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Hydraulic fluid power — Test code for determination of airborne noise levels —

Part 1: Pumps

*Transmissions hydrauliques — Code d'essai pour la détermination du
niveau de bruit aérien —*

Partie 1: Pompes



Reference number
ISO 4412-1:1991(E)

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Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

Draft International Standards adopted by the technical committees are circulated to the member bodies for voting. Publication as an International Standard requires approval by at least 75 % of the member bodies casting a vote.

International Standard ISO 4412-1 was prepared jointly by Technical Committees ISO/TC 131, *Fluid power systems*, Sub-Committee SC 8, *Product testing and contamination control* and ISO/TC 43, *Acoustics*.

This second edition cancels and replaces the first edition (ISO 4412-1:1979), of which clauses 12 and 13 have been transferred to form a new annex A. The former annex A has become annex B, and annexes C and D have been added.

ISO 4412 consists of the following parts, under the general title *Hydraulic fluid power — Test code for determination of airborne noise levels*:

- Part 1: Pumps
- Part 2: Motors
- Part 3: Pumps — Method using a parallelepiped microphone array

Annexes A and B form an integral part of this part of ISO 4412. Annexes C and D are for information only.

Introduction

In hydraulic fluid power systems, power is transmitted and controlled through a liquid under pressure in a closed circuit. Pumps are components which convert rotary mechanical power into fluid power. During the process of converting mechanical power into hydraulic fluid power, airborne noise, fluid-borne vibrations and structure-borne vibrations are radiated from the pump.

The airborne noise level of a hydraulic fluid power pump is an important consideration in component selection. The noise measurement technique must, therefore, be such as to yield accurate appraisals of these airborne noise levels. The determination of noise levels is complicated by the interactions which occur during noise measurements. The fluid-borne and structure-borne vibrations from the pump can be transmitted to the circuit and ultimately give rise to background airborne noise levels which could affect the determination of the pump airborne noise levels.

The procedures described in this part of ISO 4412 are intended to measure only the airborne noise radiated directly from the pump under test.

Hydraulic fluid power — Test code for determination of airborne noise levels —

Part 1: Pumps

1 Scope

This part of ISO 4412 establishes a test code describing procedures, based on ISO 2204, for the determination of the sound power levels of a hydraulic fluid power pump, under controlled conditions of installation and operation, suitable for providing a basis for comparing the noise levels of pumps in terms of:

- A-weighted sound power level;
- octave band sound power levels.

From these sound power levels, if required, reference sound pressure levels may be calculated for reporting purposes in accordance with annex A.

For general purposes, the frequency range of interest includes the octave bands with centre frequencies between 125 Hz and 8 000 Hz.¹⁾

Guidelines for the application of this part of ISO 4412 are given in annex C.

This part of ISO 4412 is applicable to all types of hydraulic fluid power pumps operating under steady-state conditions, irrespective of size, except for any limitations imposed by the size of the test environment (see clause 5).

2 Normative references

The following standards contain provisions which, through reference in this text, constitute provisions of this part of ISO 4412. At the time of publication, the editions indicated were valid. All standards are subject to revision, and parties to agreements based

on this part of ISO 4412 are encouraged to investigate the possibility of applying the most recent editions of the standards indicated below. Members of IEC and ISO maintain registers of currently valid International Standards.

ISO 3448:1975, *Industrial liquid lubricants — ISO viscosity classification*.

ISO 3744:1981, *Acoustics — Determination of sound power levels of noise sources — Engineering methods for free-field conditions over a reflecting plane*.

ISO 3745:1977, *Acoustics — Determination of sound power levels of noise sources — Precision methods for anechoic and semi-anechoic rooms*.

ISO 5598:1985, *Fluid power systems and components — Vocabulary*.

ISO 6743-4:1982, *Lubricants, industrial oils and related products (class L) — Classification — Part 4: Family H (Hydraulic systems)*.

IEC 50(801):1984, *International Electrotechnical Vocabulary — Chapter 801: Acoustics and electroacoustics*.

IEC 651:1979, *Sound level meters*.

3 Definitions

For the purposes of this part of ISO 4412, the definitions given in ISO 5598, IEC 50 and the following definitions apply. It is accepted that the latter definitions may differ from those in other specific International Standards.

1) 1 Hz = 1 s⁻¹

3.1 free sound field: Sound field in a homogeneous, isotropic medium free of boundaries.

NOTE 1 In practice, it is a field in which the effects of the boundaries are negligible over the frequency range of interest.

3.2 free field over a reflecting plane: Field produced by a source in the presence of one reflecting plane on which the source is located.

3.3 reverberant sound field: That portion of the sound field in a test room over which the influence of sound received directly from the source is negligible.

3.4 anechoic room: Test room having boundaries which absorb essentially all of the incident sound energy over the frequency range of interest, thereby affording free-field conditions over the measurement surface.

3.5 mean-square sound pressure: The sound pressure averaged in space and time on a mean-square basis.

NOTE 2 In practice, this is estimated by space and time averaging over a finite path length or over a number of fixed microphone positions.

3.6 mean sound pressure level: Ten times the logarithm to the base 10 of the ratio of the mean-square sound pressure to the square of the reference sound pressure, in decibels (dB).

NOTE 3 The weighting network or the width of the frequency band used should always be indicated; for example, A-weighted sound pressure level, octave band sound pressure level. The reference sound pressure is $20 \mu\text{Pa}$ ²⁾.

3.7 sound power level: Ten times the logarithm to the base 10 of the ratio of a given sound power to the reference sound power, in decibels.

NOTE 4 The weighting network or the width of the frequency band used should always be indicated. The reference sound power is 1 pW ³⁾.

3.8 volume of source under test: Volume of the envelope of the whole pump under test.

4 Measurement uncertainty

Methods of measurement should be used which tend to result in standard deviations which are equal to or less than those specified in table 1. Methods given in ISO 3744 meet this requirement.

2) $1 \mu\text{Pa} = 10^{-6} \text{ N/m}^2$

3) $1 \text{ pW} = 10^{-12} \text{ W}$

Table 1 — Standard deviation of sound power level determinations

Standard deviation, dB, for octave bands centred on:				
125 Hz	250 Hz	500 Hz	1 000 Hz to 4 000 Hz	8 000 Hz
5,0	3,0	2,0	2,0	3,0

The standard deviations given in table 1 include the effects of allowable variations in the positioning of the measurement points and in the selection of any prescribed measurement surface, but exclude variations in the sound power output of the source from test to test.

NOTE 5 The A-weighted sound power level will in most practical cases be determined with a standard deviation of approximately 2 dB.

5 Test environment

Tests shall be conducted in an environment which provides "free-field over a reflecting plane" conditions which meet the environmental qualification requirements described in ISO 3744:1981, clause 4 and annex A.

For more precise measurements, conduct tests in accordance with ISO 3745.

6 Instrumentation

6.1 The instrumentation used to measure fluid flow, fluid pressure, pump speed and fluid temperature shall be in accordance with the recommendations for "industrial class" accuracy of testing; i.e. class C given in annex B.

6.2 The instrumentation used for acoustical measurements shall be in accordance with IEC 651. This instrumentation shall be in accordance with ISO 3744 for both performance and calibration; i.e. type 2 instruments for engineering (grade 2) measurements.

7 Installation conditions

7.1 Pump location

The pump may be located in any position consistent with the source installation and measurement surface (or microphone traverse) requirements specified in ISO 3744 for the test environment being used.

7.2 Pump mounting

7.2.1 The pump mounting shall be constructed so that it will minimize the noise radiated by the mounting as a result of pump vibrations.

7.2.2 The mounting bracket shall be constructed of high-damping material or with sound-damping and sound-insulating material applied to the bracket as required.

7.2.3 Vibration isolation techniques, if needed, shall be used even if the pump is usually securely mounted.

7.2.4 Flange mountings that are as small as practical shall be used so as to minimize interference with radiation of sound towards the shaft end of the pump.

7.3 Pump drive

The drive motor shall be located outside the test space and the pump shall be driven through flexible couplings and an intermediate shaft, or the motor shall be isolated in an acoustic enclosure.

7.4 Hydraulic circuit

7.4.1 The circuit shall include all oil filters, oil coolers, reservoirs and restrictor valves as required to meet the pump hydraulic operating conditions (see clause 8).

7.4.2 The test fluid and degree of filtration shall be in accordance with the pump manufacturer's recommendations.

7.4.3 Inlet and discharge lines shall be installed with diameters in accordance with the manufacturers' recommended practice. Extra care shall be exercised when assembling inlet lines to prevent air leaking into the circuit.

7.4.4 The inlet pressure gauge shall be mounted at the same height as the inlet fittings or it shall be calibrated for any height difference.

7.4.5 The length of line between the pump and the load valve shall be selected in order to minimize the effect of standing waves in the discharge line which can increase the sound radiated from the pump. At

least 15 m of hose shall be used to meet this requirement.

7.4.6 A stable load valve shall be used.

NOTE 6 Unstable load valves in the discharge line can generate and transmit noise through the fluid and piping which can emerge as airborne sound at the pump.

7.4.7 The load valve shall be positioned far from the pump, preferably outside the test room, to minimize the interaction. The load valve shall be located close to the pump only when adequate control of its acoustic performance can be provided.

7.4.8 All fluid lines and load valves in the test space shall be wrapped with sound-isolating materials, if required (see 10.1). Material having a sound-transmission loss of at least 10 dB at 125 Hz, and a greater loss at higher frequencies, shall be used.

8 Operating conditions

8.1 Determine the sound power levels of the pump (see annex A) for any desired set of operating conditions (see 11.3.7).

8.2 These test conditions shall be maintained throughout the test within the limits given in table 2.

Table 2 — Allowable variations of mean indicated values of controlled parameters

Test parameter	Allowable variation
Flow	$\pm 2 \%$
Pressure	$\pm 2 \%$
Speed	$\pm 2 \%$
Temperature	$\pm 2 ^\circ\text{C}$

8.3 The pump shall be tested in the "as-delivered" condition with any ancillary pumps and valves operating normally during the test, so as to include their noise contributions to the airborne noise level of the pump.

9 Location and number of sound measurement points

The location and number of measurement points shall be as required by ISO 3744 for the method of measurement selected for the pump noise test.

10 Test procedure

10.1 Background noise measurements

10.1.1 Measure the background noise of interest that is present during the pump noise test which does not emanate from the pump itself.

Over the frequency range of interest, the band sound pressure levels of this background noise shall be at least 6 dB below the pump band sound pressure levels at each measurement point.

10.1.2 Correct for this background noise, if evidenced by these measurements, by applying the corrections for this purpose given in ISO 3744.

10.1.3 When measurement of band levels of background noise is not practical, the A-weighted background sound level of each measurement point shall be at least 6 dB below the pump A-weighted sound level.

Correct these A-weighted measurements for background noise.

NOTES

7 Easing the requirements for background noise levels can lead to an overestimate of the pump band sound pressure levels.

8 The A-weighted background sound level at each measurement point may be checked by covering the pump with sound-insulating materials capable of a transmission loss of at least 10 dB over the frequency range which is "determining" the A-weighted sound level of the pump.

10.1.4 If the background level is found to be too high, check for further noise control of the pump mounting, drive or hydraulic circuit, as indicated.

10.1.5 Ensure that the orientation of the microphone and the period of observation are as specified in ISO 3744.

10.2 Pump measurements

10.2.1 Measurement sequence

Prior to commencement of a series of tests, operate the pump for a sufficient time to purge air from the system and to stabilize all variables, including fluid condition, to within the limits specified in table 2.

Measure the following for each test:

- a) pump speed and flow rate;
- b) fluid temperature and pressure at pump inlet and fluid pressure at discharge fittings or at the test point provided by the pump manufacturer;
- c) band sound pressure levels at each measurement point over the frequency range of interest;
- d) A-weighted sound pressure level at each measurement point.

10.2.2 New or rebuilt pumps

10.2.2.1 Repeat the initial pump measurement test of the series at the end of a test series or after 1 h of testing.

10.2.2.2 If the A-weighted sound level at any selected measurement point does not duplicate that of the first test within 2 dB (A), the whole test series shall be invalidated.

11 Information to be recorded

11.1 Specifications

The information given in 11.2 and 11.3 shall be compiled and recorded for all measurements made according to the requirements of this part of ISO 4412.

11.2 General information

- a) name and address of the pump manufacturer and, if applicable, the user;
- b) reference number(s) for identification of the pump;
- c) name and address of persons or organization responsible for the acoustic tests on the pump;
- d) date and place of acoustic tests;
- e) statement that the sound power levels of the pump have been obtained in full conformance with this part of ISO 4412 and ISO 3744 for the determination of sound power levels of noise sources (see also clause 13).

11.3 Pump under test

11.3.1 Description of pump

- a) type of pump (e.g. gear or piston), including ancillary equipment;

- b) type of displacement (e.g. fixed or variable);
- c) pump overall linear dimensions (with sketch if necessary);
- d) pump maximum displacement;
- e) type of displacement controller and setting.

11.3.2 Acoustic environment for tests

- a) internal dimensions of the test room and the type of acoustic field for the measurements (e.g. free field over a reflecting plane);
- b) the acoustical treatment of the test room;
- c) the date of measurement;
- d) ambient air temperature (in degrees Celsius), relative humidity (in percentage) and barometric pressure (in pascals⁴⁾;
- e) results of acoustical qualification of test environments as required by clause 5.

11.3.3 Reference sound source (when applicable)

- a) manufacturer, type and serial number;
- b) sound power level calibration data, including name of calibrating laboratory and date of calibration.

11.3.4 Mounting and installation conditions of pump

- a) description of pump mounting conditions;
- b) nature and characteristics of the hydraulic circuit and details of any acoustic insulation treatment;
- c) nature and description of other machines being used which could have an influence on the measured sound pressure levels of the pump.

11.3.5 Location of pump in test environment

11.3.5.1 Include a sketch showing the location of the pump in relation to walls, floor and ceiling of the test room.

11.3.5.2 Show on this sketch the location of other reflecting or absorbing screens and noise sources which can influence measurements.

11.3.6 Instrumentation

- a) details of equipment used to monitor pump operating conditions (see 11.3.7), including type, serial number and manufacturer;
- b) details of equipment used for acoustic measurements including name, type, serial number and manufacturer;
- c) bandwidth of frequency analyser;
- d) overall frequency response of instrumentation system and date and method of calibration;
- e) method of calibration of microphones and date and place of calibration.

11.3.7 Pump operating conditions

Include the following details for each test:

- a) full description of fluid, including classification in accordance with ISO 6743-4;
- b) fluid viscosity classification in accordance with ISO 3448, in centistokes or in square millimetres per second⁵⁾;
- c) shaft speed, in revolutions per minute;
- d) inlet pressure, in megapascals (bars⁶⁾);
- e) outlet pressure, in megapascals (bars);
- f) pump delivery (flow) either measured or calculated, in litres per minute;
- g) temperature of fluid at pump inlet, in degrees Celsius.

11.3.8 Acoustical data

Include all data as required by ISO 3744.

4) 1 Pa = 10^{-5} bar

5) 1 cSt = 1 mm²/s

6) 1 bar = 10⁵ N/m² = 10⁵ Pa = 0,1 MPa

12 Test report

The test report shall contain the following information:

- a) the A-weighted sound power level and octave band sound power levels for each frequency band of interest for each set of operating conditions;
- b) a statement that the sound power levels have been obtained in full conformance with the procedures of this part of ISO 4412 and specific

paragraphs of ISO 3744 for the determination of sound power levels of noise sources.

13 Identification statement (Reference to this part of ISO 4412)

Use the following statement in test reports, catalogues and sales literature when electing to comply with this part of ISO 4412:

"Airborne noise levels determined in accordance with ISO 4412-1, *Hydraulic fluid power — Test code for determination of airborne noise levels — Part 1: Pumps*".

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Annex A (normative)

Calculation of sound levels

A.1 Calculation of pump mean sound pressure levels and sound power levels

A.1.1 Refer to ISO 3744 for information regarding corrections to be applied and the method of calculating the mean levels and the pump sound power levels.

A.1.2 Correct the measured band sound pressure levels (and A-weighted sound levels, where appropriate) at each measurement position for the measured background noise (background noise corrections).

A.1.3 Use these corrected levels to calculate the pump mean band sound levels and mean A-weighted sound level.

A.1.4 Calculate the pump sound power level from these mean sound pressure levels, taking into account any correction for unwanted environmental reflections (environmental correction factor).

A.2 Calculation of mean sound pressure level at a reference distance

The mean sound pressure level at a distance r , in metres, from the equivalent point source radiating into a free field over a reflecting plane (hemispherical radiation) from the calculated pump sound power level is evaluated as follows:

$$\bar{L}_p = L_w - 10 \log[2\pi r^2 / S_0]$$

where

$\bar{L}_p$ is the mean sound pressure level, A-weighted or in bands, in decibels (reference: 20 μ Pa);

L_w is the A-weighted or band power level of the pump under test, in decibels (reference: 1 pW);

$2\pi r^2$ is the area of the hemisphere, in square metres, of radius r ;

$S_0 = 1 \text{ m}^2$.

For calculation purposes, choose a reference distance of $r = 1 \text{ m}$, in which case the numerical value of $\bar{L}_p$ is obtained by subtracting 8 dB from the numerical value of the calculated sound power level, L_w .

Annex B (normative)

Errors and classes of measurement

B.1 Classes of measurement

Depending on the accuracy required, the tests may be carried out to one of three classes of measurement, A, B or C. The classes of measurement shall be agreed between the parties concerned. The use of class A and B is restricted to special cases when there is a need to have the performance more precisely defined. Class A and B tests require more accurate apparatus and methods, which may increase the costs of such tests.

B.2 Errors

Any device or method which by calibration or comparison with International Standards has been demonstrated to be capable of measuring with systematic errors not exceeding the limits given in table B.1 may be used.

Table B.1 — Permissible systematic errors of measuring instruments as determined during calibration

Class of measurement	Units	A	B	C
Input signal	%	$\pm 0,5$	$\pm 1,5$	$\pm 2,5$
Flow	%	$\pm 0,5$	$\pm 1,5$	$\pm 2,5$
Pressure	%	$\pm 0,5$	$\pm 1,5$	$\pm 2,5$
Temperature	$^{\circ}\text{C}$	$\pm 0,5$	$\pm 1,0$	$\pm 2,0$
Speed	%	$\pm 0,5$	$\pm 1,0$	$\pm 2,0$
NOTE — The percentage limits given are of the value of the quantity being measured and not of the maximum values of the test or the maximum reading of the instrument.				

Annex C (informative)

Guidelines for the application of this part of ISO 4412

C.1 Introduction

This annex describes a series of recommended techniques that are designed to enable reliable measurements of hydraulic pump airborne noise to be taken, using an anechoic chamber, in accordance with this part of ISO 4412.

C.2 General

This annex should be read in conjunction with ISO 2204 and ISO 3744.

The principle of this part of ISO 4412 is based on measurements taken over a hemispherical surface centred over the pump unit under test. It does, however, present certain operational difficulties. The methods outlined in this annex represent a practical solution to these problems and allow compliance with the requirements of this part of ISO 4412.

In a hydraulic installation, the vibrational energy of the pump becomes distributed among other components in the system, such as the connecting pipe-work, the pump mounting, the drive shaft and the prime mover. This distribution of energy is a characteristic of the particular installation and is not inherently a measure of pump noise. The pump, however, produces sound energy which can cause the installation as a whole to emit noise. Figure C.1 illustrates the mechanism. It is the objective of this annex to ensure that the measured noise is that radiated by the external casing of the pump and nothing else. This component of noise will then be genuinely a characteristic of the pump and as little affected as possible by the particular installation.

The total airborne noise of a practical installation includes radiation from all the components of the hydraulic system. These are excited, in the main, by pump-generated fluid-borne noise (pressure ripple) present in the circuit and by structural transmission of vibration from the pump to attached components.

These mechanisms may well predominate in the generation of total system noise. It is found, however, that low airborne noise radiation from the pump casing tends to be associated with low fluid-borne and structural noise generation. The values obtained for airborne noise radiation from the casing of a pump may thus be taken as an indication,

but not an exact measure, of its overall acoustic performance.

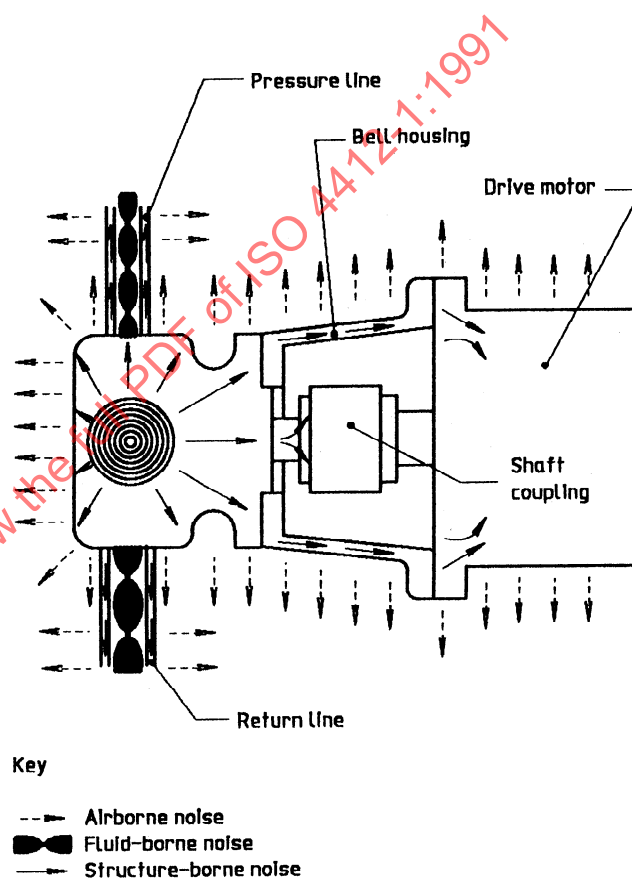


Figure C.1 — Transmission paths of sound energy from pumps

C.3 Choice of measurement environment

This part of ISO 4412 permits measurement in a reverberant or an anechoic room. The anechoic room may take the form of a fully free-field environment or a free field over a single reflecting plane, termed a "semi-anechoic chamber".

An anechoic or semi-anechoic room is normally preferable for pump testing work because there are fewer measurement uncertainties associated with the strongly periodic noise typically radiated by pumps. Anechoic or semi-anechoic environments

also allow directivity information to be obtained which, though not required by this part of ISO 4412, can provide valuable assistance when setting up a system or diagnosing pump acoustic output.

Although a reverberant room is the least affected by accidental oil spillage, the acoustic advantages of an anechoic or semi-anechoic room are frequently more important. Oil spillage in a semi-anechoic room is less serious than in a fully anechoic room if the floor is used as the reflecting plane.

The following discussion relates only to the use of anechoic or semi-anechoic test environments.

C.4 Measurement techniques

C.4.1 Microphones

High-quality condenser microphones, complying with the requirements of the appropriate International Standards listed in ISO 3744 are required to measure the sound pressure levels in the anechoic chamber. The profile of the microphones, connecting leads and support frame should be minimized to reduce interference with the sound field. The sound level meter is placed outside the chamber, and is connected to the microphone via a pre-amplifier and extension lead. A typical set-up, with two microphones connected via a common power supply, is shown in figure C.2.

C.4.2 Number and position of microphones

In order to obtain a valid estimate of the mean sound pressure, the sound field has to be sampled at several points over the measurement surface. A basic array of 10 points is called for, but this number may be reduced if experience shows that the sound field is sufficiently symmetrical for the resultant loss in accuracy not to give errors greater than 1 dB when compared with data obtained using the full array.

As a guide, use at least as many microphones as there is difference between the lowest and highest sound pressure levels, in decibels, recorded on the individual microphones.

Each sampling point should be associated with an equal area of the measurement surface and should be placed in a sequence that minimizes the effect of interference patterns. ISO 3744 gives relative co-ordinates and preferred radii for suitable hemispherical arrays. Sources with the dimensions of a normal fluid power pump usually require a measurement radius of 1 m. Avoid microphone positions close to necessary ancillary equipment such as the pump drive shaft and fluid lines, and ensure that, as far as possible, each microphone has a clear "line of sight" to the pump under test.

It is possible to use a single microphone, moving it to each sampling point in sequence, but it is usually more economic to invest in one microphone channel per measurement point.

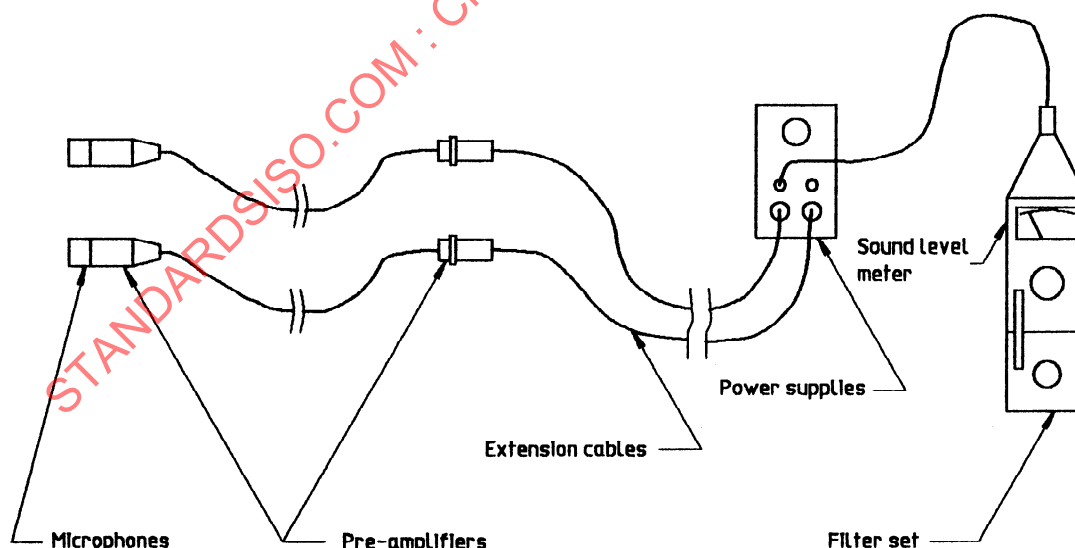


Figure C.2 — Instrumentation for manual data logging

C.4.3 Calculation of mean sound pressure

The mean sound pressure can be calculated from equations 1 and 2 in ISO 3744:1981.

C.4.4 Recording instruments

The microphones may be directly connected to individual sound level meters, but this is a rather uneconomic use of expensive equipment. Used in conjunction with microphone power supplies, which allow individual microphone gain adjustment, each channel may be fed into a single meter via a manual selector switch.

Either technique involves a considerable amount of manual data logging. For example, 168 data records are required to obtain a one-third octave spectrum

from an eight-microphone array covering the range 100 Hz to 10 kHz. If directivity information is not required, it is possible to multiplex the channels into a time-integrating r.m.s. meter. The maximum scan speed is limited by the lowest frequency of interest. Normally a scan speed of 10 channels per second is satisfactory for frequencies of 100 Hz and above.

The scanning device has to operate with very low level switching transients if the background electronic noise is not to influence the sound signal. A typical set-up is shown in figure C.3. This arrangement can be used in conjunction with octave or one-third octave filter sets as well as the weighting networks built into the sound level meter. Comparisons between individually logged data channels and scanned data using the equipment shown in figure C.3 show very good agreement above the 100 Hz one-third octave band.

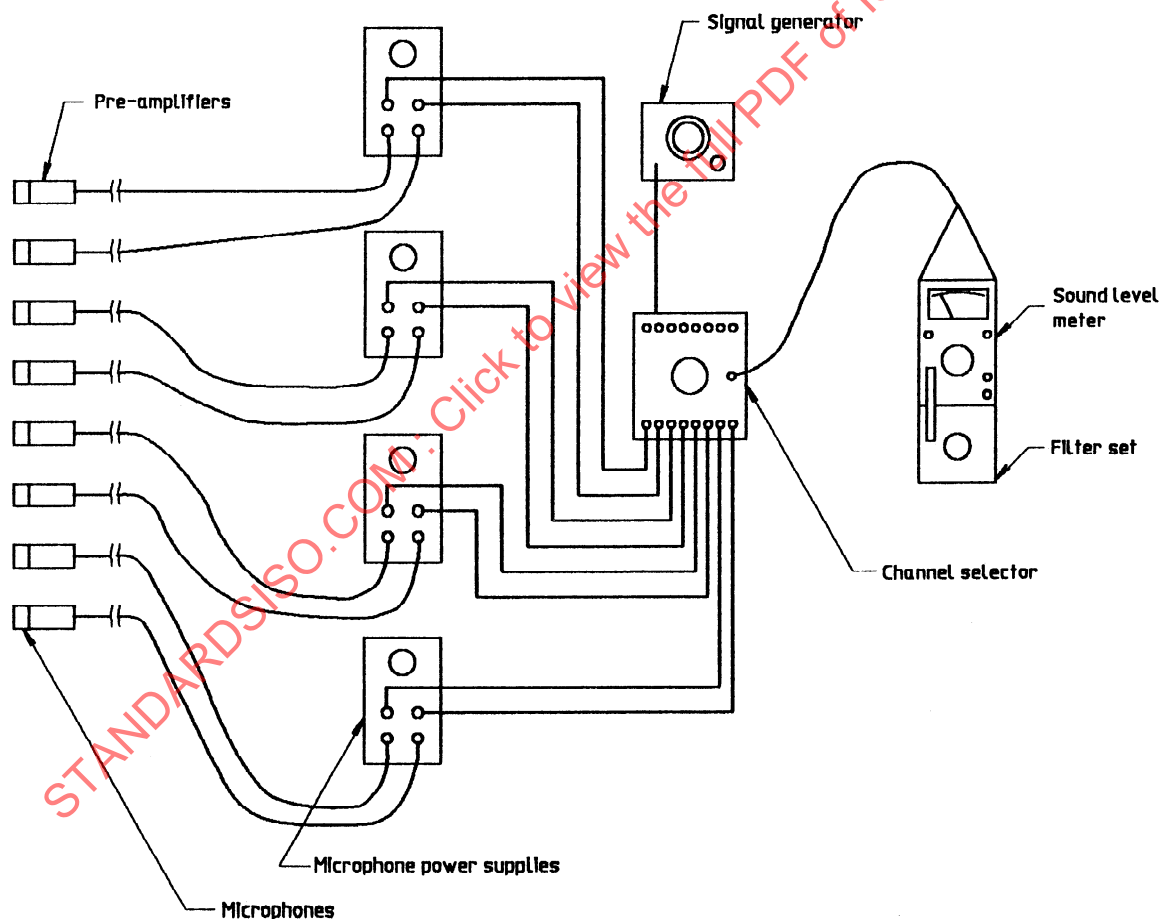


Figure C.3 — Multiple microphone scanning instrumentation

C.4.5 Calculation of sound power level

The sound power level can be calculated from equation 3 in ISO 3744:1981.

Assuming a measurement radius of 1 m, the correction for free-field conditions (i.e. fully anechoic) is + 11 dB. The correction for a free field over a reflecting plane, as required by this part of ISO 4412, is + 8 dB. It is recommended that, whenever possible, the sound field be calibrated by placing a standard sound source at the position normally occupied by the pump, with pump drive shaft and fluid lines in position. Significant variation from the + 8 dB correction may indicate excessive distortion of the sound field by pump ancillaries, inadequate reflecting plane, or some other problem.

C.4.6 Frequency analysis

The response of the human ear is very dependent on the frequency as well as the amplitude of sound. Microphones complying with the requirements of IEC 561 have a linear response to sound pressure from 10 Hz to 20 kHz. In order to model the physiological effect of sound, a frequency-weighting filter is built into sound level meters. This weighting is termed the "A scale" and overall sound levels are measured in terms of decibels (A). This single figure rating is the common basis for rating sound levels. If more information is required about the spectral content of the sound, octave or one-third octave filters are used to give low resolution frequency analysis.

For diagnostic and development work, a higher resolution frequency analysis may be required to help identify particular noise sources or pathways. The two basic forms of narrow-band frequency analysers are analog filters or digital Fourier analysers. The analog filters are rapidly becoming obsolete with the availability of hard-wired dedicated digital Fourier analysers, made possible by advances in micro-electronics. An alternative to the dedicated digital analyser is a minicomputer which, although slower in operation, retains the high degree of flexibility of its associated software.

A detailed description of this equipment is outside the scope of this part of ISO 4412.

C.4.7 Background noise

The airborne noise from the pump under test has to be the dominant component of the noise reaching the microphones. Other noise sources, from both inside and outside the chamber, cannot be completely eliminated but the effect of the unwanted

additional noise becomes insignificant if this background level is more than 10 dB below the measured total noise. If the difference is less than 10 dB but more than 6 dB, corrections can be made to the measured level to take this into account.

In the case where the background noise is 6 dB or less below the measured total noise, the requirements of this part of ISO 4412 are not satisfied, although an estimate of the pump noise can still be made. Figure C.4 shows the relationship between the correction and the background noise margin.

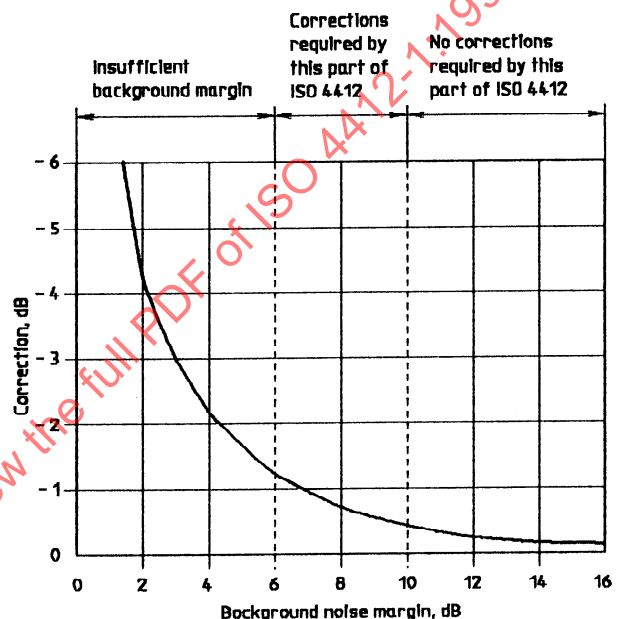


Figure C.4 — Corrections for background noise

The background noise level may be determined by running the pump under test conditions and measuring the noise level. An acoustic cover is then placed over the pump and the noise measurements repeated. The performance of the cover has to be sufficient to attenuate substantially the noise emitted by the pump itself, so that the measured noise with the cover in place is dominated by background noise sources. The cover should mask only the pump itself, and not cover the cladding over the drive shaft or fluid lines, as these might be contributing to the unwanted background noise. It is normally difficult to devise a pump cover that shrouds the entire pump when mounted according to this part of ISO 4412 without also partially covering the pump mount. This is acceptable only if the mount is known to produce a negligible contribution to overall sound level (see C.5.2).