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## Thermoplastics pipes — Determination of ring stiffness

*Tubes en matières thermoplastiques — Détermination de la  
rigidité annulaire*

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## Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

The procedures used to develop this document and those intended for its further maintenance are described in the ISO/IEC Directives, Part 1. In particular the different approval criteria needed for the different types of ISO documents should be noted. This document was drafted in accordance with the editorial rules of the ISO/IEC Directives, Part 2 (see [www.iso.org/directives](http://www.iso.org/directives)).

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. ISO shall not be held responsible for identifying any or all such patent rights. Details of any patent rights identified during the development of the document will be in the Introduction and/or on the ISO list of patent declarations received (see [www.iso.org/patents](http://www.iso.org/patents)).

Any trade name used in this document is information given for the convenience of users and does not constitute an endorsement.

For an explanation on the meaning of ISO specific terms and expressions related to conformity assessment, as well as information about ISO's adherence to the WTO principles in the Technical Barriers to Trade (TBT) see the following URL: [Foreword - Supplementary information](#)

The committee responsible for this document is ISO/TC 138, *Plastics pipes, fittings and valves for the transport of fluids*, Subcommittee SC 5, *General properties of pipes, fittings and valves of plastic materials and their accessories — Test methods and basic specifications*.

This third edition cancels and replaces the second edition (ISO 9969:2007), which has been technically revised.

# Thermoplastics pipes — Determination of ring stiffness

## 1 Scope

This International Standard specifies a test method for determining the ring stiffness of thermoplastics pipes having a circular cross section.

## 2 Normative references

The following documents, in whole or in part, are normatively referenced in this document and are indispensable for its application. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 3126, *Plastics piping systems — Plastics components — Determination of dimensions*

## 3 Symbols

For the purposes of this document, the following symbols apply.

|       |                                           | Units             |
|-------|-------------------------------------------|-------------------|
| $d_n$ | nominal diameter of pipe                  | mm                |
| $d_i$ | inside diameter of the test piece of pipe | mm                |
| $e_c$ | construction height                       | mm                |
| $F$   | loading force                             | kN                |
| $F_0$ | pre-load force                            | N                 |
| $L$   | length of test piece                      | mm                |
| $p$   | pitch of ribs or windings                 | mm                |
| $S$   | ring stiffness                            | kN/m <sup>2</sup> |
| $y$   | vertical deflection                       | mm                |

## 4 Principle

The ring stiffness is determined by measuring the force and the deflection while deflecting the pipe at a constant deflection speed.

A cut length of pipe supported horizontally is compressed vertically between two parallel flat plates moved at a constant speed that is dependent upon the diameter of the pipe.

A plot of force versus deflection is generated. The ring stiffness is calculated as a function of the force necessary to produce a 3 % diametric deflection of the pipe.

NOTE It is assumed that the test temperature is set by the referring standard, if appropriate (see 8.1).

## 5 Apparatus

**5.1 Compressive testing machine**, capable of a constant rate of crosshead movement, via a pair of parallel plates (5.2), as appropriate to the nominal diameter of the pipe in conformance with Table 1, with sufficient force and travel to produce the specified diametric deflection (see Clause 8).

**Table 1 — Deflection speeds**

| Inside diameter, $d_i$ , of the test piece of pipe<br>mm | Deflection speed<br>mm/min |
|----------------------------------------------------------|----------------------------|
| $d_i \leq 100$                                           | $2 \pm 0,1$                |
| $100 < d_i \leq 200$                                     | $5 \pm 0,25$               |
| $200 < d_i \leq 400$                                     | $10 \pm 0,5$               |
| $400 < d_i \leq 710$                                     | $20 \pm 1$                 |
| $d_i > 710$                                              | $0,03 \times d_i \pm 5 \%$ |
| $d_i$ shall be determined in accordance with 6.3.        |                            |

**5.2 A pair of hard and rigid plates**, through which the testing machine can apply the necessary force,  $F$ , to the test piece.

The plates shall have flat, smooth and clean surfaces for contact with the test piece.

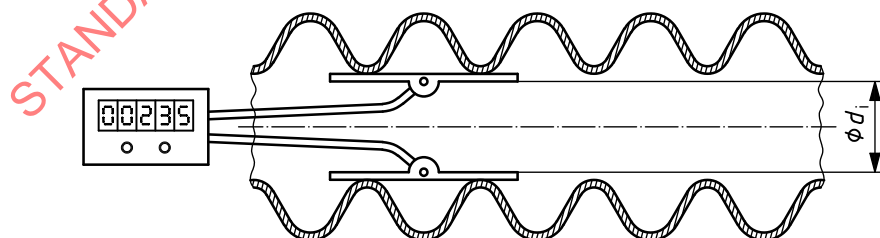
The stiffness and hardness of each plate shall be sufficient to prevent bending or deformation to an extent that would affect the results.

The length of each plate shall be at least equal to the length of the test piece. The width of each plate shall not be less than the width of the contact surface with the test piece while under load plus 25 mm.

**5.3 Dimensional measuring devices**, capable of determining

- individual values for the length of a test piece (see 6.2.2 and 6.2.3) to with an accuracy of  $\pm 1$  mm,
- the inside diameter of a test piece to with an accuracy of  $\pm 0,5 \%$ , and
- the change of inside diameter of a test piece in the direction of loading with an accuracy of 0,1 mm or 1 % of the deflection, whichever is the greater.

An example of a device for measuring the inside diameter of corrugated pipe is shown in Figure 1.



**Figure 1 — Example of device for measuring inside diameter of corrugated pipe**

**5.4 Force measuring device**, capable of determining with an accuracy of  $\pm 2 \%$  the force necessary to produce a deflection of up to 4 % of the test piece.

## 6 Test pieces

### 6.1 Marking and number of test pieces

The pipe of which the ring stiffness is to be determined shall be marked on its outside with a line along one generatrix over its entire length. Three test pieces, a, b and c, respectively, shall be taken from this marked pipe such that the ends of the test pieces are perpendicular to the pipe axis and their lengths conform to 6.2.

### 6.2 Length of test pieces

**6.2.1** The length of each test piece shall be determined by calculating the arithmetic average of three to six measurements of length equally spaced around the perimeter of the pipe, as given in Table 2. The length of each test piece shall conform to 6.2.2, 6.2.3, 6.2.4 or 6.2.5, as applicable.

Each of the three to six length measurements shall be determined to within 1 mm.

For each individual test piece, the smallest of the three to six measurements shall not be less than 0,9 times the largest length measurement.

**Table 2 — Number of length measurements**

| Nominal diameter, $d_n$ , of pipe<br>mm | Number of length measurements |
|-----------------------------------------|-------------------------------|
| $d_n \leq 200$                          | 3                             |
| $200 < d_n < 500$                       | 4                             |
| $d_n \geq 500$                          | 6                             |

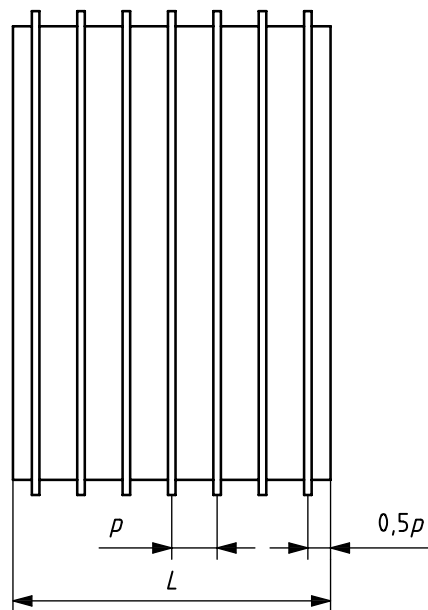
**6.2.2** For pipes that have nominal diameters equal to or less than 1 500 mm, the average length of the test pieces shall be  $(300 \pm 10)$  mm.

**6.2.3** For pipes that have nominal diameters larger than 1 500 mm, the average length of the test pieces in millimetres shall be at least  $0,2 d_n$ .

**6.2.4** Structured wall pipes with perpendicular ribs, corrugations or other regular structures shall be cut such that each test piece contains a whole number of ribs, corrugations or other structures. The cuts shall be made at the mid point between the ribs, corrugations or other structures.

The length of the test pieces shall be the minimum whole number of ribs, corrugations or other structures resulting in a length of 290 mm or greater or, for pipes greater than 1 500 mm,  $0,2 d_n$  or greater.

See Figure 2.

**Key** $L$  length of test piece $p$  pitch**Figure 2 — Test piece cut out of perpendicularly ribbed pipe**

**6.2.5** Structured wall pipes with helical ribs, corrugations or other regular structures shall be cut such that the length of the test pieces is equal to the inside diameter  $\pm 20$  mm but not less than 290 mm nor greater than 1 000 mm.

**6.3 Inside diameter of test piece(s)**

The inside diameters,  $d_{ia}$ ,  $d_{ib}$  and  $d_{ic}$ , of the respective test pieces, a, b and c (see 6.1), shall be determined either as

- the arithmetic average of four or more measurements in accordance with ISO 3126 of one cross section at mid-length, where each measurement shall be determined with an accuracy of  $\pm 0,5$  %, or
- measured at mid-length cross-section by means of a  $\pi$  tape in accordance with ISO 3126.

The calculated or measured average inside diameter for each test piece, a, b and c, shall be recorded, as  $d_{ia}$ ,  $d_{ib}$  and  $d_{ic}$ , respectively.

The average value,  $d_i$ , of these three calculated values shall be calculated using Formula (1):

$$d_i = \frac{d_{ia} + d_{ib} + d_{ic}}{3} \quad (1)$$

**6.4 Age of test pieces**

At the start of testing in accordance with [Clause 8](#), the age of the test pieces shall be at least 24 h.

For type testing, and in case of dispute, the age of the test pieces shall be  $(21 \pm 2)$  days.



## 7 Conditioning

The test pieces shall be conditioned in air at the test temperature (see 8.1) for at least 24 h immediately prior to testing in accordance with Clause 8.

## 8 Procedure

**8.1** Unless otherwise specified in the referring standard, carry out the following procedure at  $(23 \pm 2)^\circ\text{C}$  or, in countries where  $27^\circ\text{C}$  is used as standard laboratory temperature, at  $(27 \pm 2)^\circ\text{C}$ .

In case of dispute,  $(23 \pm 2)^\circ\text{C}$  shall be used.

**NOTE** It is probable that the test temperature has an influence on the ring stiffness.

**8.2** If it can be determined in which position the test piece has the lowest ring stiffness, place the first piece, a, in this position in the loading device.

Otherwise, place the first test piece in such a way that the marking line or split line is in contact with the upper parallel plate.

In the loading device, rotate the two other test pieces, b and c, respectively  $120^\circ$  and  $240^\circ$  in relation to the position of the first test piece when placing them in their loading devices.

**8.3** For each test piece, attach the deflection gauge and check the angular position of the test piece in relation to the upper plate.

Position the test piece with its longitudinal axis parallel to the plates and with its middle point vertically under the centre-line of the load cell.

In order to obtain the correct reading from the load cell, it is necessary to position the test piece so the expected resulting force is approximately in line with the axis of the load cell.

**8.4** Lower the loading plate until it touches the upper part of the test piece.

Apply one of the following pre-load forces,  $F_0$ , as applicable, rounded up to the nearest newton if calculated from Formula (2), taking into account as applicable the mass of the loading plate:

- a) for pipes with  $d_i$  less than or equal to 100 mm,  $F_0$  shall be 7,5 N;
- b) for pipes with  $d_i$  larger than 100 mm,  $F_0$  shall be calculated using Formula (2) in newtons and the result rounded up where necessary to the next higher newton:

$$F_0 = 250 \times 10^{-6} d_i \times L_1 \quad (2)$$

where

$d_i$  is the mean actual inside diameter of the pipe test piece, in millimetres;

$L_1$  is the calculated average length of the test piece, in millimetres.

The actually applied pre-load force shall be between 95 % and 105 % of the calculated force when measured with the accuracy possible with the load cell used for the test.

Then adjust the deflection gauge and load cell to zero.

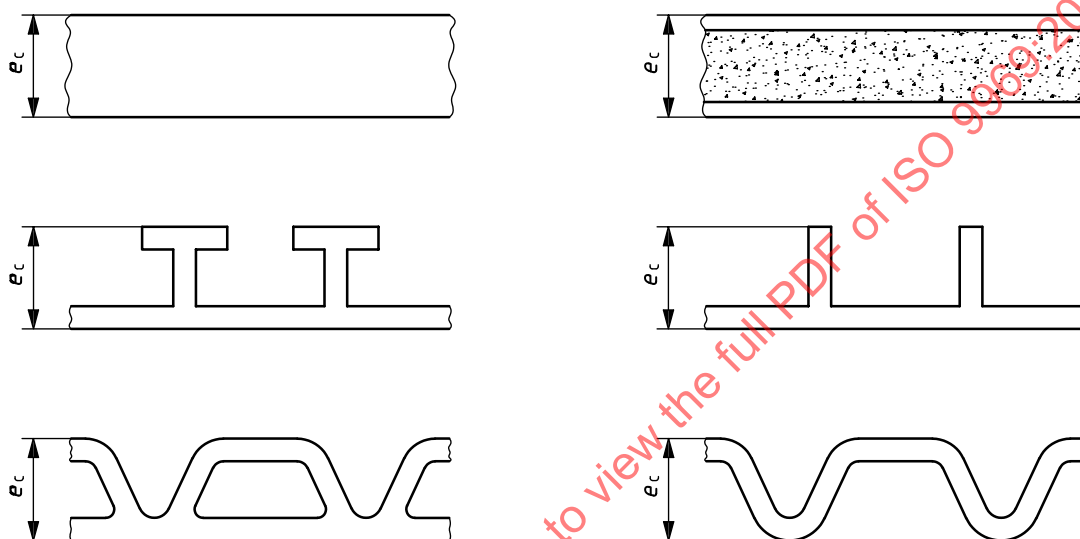
In case of dispute, the zero adjustment method shall be used, see 8.6.

**8.5** Compress the test piece at a constant speed in accordance with [Table 1](#), while continuously recording force and deflection measurements in conformance with [8.6](#), until reaching a deflection of at least  $0,03d_i$ .

**NOTE** When determination of ring flexibility is required, the deflection can be continued until the deflection required for ring flexibility has been reached.

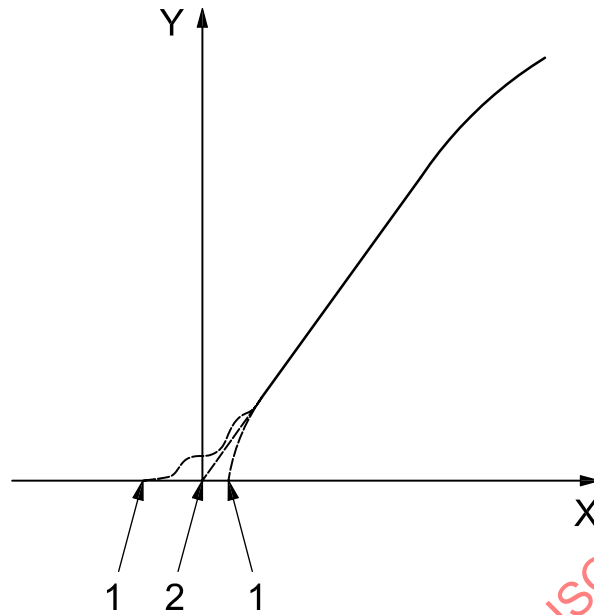
**8.6** Typically, the force and deflection measurements are generated continuously by measuring the displacement of one of the flat plates, but if during the test the pipe wall construction height,  $e_c$  (see [Figure 3](#)), changes by more than 5 %, generate the force/deflection plot by measuring the change of the inside diameter of the test piece.

In case of dispute, the change of the inside diameter shall be used as a reference.



**Figure 3 — Examples of the pipe wall construction height,  $e_c$**

If the force versus deflection plot, which is typically a smooth curve, indicates that the zero point may be in error, as shown in [Figure 4](#), extrapolate back the initial straight line portion of the curve and use the intersect with the horizontal axis as the (0,0) point (origin).

**Key**

- X deflection,  $y$   
Y force,  $F$   
1 apparent zero  
2 corrected zero

**Figure 4 — Method of correcting origin****9 Calculation of ring stiffness**

Calculate the ring stiffness,  $S_a$ ,  $S_b$  and  $S_c$ , of each of the three test pieces (a, b and c, respectively), in kilonewtons per square metre, using the following formulae:

$$S_a = \left( 0,018\,6 + 0,025 \frac{y_a}{d_i} \right) \frac{F_a}{L_a y_a} \times 10^6 \quad (3)$$

$$S_b = \left( 0,018\,6 + 0,025 \frac{y_b}{d_i} \right) \frac{F_b}{L_b y_b} \times 10^6 \quad (4)$$

$$S_c = \left( 0,018\,6 + 0,025 \frac{y_c}{d_i} \right) \frac{F_c}{L_c y_c} \times 10^6 \quad (5)$$

where

$F$  is the force, in kilonewtons, that corresponds to a 3,0 % pipe deflection;

$L$  is the calculated average length of the test piece, in millimetres;

$y$  is the deflection, in millimetres, that corresponds to a 3,0 % deflection, i.e.