                                                                                                                       | 3,828                   | 3,382 | 3,325 | 3,255 | 3,167 | 3,055 | 2,914 | 2,736 | 2,524 | 2,283 | 2,023 | 1,755 | 1,494 | 1,261 | 1,068 | 0,913 | 0,785 | 0,676 | 0,580 | 0,494 |       | 2,0           |
| 2,2                                                                                                                                       | 3,870                   | 3,395 | 3,342 | 3,277 | 3,196 | 3,093 | 2,964 | 2,800 | 2,600 | 2,369 | 2,116 | 1,850 | 1,584 | 1,339 | 1,132 | 0,964 | 0,828 | 0,714 | 0,615 | 0,526 | 0,445 | 2,2           |
| 2,4                                                                                                                                       | 3,908                   | 3,405 | 3,356 | 3,295 | 3,220 | 3,126 | 3,006 | 2,855 | 2,669 | 2,448 | 2,202 | 1,940 | 1,673 | 1,420 | 1,198 | 1,018 | 0,873 | 0,752 | 0,649 | 0,557 | 0,475 | 2,4           |
| 2,6                                                                                                                                       | 3,943                   | 3,415 | 3,367 | 3,311 | 3,241 | 3,153 | 3,043 | 2,904 | 2,730 | 2,521 | 2,283 | 2,026 | 1,760 | 1,501 | 1,267 | 1,073 | 0,918 | 0,791 | 0,683 | 0,589 | 0,504 | 2,6           |
| 2,8                                                                                                                                       | 3,975                   | 3,423 | 3,378 | 3,324 | 3,259 | 3,177 | 3,075 | 2,946 | 2,784 | 2,586 | 2,358 | 2,107 | 1,844 | 1,581 | 1,338 | 1,131 | 0,965 | 0,830 | 0,717 | 0,620 | 0,533 | 2,8           |

Table B.1 (continued)

| PEARSON CURVES (STANDARDIZED TAILS)                                                                                                       |                         |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |               |
|-------------------------------------------------------------------------------------------------------------------------------------------|-------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|---------------|
| $P_{0,135} \% (0,135 \text{ percentile}) \text{ for } \gamma_1 > 0. P_{99,865} \% (99,865 \text{ percentile}) \text{ for } \gamma_1 < 0.$ |                         |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |               |
| Kurtosis<br>( $\beta_2$ )                                                                                                                 | Skewness ( $\gamma_1$ ) |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       | ( $\beta_2$ ) |
|                                                                                                                                           | 0,0                     | 0,1   | 0,2   | 0,3   | 0,4   | 0,5   | 0,6   | 0,7   | 0,8   | 0,9   | 1,0   | 1,1   | 1,2   | 1,3   | 1,4   | 1,5   | 1,6   | 1,7   | 1,8   | 1,9   | 2,0   |               |
| 3,0                                                                                                                                       | 4,004                   | 3,430 | 3,387 | 3,326 | 3,274 | 3,198 | 3,103 | 2,983 | 2,831 | 2,646 | 2,427 | 2,183 | 1,924 | 1,661 | 1,410 | 1,191 | 1,013 | 0,870 | 0,752 | 0,651 | 0,562 | 3,0           |
| 3,2                                                                                                                                       | 4,031                   | 3,436 | 3,395 | 3,346 | 3,288 | 3,216 | 3,127 | 3,015 | 2,874 | 2,699 | 2,491 | 2,254 | 2,000 | 1,738 | 1,483 | 1,253 | 1,063 | 0,911 | 0,787 | 0,681 | 0,590 | 3,2           |
| 3,4                                                                                                                                       | 4,056                   | 3,441 | 3,402 | 3,356 | 3,300 | 3,233 | 3,149 | 3,043 | 2,911 | 2,747 | 2,549 | 2,321 | 2,072 | 1,813 | 1,555 | 1,317 | 1,115 | 0,953 | 0,822 | 0,712 | 0,618 | 3,4           |
| 3,6                                                                                                                                       | 4,079                   | 3,446 | 3,408 | 3,364 | 3,311 | 3,247 | 3,168 | 3,069 | 2,945 | 2,790 | 2,602 | 2,383 | 2,140 | 1,884 | 1,626 | 1,381 | 1,169 | 0,996 | 0,858 | 0,744 | 0,646 | 3,6           |
| 3,8                                                                                                                                       | 4,101                   | 3,450 | 3,414 | 3,371 | 3,321 | 3,259 | 3,184 | 3,091 | 2,974 | 2,829 | 2,651 | 2,440 | 2,205 | 1,953 | 1,695 | 1,446 | 1,224 | 1,041 | 0,895 | 0,775 | 0,674 | 3,8           |
| 4,0                                                                                                                                       | 4,121                   | 3,454 | 3,419 | 3,378 | 3,329 | 3,271 | 3,200 | 3,111 | 3,001 | 2,864 | 2,695 | 2,494 | 2,265 | 2,018 | 1,762 | 1,510 | 1,281 | 1,088 | 0,932 | 0,807 | 0,702 | 4,0           |
| 4,2                                                                                                                                       | 4,140                   | 3,458 | 3,423 | 3,384 | 3,337 | 3,281 | 3,213 | 3,129 | 3,025 | 2,895 | 2,735 | 2,543 | 2,321 | 2,080 | 1,827 | 1,574 | 1,338 | 1,135 | 0,971 | 0,839 | 0,730 | 4,2           |
| 4,4                                                                                                                                       | 4,157                   | 3,461 | 3,428 | 3,389 | 3,344 | 3,290 | 3,225 | 3,145 | 3,047 | 2,923 | 2,771 | 2,588 | 2,374 | 2,138 | 1,889 | 1,636 | 1,396 | 1,184 | 1,011 | 0,872 | 0,758 | 4,4           |
| v                                                                                                                                         |                         |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |               |
| 4,6                                                                                                                                       | 4,174                   | 3,464 | 3,431 | 3,394 | 3,350 | 3,299 | 3,236 | 3,160 | 3,066 | 2,945 | 2,805 | 2,629 | 2,424 | 2,194 | 1,948 | 1,697 | 1,453 | 1,234 | 1,052 | 0,905 | 0,786 | 4,6           |
| 4,8                                                                                                                                       | 4,189                   | 3,466 | 3,435 | 3,399 | 3,356 | 3,306 | 3,246 | 3,173 | 3,084 | 2,972 | 2,835 | 2,668 | 2,470 | 2,246 | 2,005 | 1,756 | 1,510 | 1,285 | 1,094 | 0,939 | 0,815 | 4,8           |
| 5,0                                                                                                                                       | 4,204                   | 3,469 | 3,438 | 3,403 | 3,362 | 3,313 | 3,256 | 3,186 | 3,100 | 2,994 | 2,863 | 2,703 | 2,513 | 2,296 | 2,059 | 1,813 | 1,566 | 1,336 | 1,137 | 0,975 | 0,844 | 5,0           |
| 5,2                                                                                                                                       | 4,218                   | 3,471 | 3,441 | 3,406 | 3,367 | 3,320 | 3,264 | 3,197 | 3,114 | 3,013 | 2,888 | 2,735 | 2,562 | 2,342 | 2,111 | 1,867 | 1,621 | 1,387 | 1,181 | 1,010 | 0,874 | 5,2           |
| 5,4                                                                                                                                       | 4,231                   | 3,473 | 3,444 | 3,410 | 3,371 | 3,326 | 3,272 | 3,207 | 3,128 | 3,031 | 2,911 | 2,765 | 2,589 | 2,386 | 2,160 | 1,920 | 1,675 | 1,438 | 1,225 | 1,047 | 0,904 | 5,4           |
| 5,6                                                                                                                                       | 4,243                   | 3,475 | 3,446 | 3,413 | 3,375 | 3,331 | 3,279 | 3,216 | 3,140 | 3,047 | 2,933 | 2,793 | 2,624 | 2,427 | 2,206 | 1,970 | 1,727 | 1,489 | 1,270 | 1,085 | 0,935 | 5,6           |
| 5,8                                                                                                                                       | 4,255                   | 3,477 | 3,448 | 3,416 | 3,379 | 3,336 | 3,286 | 3,225 | 3,152 | 3,062 | 2,952 | 2,818 | 2,656 | 2,465 | 2,250 | 2,019 | 1,778 | 1,539 | 1,316 | 1,123 | 0,966 | 5,8           |
| 6,0                                                                                                                                       | 4,266                   | 3,478 | 3,451 | 3,419 | 3,383 | 3,341 | 3,292 | 3,233 | 3,162 | 3,076 | 2,970 | 2,841 | 2,685 | 2,501 | 2,292 | 2,065 | 1,827 | 1,588 | 1,361 | 1,162 | 0,999 | 6,0           |
| 6,2                                                                                                                                       | 4,276                   | 3,480 | 3,453 | 3,422 | 3,386 | 3,345 | 3,297 | 3,240 | 3,172 | 3,089 | 2,987 | 2,863 | 2,713 | 2,535 | 2,332 | 2,109 | 1,874 | 1,635 | 1,407 | 1,202 | 1,031 | 6,2           |
| 6,4                                                                                                                                       | 4,286                   | 3,481 | 3,454 | 3,424 | 3,389 | 3,349 | 3,303 | 3,247 | 3,181 | 3,100 | 3,003 | 2,883 | 2,739 | 2,567 | 2,369 | 2,151 | 1,919 | 1,682 | 1,452 | 1,242 | 1,065 | 6,4           |
| 6,6                                                                                                                                       | 4,296                   | 3,483 | 3,456 | 3,426 | 3,392 | 3,353 | 3,308 | 3,254 | 3,189 | 3,111 | 3,017 | 2,902 | 2,763 | 2,597 | 2,405 | 2,191 | 1,962 | 1,727 | 1,496 | 1,282 | 1,099 | 6,6           |
| 6,8                                                                                                                                       | 4,305                   | 3,484 | 3,458 | 3,429 | 3,395 | 3,357 | 3,312 | 3,260 | 3,197 | 3,122 | 3,030 | 2,919 | 2,785 | 2,624 | 2,438 | 2,229 | 2,004 | 1,771 | 1,540 | 1,323 | 1,134 | 6,8           |
| 7,0                                                                                                                                       | 4,313                   | 3,485 | 3,459 | 3,431 | 3,398 | 3,360 | 3,316 | 3,265 | 3,204 | 3,131 | 3,043 | 2,936 | 2,806 | 2,651 | 2,469 | 2,265 | 2,044 | 1,814 | 1,583 | 1,363 | 1,169 | 7,0           |
| 7,2                                                                                                                                       | 4,322                   | 3,486 | 3,461 | 3,432 | 3,400 | 3,363 | 3,321 | 3,270 | 3,211 | 3,140 | 3,054 | 2,951 | 2,825 | 2,675 | 2,499 | 2,300 | 2,083 | 1,855 | 1,625 | 1,403 | 1,204 | 7,2           |
| 7,4                                                                                                                                       | 4,330                   | 3,487 | 3,462 | 3,434 | 3,403 | 3,366 | 3,324 | 3,275 | 3,218 | 3,148 | 3,065 | 2,965 | 2,843 | 2,698 | 2,527 | 2,333 | 2,120 | 1,895 | 1,666 | 1,443 | 1,240 | 7,4           |

Table B.1 (continued)

| PEARSON CURVES (STANDARDIZED TAILS)                                                                           |                         |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |               |      |
|---------------------------------------------------------------------------------------------------------------|-------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|---------------|------|
| $P_{0,135\%}$ (0,135 percentile) for $\gamma_1 > 0$ . $P_{99,865\%}$ (99,865 percentile) for $\gamma_1 < 0$ . |                         |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |               |      |
| Kurtosis<br>( $\beta_2$ )                                                                                     | Skewness ( $\gamma_1$ ) |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |               |      |
|                                                                                                               | 0,0                     | 0,1   | 0,2   | 0,3   | 0,4   | 0,5   | 0,6   | 0,7   | 0,8   | 0,9   | 1,0   | 1,1   | 1,2   | 1,3   | 1,4   | 1,5   | 1,6   | 1,7   | 1,8   | 1,9   | 2,0   | ( $\beta_2$ ) |      |
| 7,6                                                                                                           | 4,337                   | 3,488 | 3,464 | 3,436 | 3,405 | 3,369 | 3,328 | 3,280 | 3,224 | 3,156 | 3,075 | 2,978 | 2,860 | 2,720 | 2,554 | 2,364 | 2,155 | 1,933 | 1,706 | 1,482 | 1,276 | 7,6           |      |
| 7,8                                                                                                           | 4,344                   | 3,489 | 3,465 | 3,437 | 3,407 | 3,372 | 3,331 | 3,284 | 3,229 | 3,164 | 3,085 | 2,990 | 2,876 | 2,740 | 2,579 | 2,394 | 2,189 | 1,970 | 1,744 | 1,521 | 1,311 | 7,8           |      |
| 8,0                                                                                                           | 4,351                   | 3,490 | 3,466 | 3,439 | 3,409 | 3,374 | 3,335 | 3,289 | 3,235 | 3,171 | 3,094 | 3,002 | 2,891 | 2,759 | 2,603 | 2,422 | 2,221 | 2,005 | 1,782 | 1,559 | 1,347 | 8,0           |      |
| 8,2                                                                                                           | 4,358                   | 3,491 | 3,467 | 3,440 | 3,411 | 3,377 | 3,338 | 3,292 | 3,240 | 3,177 | 3,103 | 3,013 | 2,906 | 2,777 | 2,625 | 2,449 | 2,252 | 2,040 | 1,818 | 1,596 | 1,382 | 8,2           |      |
| 8,4                                                                                                           | 4,365                   | 3,492 | 3,468 | 3,442 | 3,412 | 3,379 | 3,340 | 3,296 | 3,244 | 3,183 | 3,111 | 3,023 | 2,919 | 2,794 | 2,646 | 2,475 | 2,282 | 2,073 | 1,854 | 1,632 | 1,418 | 8,4           |      |
| 8,6                                                                                                           | 4,371                   | 3,492 | 3,469 | 3,443 | 3,414 | 3,381 | 3,343 | 3,300 | 3,249 | 3,189 | 3,118 | 3,033 | 2,932 | 2,810 | 2,666 | 2,499 | 2,310 | 2,104 | 1,888 | 1,667 | 1,452 | 8,6           |      |
| 8,8                                                                                                           | 4,377                   | 3,493 | 3,470 | 3,444 | 3,416 | 3,383 | 3,346 | 3,303 | 3,253 | 3,195 | 3,125 | 3,042 | 2,943 | 2,825 | 2,685 | 2,522 | 2,337 | 2,135 | 1,921 | 1,702 | 1,486 | 8,8           |      |
| 9,0                                                                                                           | 4,382                   | 3,494 | 3,471 | 3,445 | 3,417 | 3,385 | 3,348 | 3,306 | 3,257 | 3,200 | 3,132 | 3,051 | 2,955 | 2,839 | 2,703 | 2,544 | 2,363 | 2,164 | 1,953 | 1,736 | 1,520 | 9,0           |      |
| 9,2                                                                                                           | 4,388                   | 3,495 | 3,472 | 3,447 | 3,418 | 3,387 | 3,351 | 3,309 | 3,261 | 3,205 | 3,138 | 3,059 | 2,965 | 2,853 | 2,720 | 2,565 | 2,388 | 2,192 | 1,984 | 1,768 | 1,553 | 9,2           |      |
| 9,4                                                                                                           | 4,393                   | 3,495 | 3,473 | 3,448 | 3,420 | 3,388 | 3,353 | 3,312 | 3,265 | 3,209 | 3,144 | 3,067 | 2,975 | 2,866 | 2,736 | 2,585 | 2,411 | 2,219 | 2,014 | 1,800 | 1,586 | 9,4           |      |
| 9,6                                                                                                           | 4,398                   | 3,496 | 3,473 | 3,449 | 3,421 | 3,390 | 3,355 | 3,315 | 3,268 | 3,214 | 3,150 | 3,075 | 2,985 | 2,878 | 2,752 | 2,604 | 2,434 | 2,245 | 2,042 | 1,831 | 1,617 | 9,6           |      |
| 9,8                                                                                                           | 4,403                   | 3,496 | 4,474 | 3,450 | 3,422 | 3,392 | 3,357 | 3,317 | 3,272 | 3,218 | 3,156 | 3,082 | 2,994 | 2,890 | 2,766 | 2,622 | 2,456 | 2,271 | 2,070 | 1,861 | 1,648 | 9,8           |      |
| 10,0                                                                                                          | 4,408                   | 3,497 | 3,475 | 3,451 | 3,424 | 3,393 | 3,359 | 3,320 | 3,275 | 3,222 | 3,161 | 3,088 | 3,003 | 2,901 | 2,780 | 2,639 | 2,476 | 2,295 | 2,097 | 1,890 | 1,679 | 10,0          |      |
| 10,2                                                                                                          |                         |       |       |       | 3,425 | 3,395 | 3,361 | 3,322 | 3,278 | 3,226 | 3,166 | 3,095 | 3,011 | 2,911 | 2,793 | 2,655 | 2,496 | 2,318 | 2,123 | 1,918 | 1,708 | 10,2          |      |
| 10,4                                                                                                          |                         |       |       |       |       | 3,396 | 3,363 | 3,325 | 3,281 | 3,230 | 3,171 | 3,101 | 3,019 | 2,921 | 2,806 | 2,671 | 2,515 | 2,340 | 2,148 | 1,945 | 1,737 | 10,4          |      |
| 10,6                                                                                                          |                         |       |       |       |       |       | 3,364 | 3,327 | 3,283 | 3,233 | 3,175 | 3,107 | 3,026 | 2,930 | 2,818 | 2,686 | 2,533 | 2,361 | 2,172 | 1,972 | 1,765 | 10,6          |      |
| 10,8                                                                                                          |                         |       |       |       |       |       |       | 3,329 | 3,286 | 3,237 | 3,179 | 3,112 | 3,033 | 2,940 | 2,829 | 2,700 | 2,551 | 2,382 | 2,196 | 1,998 | 1,793 | 10,8          |      |
| 11,0                                                                                                          |                         |       |       |       |       |       |       |       | 3,289 | 3,240 | 3,184 | 3,118 | 3,040 | 2,948 | 2,840 | 2,714 | 2,567 | 2,401 | 2,218 | 2,023 | 1,819 | 11,0          |      |
| 11,2                                                                                                          |                         |       |       |       |       |       |       |       |       | 3,243 | 3,188 | 3,123 | 3,046 | 2,956 | 2,851 | 2,727 | 2,583 | 2,420 | 2,240 | 2,047 | 1,845 | 11,2          |      |
| 11,4                                                                                                          |                         |       |       |       |       |       |       |       |       |       | 3,191 | 3,128 | 3,053 | 2,964 | 2,861 | 2,739 | 2,598 | 2,438 | 2,261 | 2,070 | 1,870 | 11,4          |      |
| 11,6                                                                                                          |                         |       |       |       |       |       |       |       |       |       |       | 3,195 | 3,132 | 3,058 | 2,972 | 2,870 | 2,751 | 2,613 | 2,456 | 2,281 | 2,093 | 1,895         | 11,6 |

Table B.1 (continued)

| PEARSON CURVES (STANDARDIZED TAILS)                                                                                                       |                         |     |     |     |     |     |     |     |     |     |       |       |       |       |       |       |       |               |
|-------------------------------------------------------------------------------------------------------------------------------------------|-------------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-------|-------|-------|-------|-------|-------|-------|---------------|
| $P_{0,135} \% (0,135 \text{ percentile}) \text{ for } \gamma_1 > 0. P_{99,865} \% (99,865 \text{ percentile}) \text{ for } \gamma_1 < 0.$ |                         |     |     |     |     |     |     |     |     |     |       |       |       |       |       |       |       |               |
| Kurtosis<br>( $\beta_2$ )                                                                                                                 | Skewness ( $\gamma_1$ ) |     |     |     |     |     |     |     |     |     |       |       |       |       |       |       |       |               |
|                                                                                                                                           | 0,0                     | 0,1 | 0,2 | 0,3 | 0,4 | 0,5 | 0,6 | 0,7 | 0,8 | 0,9 | 1,0   | 1,1   | 1,2   | 1,3   | 1,4   | 1,5   | 1,6   | ( $\beta_2$ ) |
| 11,8                                                                                                                                      |                         |     |     |     |     |     |     |     |     |     | 3,137 | 3,064 | 2,979 | 2,879 | 2,762 | 2,627 | 2,473 | 11,8          |
| 12,0                                                                                                                                      |                         |     |     |     |     |     |     |     |     |     | 3,141 | 3,070 | 2,986 | 2,888 | 2,773 | 2,641 | 2,489 | 12,0          |
| 12,2                                                                                                                                      |                         |     |     |     |     |     |     |     |     |     |       | 3,075 | 2,993 | 2,896 | 2,784 | 2,653 | 2,505 | 12,2          |

Table B.2

| PEARSON CURVES (STANDARDIZED TAILS)                                                                           |                         |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |               |
|---------------------------------------------------------------------------------------------------------------|-------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|---------------|
| $P_{99,865\%}$ (99,865 percentile) for $\gamma_1 > 0$ , $P_{0,135\%}$ (0,135 percentile) for $\gamma_1 < 0$ . |                         |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |               |
| Kurtosis<br>( $\beta_2$ )                                                                                     | Skewness ( $\gamma_1$ ) |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       | ( $\beta_2$ ) |
|                                                                                                               | 0,0                     | 0,1   | 0,2   | 0,3   | 0,4   | 0,5   | 0,6   | 0,7   | 0,8   | 0,9   | 1,0   | 1,1   | 1,2   | 1,3   | 1,4   | 1,5   | 1,6   | 1,7   | 1,8   | 1,9   | 2,0   |               |
| -1,4                                                                                                          | 1,512                   | 1,584 | 1,632 | 1,655 | 1,653 | 1,626 | 1,579 | 1,516 |       |       |       |       |       |       |       |       |       |       |       |       |       | -1,4          |
| -1,2                                                                                                          | 1,727                   | 1,813 | 1,871 | 1,899 | 1,895 | 1,861 | 1,803 | 1,726 | 1,636 |       |       |       |       |       |       |       |       |       |       |       |       | -1,2          |
| -1,0                                                                                                          | 1,966                   | 2,065 | 2,134 | 2,170 | 2,169 | 2,131 | 2,061 | 1,966 | 1,856 |       |       |       |       |       |       |       |       |       |       |       |       | -1,0          |
| -0,8                                                                                                          | 2,210                   | 2,320 | 2,400 | 2,446 | 2,454 | 2,422 | 2,349 | 2,241 | 2,108 | 1,965 | 1,822 |       |       |       |       |       |       |       |       |       |       | -0,8          |
| -0,6                                                                                                          | 2,442                   | 2,560 | 2,648 | 2,704 | 2,726 | 2,708 | 2,646 | 2,540 | 2,395 | 2,225 | 2,052 | 1,885 |       |       |       |       |       |       |       |       |       | -0,6          |
| -0,4                                                                                                          | 2,653                   | 2,774 | 2,869 | 2,934 | 2,969 | 2,968 | 2,926 | 2,837 | 2,699 | 2,518 | 2,314 | 2,114 | 1,928 |       |       |       |       |       |       |       |       | -0,4          |
| -0,2                                                                                                          | 2,839                   | 2,961 | 3,060 | 3,133 | 3,179 | 3,194 | 3,173 | 3,109 | 2,993 | 2,824 | 2,608 | 2,373 | 2,152 | 1,952 |       |       |       |       |       |       |       | -0,2          |
| 0,0                                                                                                           | 3,000                   | 3,123 | 3,224 | 3,303 | 3,358 | 3,387 | 3,385 | 3,345 | 3,259 | 3,116 | 2,914 | 2,665 | 2,405 | 2,169 | 1,960 |       |       |       |       |       |       | 0,0           |
| 0,2                                                                                                           | 3,140                   | 3,261 | 3,364 | 3,447 | 3,510 | 3,550 | 3,564 | 3,546 | 3,488 | 3,378 | 3,206 | 2,970 | 2,690 | 2,412 | 2,167 |       |       |       |       |       |       | 0,2           |
| 0,4                                                                                                           | 3,261                   | 3,381 | 3,484 | 3,570 | 3,639 | 3,688 | 3,715 | 3,715 | 3,681 | 3,603 | 3,468 | 3,264 | 2,993 | 2,687 | 2,398 | 2,149 |       |       |       |       |       | 0,4           |
| 0,6                                                                                                           | 3,366                   | 3,485 | 3,588 | 3,676 | 3,749 | 3,805 | 3,843 | 3,858 | 3,844 | 3,793 | 3,693 | 3,529 | 3,290 | 2,984 | 2,658 | 2,366 | 2,119 |       |       |       |       | 0,6           |
| 0,8                                                                                                           | 3,458                   | 3,575 | 3,678 | 3,768 | 3,844 | 3,905 | 3,951 | 3,978 | 3,981 | 3,953 | 3,883 | 3,758 | 3,561 | 3,283 | 2,945 | 2,609 | 2,322 |       |       |       |       | 0,8           |
| 1,0                                                                                                           | 3,539                   | 3,654 | 3,757 | 3,847 | 3,926 | 3,991 | 4,044 | 4,080 | 4,096 | 4,087 | 4,043 | 3,952 | 3,797 | 3,561 | 3,243 | 2,881 | 2,547 | 2,269 |       |       |       | 1,0           |
| 1,2                                                                                                           | 3,611                   | 3,724 | 3,826 | 3,917 | 3,997 | 4,066 | 4,124 | 4,167 | 4,194 | 4,208 | 4,177 | 4,115 | 3,998 | 3,808 | 3,529 | 3,172 | 2,798 | 2,476 |       |       |       | 1,2           |
| 1,4                                                                                                           | 3,674                   | 3,786 | 3,887 | 3,978 | 4,060 | 4,131 | 4,193 | 4,243 | 4,278 | 4,296 | 4,290 | 4,252 | 4,168 | 4,020 | 3,789 | 3,463 | 3,075 | 2,705 | 2,399 |       |       | 1,4           |
| 1,6                                                                                                           | 3,731                   | 3,842 | 3,942 | 4,033 | 4,115 | 4,189 | 4,253 | 4,308 | 4,351 | 4,378 | 4,386 | 4,367 | 4,311 | 4,200 | 4,015 | 3,736 | 3,364 | 2,961 | 2,609 |       |       | 1,6           |
| 1,8                                                                                                           | 3,782                   | 3,891 | 3,990 | 4,081 | 4,164 | 4,239 | 4,307 | 4,365 | 4,414 | 4,449 | 4,468 | 4,472 | 4,431 | 4,352 | 4,209 | 3,979 | 3,646 | 3,238 | 2,840 | 2,511 |       | 1,8           |
| 2,0                                                                                                           | 3,828                   | 3,936 | 4,034 | 4,125 | 4,208 | 4,285 | 4,354 | 4,416 | 4,468 | 4,511 | 4,539 | 4,549 | 4,532 | 4,479 | 4,372 | 4,189 | 3,907 | 3,522 | 3,095 | 2,719 |       | 2,0           |
| 2,2                                                                                                           | 3,870                   | 3,976 | 4,073 | 4,164 | 4,248 | 4,325 | 4,396 | 4,460 | 4,517 | 4,564 | 4,600 | 4,620 | 4,619 | 4,587 | 4,510 | 4,369 | 4,137 | 3,796 | 3,370 | 2,949 | 2,603 | 2,2           |
| 2,4                                                                                                           | 3,908                   | 4,013 | 4,109 | 4,199 | 4,283 | 4,361 | 4,433 | 4,500 | 4,559 | 4,611 | 4,653 | 4,682 | 4,693 | 4,678 | 4,627 | 4,521 | 4,336 | 4,047 | 3,648 | 3,201 | 2,808 | 2,4           |
| 2,6                                                                                                           | 3,943                   | 4,046 | 4,142 | 4,231 | 4,315 | 4,394 | 4,467 | 4,535 | 4,597 | 4,653 | 4,700 | 4,736 | 4,757 | 4,756 | 4,725 | 4,649 | 4,506 | 4,269 | 3,916 | 3,471 | 3,033 | 2,6           |
| 2,8                                                                                                           | 3,975                   | 4,077 | 4,172 | 4,261 | 4,344 | 4,423 | 4,498 | 4,567 | 4,631 | 4,690 | 4,741 | 4,783 | 4,812 | 4,824 | 4,809 | 4,758 | 4,650 | 4,460 | 4,160 | 3,745 | 3,280 | 2,8           |

Table B.2 (continued)

| PEARSON CURVES (STANDARDIZED TAILS)                                                                             |                         |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |               |  |
|-----------------------------------------------------------------------------------------------------------------|-------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|---------------|--|
| $P_{99,865} \%$ (99,865 percentile) for $\gamma_1 > 0$ , $P_{0,135} \%$ (0,135 percentile) for $\gamma_1 < 0$ . |                         |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |               |  |
| Kurtosis<br>( $\beta_2$ )                                                                                       | Skewness ( $\gamma_1$ ) |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |               |  |
|                                                                                                                 | 0,0                     | 0,1   | 0,2   | 0,3   | 0,4   | 0,5   | 0,6   | 0,7   | 0,8   | 0,9   | 1,0   | 1,1   | 1,2   | 1,3   | 1,4   | 1,5   | 1,6   | 1,7   | 1,8   | 1,9   | 2,0   | ( $\beta_2$ ) |  |
| 3,0                                                                                                             | 4,004                   | 4,105 | 4,199 | 4,287 | 4,371 | 4,450 | 4,525 | 4,596 | 4,662 | 4,723 | 4,777 | 4,824 | 4,860 | 4,882 | 4,881 | 4,850 | 4,771 | 4,623 | 4,376 | 4,007 | 3,544 | 3,0           |  |
| 3,2                                                                                                             | 4,031                   | 4,131 | 4,224 | 4,312 | 4,396 | 4,475 | 4,550 | 4,622 | 4,689 | 4,752 | 4,810 | 4,861 | 4,903 | 4,932 | 4,944 | 4,929 | 4,875 | 4,762 | 4,563 | 4,247 | 3,813 | 3,2           |  |
| 3,4                                                                                                             | 4,056                   | 4,155 | 4,247 | 4,335 | 4,418 | 4,498 | 4,573 | 4,645 | 4,714 | 4,779 | 4,839 | 4,893 | 4,940 | 4,976 | 4,997 | 4,996 | 4,963 | 4,880 | 4,723 | 4,461 | 4,072 | 3,4           |  |
| 3,6                                                                                                             | 4,079                   | 4,177 | 4,269 | 4,356 | 4,439 | 4,518 | 4,594 | 4,667 | 4,737 | 4,803 | 4,865 | 4,922 | 4,973 | 5,015 | 5,044 | 5,055 | 5,038 | 4,980 | 4,859 | 4,647 | 4,311 | 3,6           |  |
| 3,8                                                                                                             | 4,101                   | 4,197 | 4,288 | 4,375 | 4,458 | 4,537 | 4,614 | 4,687 | 4,757 | 4,825 | 4,888 | 4,948 | 5,002 | 5,049 | 5,085 | 5,106 | 5,103 | 5,066 | 4,976 | 4,806 | 4,524 | 3,8           |  |
| 4,0                                                                                                             | 4,121                   | 4,217 | 4,307 | 4,393 | 4,476 | 4,555 | 4,631 | 4,705 | 4,776 | 4,845 | 4,910 | 4,972 | 5,029 | 5,080 | 5,122 | 5,150 | 5,159 | 5,139 | 5,075 | 4,943 | 4,712 | 4,0           |  |
| 4,2                                                                                                             | 4,140                   | 4,234 | 4,324 | 4,410 | 4,492 | 4,571 | 4,648 | 4,722 | 4,794 | 4,863 | 4,929 | 4,993 | 5,052 | 5,107 | 5,153 | 5,189 | 5,208 | 5,202 | 5,159 | 5,059 | 4,873 | 4,2           |  |
| 4,4                                                                                                             | 4,157                   | 4,251 | 4,340 | 4,425 | 4,508 | 4,587 | 4,663 | 4,737 | 4,809 | 4,879 | 4,947 | 5,012 | 5,074 | 5,131 | 5,181 | 5,223 | 5,250 | 5,257 | 5,232 | 5,159 | 5,012 | 4,4           |  |
| 4,6                                                                                                             | 4,174                   | 4,267 | 4,355 | 4,440 | 4,522 | 4,601 | 4,677 | 4,752 | 4,824 | 4,895 | 4,963 | 5,029 | 5,093 | 5,152 | 5,207 | 5,253 | 5,288 | 5,305 | 5,295 | 5,244 | 5,131 | 4,6           |  |
| 4,8                                                                                                             | 4,189                   | 4,281 | 4,369 | 4,454 | 4,535 | 4,614 | 4,691 | 4,765 | 4,838 | 4,909 | 4,978 | 5,045 | 5,110 | 5,172 | 5,229 | 5,280 | 5,321 | 5,346 | 5,349 | 5,318 | 5,233 | 4,8           |  |
| 5,0                                                                                                             | 4,204                   | 4,295 | 4,383 | 4,467 | 4,548 | 4,627 | 4,703 | 4,778 | 4,851 | 4,922 | 4,992 | 5,060 | 5,126 | 5,190 | 5,249 | 5,303 | 5,350 | 5,383 | 5,396 | 5,381 | 5,320 | 5,0           |  |
| 5,2                                                                                                             | 4,218                   | 4,308 | 4,395 | 4,479 | 4,560 | 4,638 | 4,715 | 4,789 | 4,862 | 4,934 | 5,004 | 5,073 | 5,141 | 5,206 | 5,267 | 5,325 | 5,376 | 5,415 | 5,437 | 5,436 | 5,395 | 5,2           |  |
| 5,4                                                                                                             | 4,231                   | 4,321 | 4,407 | 4,490 | 4,571 | 4,649 | 4,725 | 4,800 | 4,873 | 4,945 | 5,016 | 5,086 | 5,154 | 5,220 | 5,284 | 5,344 | 5,399 | 5,443 | 5,474 | 5,483 | 5,460 | 5,4           |  |
| 5,6                                                                                                             | 4,243                   | 4,332 | 4,418 | 4,501 | 4,581 | 4,659 | 4,736 | 4,810 | 4,884 | 4,956 | 5,027 | 5,097 | 5,166 | 5,233 | 5,299 | 5,361 | 5,418 | 5,468 | 5,505 | 5,525 | 5,516 | 5,6           |  |
| 5,8                                                                                                             | 4,255                   | 4,343 | 4,429 | 4,511 | 4,591 | 4,669 | 4,745 | 4,820 | 4,893 | 4,966 | 5,037 | 5,108 | 5,177 | 5,246 | 5,312 | 5,376 | 5,436 | 5,491 | 5,533 | 5,561 | 5,565 | 5,8           |  |
| 6,0                                                                                                             | 4,266                   | 4,354 | 4,439 | 4,521 | 4,600 | 4,678 | 4,754 | 4,829 | 4,902 | 4,975 | 5,046 | 5,117 | 5,188 | 5,257 | 5,325 | 5,390 | 5,452 | 5,511 | 5,558 | 5,593 | 5,608 | 6,0           |  |
| 6,2                                                                                                             | 4,276                   | 4,364 | 4,448 | 4,530 | 4,609 | 4,695 | 4,763 | 4,837 | 4,911 | 4,983 | 5,055 | 5,126 | 5,197 | 5,267 | 5,336 | 5,403 | 5,467 | 5,529 | 5,581 | 5,621 | 5,645 | 6,2           |  |
| 6,4                                                                                                             | 4,286                   | 4,373 | 4,457 | 4,538 | 4,618 | 4,703 | 4,771 | 4,845 | 4,919 | 4,991 | 5,063 | 5,135 | 5,206 | 5,276 | 5,346 | 5,414 | 5,480 | 5,542 | 5,600 | 5,646 | 5,678 | 6,4           |  |
| 6,6                                                                                                             | 4,296                   | 4,382 | 4,466 | 4,547 | 4,626 | 4,710 | 4,778 | 4,853 | 4,926 | 4,999 | 5,071 | 5,143 | 5,214 | 5,285 | 5,356 | 5,425 | 5,492 | 5,557 | 5,618 | 5,669 | 5,706 | 6,6           |  |
| 6,8                                                                                                             | 4,305                   | 4,391 | 4,474 | 4,554 | 4,633 | 4,717 | 4,785 | 4,860 | 4,933 | 5,006 | 5,078 | 5,150 | 5,222 | 5,293 | 5,364 | 5,434 | 5,503 | 5,569 | 5,634 | 5,688 | 5,732 | 6,8           |  |
| 7,0                                                                                                             | 4,313                   | 4,399 | 4,481 | 4,562 | 4,640 | 4,724 | 4,792 | 4,867 | 4,940 | 5,013 | 5,085 | 5,157 | 5,229 | 5,301 | 5,372 | 5,443 | 5,513 | 5,581 | 5,648 | 5,706 | 5,754 | 7,0           |  |
| 7,2                                                                                                             | 4,322                   | 4,406 | 4,489 | 4,569 | 4,647 | 4,730 | 4,799 | 4,873 | 4,946 | 5,019 | 5,091 | 5,164 | 5,236 | 5,308 | 5,380 | 5,451 | 5,522 | 5,591 | 5,658 | 5,722 | 5,775 | 7,2           |  |
| 7,4                                                                                                             | 4,330                   | 4,414 | 4,496 | 4,576 | 4,654 | 4,736 | 4,805 | 4,879 | 4,952 | 5,025 | 5,097 | 5,170 | 5,242 | 5,314 | 5,387 | 5,459 | 5,530 | 5,601 | 5,669 | 5,736 | 5,792 | 7,4           |  |

Table B.2 (continued)

| PEARSON CURVES (STANDARDIZED TAILS)                                                                           |                         |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |               |      |
|---------------------------------------------------------------------------------------------------------------|-------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|---------------|------|
| $P_{99,865\%}$ (99,865 percentile) for $\gamma_1 > 0$ , $P_{0,135\%}$ (0,135 percentile) for $\gamma_1 < 0$ . |                         |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |               |      |
| Kurtosis<br>( $\beta_2$ )                                                                                     | Skewness ( $\gamma_1$ ) |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |               |      |
|                                                                                                               | 0,0                     | 0,1   | 0,2   | 0,3   | 0,4   | 0,5   | 0,6   | 0,7   | 0,8   | 0,9   | 1,0   | 1,1   | 1,2   | 1,3   | 1,4   | 1,5   | 1,6   | 1,7   | 1,8   | 1,9   | 2,0   | ( $\beta_2$ ) |      |
| 7,6                                                                                                           | 4,337                   | 4,421 | 4,503 | 4,582 | 4,660 | 4,742 | 4,811 | 4,885 | 4,958 | 5,031 | 5,103 | 5,175 | 5,248 | 5,320 | 5,393 | 5,466 | 5,538 | 5,609 | 5,679 | 5,749 | 5,808 | 7,6           |      |
| 7,8                                                                                                           | 4,344                   | 4,428 | 4,509 | 4,588 | 4,666 | 4,747 | 4,817 | 4,890 | 4,963 | 5,036 | 5,109 | 5,181 | 5,253 | 5,326 | 5,399 | 5,472 | 5,545 | 5,617 | 5,688 | 5,760 | 5,823 | 7,8           |      |
| 8,0                                                                                                           | 4,351                   | 4,434 | 4,515 | 4,594 | 4,672 | 4,753 | 4,822 | 4,896 | 4,969 | 5,041 | 5,114 | 5,186 | 5,259 | 5,331 | 5,404 | 5,478 | 5,551 | 5,624 | 5,696 | 5,771 | 5,836 | 8,0           |      |
| 8,2                                                                                                           | 4,358                   | 4,441 | 4,521 | 4,600 | 4,677 | 4,758 | 4,827 | 4,901 | 4,974 | 5,046 | 5,118 | 5,191 | 5,263 | 5,336 | 5,410 | 5,483 | 5,557 | 5,631 | 5,704 | 5,775 | 5,847 | 8,2           |      |
| 8,4                                                                                                           | 4,365                   | 4,447 | 4,527 | 4,605 | 4,682 | 4,762 | 4,832 | 4,905 | 4,978 | 5,051 | 5,123 | 5,195 | 5,268 | 5,341 | 5,414 | 5,488 | 5,562 | 5,637 | 5,710 | 5,783 | 5,858 | 8,4           |      |
| 8,6                                                                                                           | 4,371                   | 4,452 | 4,532 | 4,611 | 4,687 | 4,767 | 4,837 | 4,910 | 4,983 | 5,055 | 5,127 | 5,200 | 5,272 | 5,345 | 5,419 | 5,493 | 5,567 | 5,642 | 5,717 | 5,790 | 5,867 | 8,6           |      |
| 8,8                                                                                                           | 4,377                   | 4,458 | 4,538 | 4,616 | 4,692 | 4,772 | 4,841 | 4,914 | 4,987 | 5,059 | 5,132 | 5,204 | 5,276 | 5,349 | 5,423 | 5,497 | 5,572 | 5,647 | 5,722 | 5,797 | 5,875 | 8,8           |      |
| 9,0                                                                                                           | 4,382                   | 4,463 | 4,543 | 4,621 | 4,697 | 4,776 | 4,845 | 4,918 | 4,991 | 5,063 | 5,135 | 5,208 | 5,280 | 5,353 | 5,427 | 5,501 | 5,576 | 5,652 | 5,727 | 5,803 | 5,883 | 9,0           |      |
| 9,2                                                                                                           | 4,388                   | 4,468 | 4,548 | 4,625 | 4,701 | 4,780 | 4,850 | 4,923 | 4,995 | 5,067 | 5,139 | 5,211 | 5,284 | 5,357 | 5,431 | 5,505 | 5,580 | 5,656 | 5,732 | 5,808 | 5,883 | 9,2           |      |
| 9,4                                                                                                           | 4,393                   | 4,473 | 4,552 | 4,630 | 4,705 | 4,784 | 4,854 | 4,926 | 4,999 | 5,071 | 5,143 | 5,215 | 5,287 | 5,361 | 5,434 | 5,509 | 5,584 | 5,660 | 5,736 | 5,813 | 5,889 | 9,4           |      |
| 9,6                                                                                                           | 4,398                   | 4,478 | 4,557 | 4,634 | 4,710 | 4,788 | 4,857 | 4,930 | 5,002 | 5,074 | 5,146 | 5,218 | 5,291 | 5,364 | 5,437 | 5,512 | 5,587 | 5,663 | 5,740 | 5,817 | 5,894 | 9,6           |      |
| 9,8                                                                                                           | 4,403                   | 4,483 | 4,561 | 4,638 | 4,714 | 4,791 | 4,861 | 4,934 | 5,006 | 5,078 | 5,149 | 5,222 | 5,294 | 5,367 | 5,440 | 5,515 | 5,590 | 5,667 | 5,744 | 5,821 | 5,898 | 9,8           |      |
| 10,0                                                                                                          | 4,408                   | 4,487 | 4,565 | 4,642 | 4,717 | 4,795 | 4,865 | 4,937 | 5,009 | 5,081 | 5,153 | 5,225 | 5,297 | 5,370 | 5,443 | 5,518 | 5,593 | 5,670 | 5,747 | 5,825 | 5,903 | 10,0          |      |
| 10,2                                                                                                          |                         |       |       |       | 4,721 | 4,798 | 4,868 | 4,940 | 5,012 | 5,084 | 5,156 | 5,228 | 5,300 | 5,373 | 5,446 | 5,521 | 5,596 | 5,673 | 5,750 | 5,828 | 5,906 | 10,2          |      |
| 10,4                                                                                                          |                         |       |       |       |       | 4,871 | 4,943 | 5,015 | 5,087 | 5,158 | 5,230 | 5,303 | 5,375 | 5,449 | 5,523 | 5,599 | 5,675 | 5,753 | 5,831 | 5,910 | 10,4  |               |      |
| 10,6                                                                                                          |                         |       |       |       |       |       | 4,874 | 4,947 | 5,018 | 5,090 | 5,161 | 5,233 | 5,305 | 5,378 | 5,451 | 5,526 | 5,601 | 5,678 | 5,755 | 5,834 | 5,913 | 10,6          |      |
| 10,8                                                                                                          |                         |       |       |       |       |       |       | 4,949 | 5,021 | 5,092 | 5,164 | 5,236 | 5,308 | 5,380 | 5,454 | 5,528 | 5,603 | 5,680 | 5,757 | 5,836 | 5,915 | 10,8          |      |
| 11,0                                                                                                          |                         |       |       |       |       |       |       |       | 5,024 | 5,095 | 5,166 | 5,238 | 5,310 | 5,383 | 5,456 | 5,530 | 5,605 | 5,682 | 5,760 | 5,838 | 5,918 | 11,0          |      |
| 11,2                                                                                                          |                         |       |       |       |       |       |       |       |       | 5,098 | 5,169 | 5,240 | 5,312 | 5,385 | 5,458 | 5,532 | 5,607 | 5,684 | 5,762 | 5,840 | 5,920 | 11,2          |      |
| 11,4                                                                                                          |                         |       |       |       |       |       |       |       |       |       | 5,171 | 5,243 | 5,314 | 5,387 | 5,460 | 5,534 | 5,609 | 5,686 | 5,763 | 5,842 | 5,922 | 11,4          |      |
| 11,6                                                                                                          |                         |       |       |       |       |       |       |       |       |       |       | 5,173 | 5,245 | 5,316 | 5,389 | 5,462 | 5,536 | 5,611 | 5,687 | 5,765 | 5,844 | 5,924         | 11,6 |

Table B.2 (continued)

| PEARSON CURVES (STANDARDIZED TAILS)                                                                             |                         |     |     |     |     |     |     |     |     |     |       |       |       |       |       |       |       |               |
|-----------------------------------------------------------------------------------------------------------------|-------------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-------|-------|-------|-------|-------|-------|-------|---------------|
| $P_{99,865 \%}$ (99,865 percentile) for $\gamma_1 > 0$ , $P_{0,135 \%}$ (0,135 percentile) for $\gamma_1 < 0$ . |                         |     |     |     |     |     |     |     |     |     |       |       |       |       |       |       |       |               |
| Kurtosis<br>( $\beta_2$ )                                                                                       | Skewness ( $\gamma_1$ ) |     |     |     |     |     |     |     |     |     |       |       |       |       |       |       |       |               |
|                                                                                                                 | 0,0                     | 0,1 | 0,2 | 0,3 | 0,4 | 0,5 | 0,6 | 0,7 | 0,8 | 0,9 | 1,0   | 1,1   | 1,2   | 1,3   | 1,4   | 1,5   | 1,6   | ( $\beta_2$ ) |
| 11,8                                                                                                            |                         |     |     |     |     |     |     |     |     |     | 5,247 | 5,318 | 5,391 | 5,464 | 5,538 | 5,613 | 5,689 | 11,8          |
| 12,0                                                                                                            |                         |     |     |     |     |     |     |     |     |     | 5,249 | 5,320 | 5,393 | 5,465 | 5,539 | 5,614 | 5,690 | 12,0          |
| 12,2                                                                                                            |                         |     |     |     |     |     |     |     |     |     |       | 5,322 | 5,394 | 5,467 | 5,541 | 5,616 | 5,692 | 12,2          |

Table B.3

| PEARSON CURVES (STANDARDIZED MEDIAN)                                   |                            |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |                   |       |       |
|------------------------------------------------------------------------|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------------------|-------|-------|
| P <sub>50</sub> % (50 percentile). Change sign for γ <sub>1</sub> > 0. |                            |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |                   |       |       |
| Kurtosis<br>(β <sub>2</sub> )                                          | Skewness (γ <sub>1</sub> ) |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       | (β <sub>2</sub> ) |       |       |
|                                                                        | 0,0                        | 0,1   | 0,2   | 0,3   | 0,4   | 0,5   | 0,6   | 0,7   | 0,8   | 0,9   | 1,0   | 1,1   | 1,2   | 1,3   | 1,4   | 1,5   | 1,6   | 1,7   |                   | 1,8   | 1,9   |
| -1,4                                                                   | 0,000                      | 0,053 | 0,111 | 0,184 | 0,282 | 0,424 | 0,627 | 0,754 |       |       |       |       |       |       |       |       |       |       |                   |       |       |
| -1,2                                                                   | 0,000                      | 0,039 | 0,082 | 0,132 | 0,196 | 0,284 | 0,412 | 0,591 | 0,727 |       |       |       |       |       |       |       |       |       |                   |       |       |
| -1,0                                                                   | 0,000                      | 0,031 | 0,065 | 0,103 | 0,151 | 0,212 | 0,297 | 0,419 | 0,586 |       |       |       |       |       |       |       |       |       |                   |       |       |
| -0,8                                                                   | 0,000                      | 0,026 | 0,054 | 0,085 | 0,123 | 0,169 | 0,231 | 0,317 | 0,439 | 0,598 | 0,681 |       |       |       |       |       |       |       |                   |       |       |
| -0,6                                                                   | 0,000                      | 0,023 | 0,047 | 0,073 | 0,104 | 0,142 | 0,190 | 0,254 | 0,343 | 0,468 | 0,616 | 0,653 |       |       |       |       |       |       |                   |       |       |
| -0,4                                                                   | 0,000                      | 0,020 | 0,041 | 0,064 | 0,091 | 0,122 | 0,161 | 0,212 | 0,280 | 0,375 | 0,504 | 0,633 | 0,616 |       |       |       |       |       |                   |       |       |
| -0,2                                                                   | 0,000                      | 0,018 | 0,037 | 0,058 | 0,081 | 0,108 | 0,141 | 0,183 | 0,237 | 0,311 | 0,413 | 0,542 | 0,638 | 0,574 |       |       |       |       |                   |       |       |
| 0,0                                                                    | 0,000                      | 0,017 | 0,034 | 0,053 | 0,073 | 0,097 | 0,126 | 0,161 | 0,206 | 0,266 | 0,347 | 0,456 | 0,579 | 0,621 | 0,531 |       |       |       |                   |       |       |
| 0,2                                                                    | 0,000                      | 0,015 | 0,032 | 0,049 | 0,068 | 0,089 | 0,114 | 0,145 | 0,183 | 0,233 | 0,299 | 0,388 | 0,501 | 0,605 | 0,582 |       |       |       |                   |       |       |
| 0,4                                                                    | 0,000                      | 0,014 | 0,029 | 0,045 | 0,063 | 0,082 | 0,105 | 0,132 | 0,165 | 0,208 | 0,263 | 0,336 | 0,433 | 0,545 | 0,607 | 0,536 |       |       |                   |       |       |
| 0,6                                                                    | 0,000                      | 0,013 | 0,028 | 0,043 | 0,059 | 0,077 | 0,097 | 0,122 | 0,151 | 0,188 | 0,235 | 0,297 | 0,379 | 0,481 | 0,579 | 0,579 | 0,489 |       |                   |       |       |
| 0,8                                                                    | 0,000                      | 0,013 | 0,026 | 0,040 | 0,055 | 0,072 | 0,091 | 0,113 | 0,140 | 0,172 | 0,213 | 0,266 | 0,336 | 0,425 | 0,527 | 0,590 | 0,533 |       |                   |       |       |
| 1,0                                                                    | 0,000                      | 0,012 | 0,025 | 0,038 | 0,053 | 0,068 | 0,086 | 0,106 | 0,130 | 0,159 | 0,196 | 0,242 | 0,304 | 0,379 | 0,474 | 0,563 | 0,569 | 0,484 |                   |       |       |
| 1,2                                                                    | 0,000                      | 0,011 | 0,024 | 0,036 | 0,050 | 0,065 | 0,082 | 0,100 | 0,122 | 0,148 | 0,181 | 0,222 | 0,274 | 0,341 | 0,426 | 0,520 | 0,576 | 0,524 |                   |       |       |
| 1,4                                                                    | 0,000                      | 0,011 | 0,023 | 0,035 | 0,048 | 0,062 | 0,078 | 0,095 | 0,116 | 0,140 | 0,169 | 0,206 | 0,252 | 0,310 | 0,385 | 0,474 | 0,554 | 0,555 | 0,475             |       |       |
| 1,6                                                                    | 0,000                      | 0,010 | 0,022 | 0,034 | 0,046 | 0,060 | 0,074 | 0,091 | 0,110 | 0,132 | 0,159 | 0,192 | 0,233 | 0,285 | 0,351 | 0,432 | 0,518 | 0,564 | 0,510             |       |       |
| 1,8                                                                    | 0,000                      | 0,010 | 0,021 | 0,032 | 0,044 | 0,057 | 0,072 | 0,087 | 0,105 | 0,126 | 0,151 | 0,180 | 0,217 | 0,264 | 0,323 | 0,396 | 0,480 | 0,549 | 0,540             | 0,461 |       |
| 2,0                                                                    | 0,000                      | 0,009 | 0,020 | 0,031 | 0,043 | 0,055 | 0,069 | 0,084 | 0,101 | 0,120 | 0,143 | 0,171 | 0,204 | 0,246 | 0,299 | 0,365 | 0,443 | 0,521 | 0,552             | 0,494 |       |
| 2,2                                                                    | 0,000                      | 0,009 | 0,020 | 0,030 | 0,042 | 0,054 | 0,067 | 0,081 | 0,097 | 0,115 | 0,137 | 0,162 | 0,193 | 0,231 | 0,279 | 0,338 | 0,410 | 0,488 | 0,544             | 0,522 | 0,445 |
| 2,4                                                                    | 0,000                      | 0,009 | 0,019 | 0,029 | 0,040 | 0,052 | 0,065 | 0,078 | 0,094 | 0,111 | 0,131 | 0,155 | 0,183 | 0,218 | 0,261 | 0,315 | 0,381 | 0,456 | 0,524             | 0,538 | 0,475 |
| 2,6                                                                    | 0,000                      | 0,008 | 0,018 | 0,029 | 0,039 | 0,051 | 0,063 | 0,076 | 0,091 | 0,107 | 0,126 | 0,148 | 0,175 | 0,207 | 0,246 | 0,295 | 0,355 | 0,426 | 0,498             | 0,539 | 0,503 |
| 2,8                                                                    | 0,000                      | 0,008 | 0,018 | 0,028 | 0,038 | 0,049 | 0,061 | 0,074 | 0,088 | 0,104 | 0,122 | 0,143 | 0,167 | 0,197 | 0,233 | 0,278 | 0,333 | 0,398 | 0,470             | 0,526 | 0,522 |

34

34

Table B.3 (continued)

| PEARSON CURVES (STANDARDIZED MEDIAN)                                   |                            |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |      |                   |
|------------------------------------------------------------------------|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|-------------------|
| P <sub>50</sub> % (50 percentile). Change sign for γ <sub>1</sub> > 0. |                            |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |      |                   |
| Kurtosis<br>(β <sub>2</sub> )                                          | Skewness (γ <sub>1</sub> ) |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |      | (β <sub>2</sub> ) |
|                                                                        | 0,0                        | 0,1   | 0,2   | 0,3   | 0,4   | 0,5   | 0,6   | 0,7   | 0,8   | 0,9   | 1,0   | 1,1   | 1,2   | 1,3   | 1,4   | 1,5   | 1,6   | 1,7   | 1,8   | 1,9   | 2,0   |      |                   |
| 7,6                                                                    | 0,000                      | 0,005 | 0,012 | 0,020 | 0,027 | 0,035 | 0,043 | 0,051 | 0,060 | 0,069 | 0,079 | 0,089 | 0,100 | 0,113 | 0,126 | 0,141 | 0,157 | 0,176 | 0,197 | 0,221 | 0,249 | 7,6  |                   |
| 7,8                                                                    | 0,000                      | 0,005 | 0,012 | 0,020 | 0,027 | 0,035 | 0,043 | 0,051 | 0,059 | 0,068 | 0,078 | 0,088 | 0,099 | 0,111 | 0,124 | 0,139 | 0,155 | 0,173 | 0,193 | 0,217 | 0,243 | 7,8  |                   |
| 8,0                                                                    | 0,000                      | 0,005 | 0,012 | 0,019 | 0,027 | 0,034 | 0,042 | 0,050 | 0,059 | 0,068 | 0,077 | 0,087 | 0,098 | 0,110 | 0,123 | 0,137 | 0,153 | 0,170 | 0,190 | 0,213 | 0,238 | 8,0  |                   |
| 8,2                                                                    | 0,000                      | 0,005 | 0,012 | 0,019 | 0,027 | 0,034 | 0,042 | 0,050 | 0,058 | 0,067 | 0,076 | 0,086 | 0,097 | 0,109 | 0,121 | 0,135 | 0,151 | 0,168 | 0,187 | 0,209 | 0,234 | 8,2  |                   |
| 8,4                                                                    | 0,000                      | 0,005 | 0,012 | 0,019 | 0,026 | 0,034 | 0,042 | 0,050 | 0,058 | 0,067 | 0,076 | 0,086 | 0,096 | 0,108 | 0,120 | 0,134 | 0,149 | 0,165 | 0,184 | 0,205 | 0,229 | 8,4  |                   |
| 8,6                                                                    | 0,000                      | 0,005 | 0,012 | 0,019 | 0,026 | 0,034 | 0,041 | 0,049 | 0,057 | 0,066 | 0,075 | 0,085 | 0,095 | 0,107 | 0,119 | 0,132 | 0,147 | 0,163 | 0,181 | 0,202 | 0,225 | 8,6  |                   |
| 8,8                                                                    | 0,000                      | 0,005 | 0,012 | 0,019 | 0,026 | 0,033 | 0,041 | 0,049 | 0,057 | 0,066 | 0,075 | 0,084 | 0,094 | 0,106 | 0,118 | 0,131 | 0,145 | 0,161 | 0,179 | 0,199 | 0,221 | 8,8  |                   |
| 9,0                                                                    | 0,000                      | 0,005 | 0,012 | 0,019 | 0,026 | 0,033 | 0,041 | 0,049 | 0,057 | 0,065 | 0,074 | 0,084 | 0,094 | 0,105 | 0,116 | 0,129 | 0,143 | 0,159 | 0,176 | 0,196 | 0,218 | 9,0  |                   |
| 9,2                                                                    | 0,000                      | 0,005 | 0,012 | 0,019 | 0,026 | 0,033 | 0,040 | 0,048 | 0,056 | 0,065 | 0,073 | 0,083 | 0,093 | 0,104 | 0,115 | 0,128 | 0,142 | 0,157 | 0,174 | 0,193 | 0,214 | 9,2  |                   |
| 9,4                                                                    | 0,000                      | 0,005 | 0,012 | 0,019 | 0,026 | 0,033 | 0,040 | 0,048 | 0,056 | 0,064 | 0,073 | 0,082 | 0,092 | 0,103 | 0,114 | 0,127 | 0,140 | 0,155 | 0,172 | 0,190 | 0,211 | 9,4  |                   |
| 9,6                                                                    | 0,000                      | 0,005 | 0,012 | 0,019 | 0,025 | 0,033 | 0,040 | 0,048 | 0,055 | 0,064 | 0,072 | 0,082 | 0,091 | 0,102 | 0,113 | 0,125 | 0,139 | 0,153 | 0,170 | 0,188 | 0,208 | 9,6  |                   |
| 9,8                                                                    | 0,000                      | 0,005 | 0,012 | 0,018 | 0,025 | 0,032 | 0,040 | 0,047 | 0,055 | 0,063 | 0,072 | 0,081 | 0,091 | 0,101 | 0,112 | 0,124 | 0,137 | 0,152 | 0,168 | 0,185 | 0,205 | 9,8  |                   |
| 10,0                                                                   | 0,000                      | 0,005 | 0,011 | 0,018 | 0,025 | 0,032 | 0,040 | 0,047 | 0,055 | 0,063 | 0,071 | 0,080 | 0,090 | 0,100 | 0,111 | 0,123 | 0,136 | 0,150 | 0,166 | 0,183 | 0,202 | 10,0 |                   |
| 10,2                                                                   | 0,000                      |       |       |       |       | 0,032 | 0,039 | 0,047 | 0,054 | 0,063 | 0,071 | 0,080 | 0,089 | 0,099 | 0,110 | 0,122 | 0,135 | 0,149 | 0,164 | 0,181 | 0,200 | 10,2 |                   |
| 10,4                                                                   | 0,000                      |       |       |       |       | 0,032 | 0,039 | 0,047 | 0,054 | 0,062 | 0,071 | 0,079 | 0,089 | 0,099 | 0,109 | 0,121 | 0,133 | 0,147 | 0,162 | 0,179 | 0,197 | 10,4 |                   |
| 10,6                                                                   | 0,000                      |       |       |       |       | 0,039 | 0,046 | 0,054 | 0,062 | 0,070 | 0,079 | 0,088 | 0,098 | 0,109 | 0,120 | 0,132 | 0,146 | 0,160 | 0,177 | 0,195 |       | 10,6 |                   |
| 10,8                                                                   | 0,000                      |       |       |       |       | 0,046 | 0,054 | 0,061 | 0,070 | 0,078 | 0,087 | 0,097 | 0,108 | 0,119 | 0,131 | 0,144 | 0,159 | 0,175 | 0,192 |       |       | 10,8 |                   |
| 11,0                                                                   | 0,000                      |       |       |       |       | 0,053 | 0,061 | 0,069 | 0,078 | 0,087 | 0,097 | 0,107 | 0,118 | 0,130 | 0,143 | 0,157 | 0,173 | 0,190 |       |       |       | 11,0 |                   |
| 11,2                                                                   | 0,000                      |       |       |       |       | 0,061 | 0,069 | 0,078 | 0,087 | 0,096 | 0,106 | 0,117 | 0,129 | 0,142 | 0,156 | 0,171 | 0,188 |       |       |       |       | 11,2 |                   |
| 11,4                                                                   | 0,000                      |       |       |       |       | 0,069 | 0,077 | 0,086 | 0,095 | 0,105 | 0,116 | 0,128 | 0,141 | 0,154 | 0,169 | 0,186 |       |       |       |       |       | 11,4 |                   |
| 11,6                                                                   | 0,000                      |       |       |       |       | 0,068 | 0,077 | 0,086 | 0,095 | 0,104 | 0,116 | 0,127 | 0,139 | 0,153 | 0,168 | 0,184 |       |       |       |       |       | 11,6 |                   |