

Issued 1991-01
Revised 2003-06
Reaffirmed 2007-06

Superseding AS7475B

**Bolts, Cobalt-Chromium-Nickel Alloy, UNS R30159,
Tensile Strength 260 ksi, Procurement Specification**

FSC 5306

RATIONALE

This document has been reaffirmed to comply with the SAE 5-Year Review policy.

1. SCOPE:

This procurement specification covers bolts made from a corrosion resistant, work-strengthened, cobalt-chromium-nickel alloy of the type identified under the Unified Numbering System as UNS R30159.

1.1 Type:

The following specification designations and their properties are covered:

AS7475	260 ksi minimum ultimate tensile strength at room temperature 205 ksi minimum ultimate tensile strength at 1100 °F 140 ksi stress-rupture strength at 1100 °F 135 ksi tension to 13.5 ksi tension fatigue at room temperature
AS7475-1	260 ksi minimum ultimate tensile strength at room temperature 132 ksi minimum ultimate shear strength at room temperature

1.1.1 Classification:

260 ksi minimum tensile strength at room temperature.

1.2 Application:

Primarily for use in aerospace propulsion system applications where an excellent combination of strength, creep, fatigue, and relaxation resistance is required.

1.3 Safety - Hazardous Materials:

While the materials, methods, applications, and processes described or referenced in this specification may involve the use of hazardous materials, this specification does not address the hazards which may be involved in such use. It is the sole responsibility of the user to ensure familiarity with the safe and proper use of any hazardous materials and to take necessary precautionary measures to ensure the health and safety of all personnel involved.

SAE Technical Standards Board Rules provide that: "This report is published by SAE to advance the state of technical and engineering sciences. The use of this report is entirely voluntary, and its applicability and suitability for any particular use, including any patent infringement arising therefrom, is the sole responsibility of the user."

SAE reviews each technical report at least every five years at which time it may be reaffirmed, revised, or cancelled. SAE invites your written comments and suggestions.

Copyright © 2007 SAE International

All rights reserved. No part of this publication may be reproduced, stored in a retrieval system or transmitted, in any form or by any means, electronic, mechanical, photocopying, recording, or otherwise, without the prior written permission of SAE.

TO PLACE A DOCUMENT ORDER: Tel: 877-606-7323 (inside USA and Canada)
Tel: 724-776-4970 (outside USA)
Fax: 724-776-0790
Email: CustomerService@sae.org
SAE WEB ADDRESS: <http://www.sae.org>

2. REFERENCES:

2.1 Applicable Documents:

The following publications form a part of this document to the extent specified herein. The latest issue of SAE publications shall apply. The applicable issue of other publications shall be the issue in effect on the date of the purchase order. In the event of conflict between the text of this document and references cited herein, the text of this document takes precedence. Nothing in this document, however, supersedes applicable laws and regulations unless a specific exemption has been obtained.

2.1.1 SAE Publications: Available from SAE, 400 Commonwealth Drive, Warrendale, PA 15096-0001.

AMS 2750 Pyrometry
AMS 5842 Cobalt-Nickel Alloy, Corrosion Heat Resistant, Bars, 19Cr 36Co 25Ni 7.0Mo 0.50Cb
2.9Ti 0.20Al 9.0Fe, Vacuum Induction Plus Vacuum Consumable

AS3062 Bolts, Screws and Studs, Screw Thread Requirements
AS3063 Bolts, Screws and Studs, Geometric Control Requirements
AS8879 Screw Threads - UNJ Profile, Inch

2.1.2 U.S. Government Publications:

MS21296 Bolt, Tension, Steel, 260 ksi Ft_u, 450 °F, External Wrenching, Spline Drive,
Flanged Head

2.1.3 ASTM Publications: Available from ASTM, 100 Barr Harbor Drive, West Conshohocken, PA 19428-2959.

ASTM E 8 Tension Testing of Metallic Materials
ASTM E 21 Elevated Temperature Tension Tests of Metallic Materials
ASTM E 112 Determining Average Grain Size
ASTM E 139 Conducting Creep, Creep-Rupture, and Stress-Rupture Tests in Metallic Materials
ASTM E 140 Standard Hardness Conversion Tables for Metals
ASTM E 1417 Liquid Penetrant Examination
ASTM D 3951 Commercial Packaging

SAE AS7475 Revision C

2.1.4 AIA/NAS Publications: Available from Aerospace Industries Association of America, Inc. (AIA), 1250 Eye Street NW, Suite 1100, Washington, DC 20005-3924.

NASM 1312-6	Fastener Test Methods, Method 6, Hardness
NASM 1312-8	Fastener Test Methods, Method 8, Tensile Strength
NASM 1312-10	Fastener Test Methods, Method 10, Stress-Rupture
NASM 1312-11	Fastener Test Methods, Method 11, Tension Fatigue
NASM 1312-13	Fastener Test Methods, Method 13, Double Shear Test
NASM 1312-18	Fastener Test Methods, Method 18, Elevated Temperature Tensile Strength

2.1.5 ASME Publications: Available from ASME, 22 Law Drive, Box 2900, Fairfield, NJ 07007-2900.

ASME B46.1 Surface Texture (Surface Roughness, Waviness, and Lay)

2.2 Definitions:

BURR: A rough edge or ridge left on the metal due to a cutting, grinding, piercing or blanking operation.

COLD WORKING: Forming material below the recrystallation temperature.

CRACK: Rupture in the material which may extend in any direction and which may be intercrystalline or transcrystalline in character.

DISCONTINUITY: An interruption in the normal physical structure or configuration of a part; such as a lap, seam, inclusion, crack, machining tear, or stringer.

HEAT PATTERN: The discernible difference in the etched appearance between the head and shank caused by the plastic forming of the head.

INCLUSION: Nonmetallic particles originating from the material making process. They may exist as discrete particles or strings of particles extending longitudinally.

INSPECTION LOT: Shall consist of parts from a single production lot, of the same part number.

LAP: Surface imperfection caused by folding over metal fins or sharp corners and then rolling or forging them into the surface. The allowable lap depth shall not exceed the limit specified herein. The minimum condition that shall be rated as a lap is a fold having its length equal to or greater than three times its width with a depth of 0.0005 inch when viewed at 200X magnification.

MACHINING TEAR: A pattern of short, jagged individual cracks, generally at right angles to the direction of machining, frequently the result of improperly set cutting tools, or dull cutting tools.

NON-CONFORMANCE: A departure from a specified requirement for any characteristic.

NON-CONFORMING UNIT: A unit of the product that has one or more non-conformances.

SAE AS7475 Revision C

2.2 (Continued):

PRODUCTION INSPECTION LOT: Shall be all finished parts of the same part number, made from a single heat of alloy, heat treated at the same time to the same specified condition, produced as one continuous run, and submitted for the vendor's inspection at the same time.

ROOM TEMPERATURE: Ambient temperature (68 °F approximately).

SEAM: Longitudinal surface imperfection in the form of an unwelded, open fold in the material.

STRINGER: A solid nonmetallic impurity in the metal or bar, often the result of inclusions that have been extended during the rolling process.

TIGHT BURR: A burr closely compacted and binding in the periphery of a part without any loose ends and is within the dimensional limits of the part.

2.3 Unit Symbols:

- ° - degree, angle
- °F - degree Fahrenheit
- % - percent (1% = 1/100)
- lbf - pounds force
- ksi - kips (1000 pounds) per square inch
- sp gr - specific gravity
- HRC - hardness, Rockwell C scale

3. TECHNICAL REQUIREMENTS:

3.1 Material:

Shall be AMS 5843 alloy heading stock.

3.2 Design:

Finished (completely manufactured) parts shall conform to the following requirements:

- 3.2.1 Dimensions: The dimensions of finished parts, after all processing, including plating, shall conform to the part drawing. Dimensions apply after plating but before coating with solid film lubricants.
- 3.2.2 Surface Texture: Surface texture of finished parts, prior to plating or coating, shall conform to the requirements as specified on the part drawing, determined in accordance with ASME B46.1.
- 3.2.3 Threads: Screw thread UNJ profile and dimensions shall be in accordance with AS8879, unless otherwise specified on the part drawing.

SAE AS7475 Revision C

- 3.2.3.1 Incomplete Lead and Runout Threads: Incomplete threads are permissible at the entering end and at the juncture of the unthreaded portion of the shank or adjacent to the head as specified in AS3062.
- 3.2.3.2 Chamfer: The entering end of the thread shall be chamfered as specified on the part drawing.
- 3.2.4 Geometric Tolerances: Part features shall be within the geometric tolerances specified on the part drawing and, where applicable, in accordance with AS3063.
- 3.3 Fabrication:
- 3.3.1 Blanks: Heads shall be formed by hot or cold forging; machined heads are not permitted, except lightening holes may be produced by any suitable method. Wrenching recesses may be forged or machined. Flash or chip clearance in machined recesses shall not cause recess dimensions to exceed the specified limits.
- 3.3.2 Heat Treatment: Before finishing the shank and bearing surface of the head, cold working the head-to-shank fillet radius, and rolling the threads, headed blanks shall be aged as follows:
- 3.3.2.1 Heating Equipment: Furnaces may be any type ensuring uniform temperature throughout the parts being heated and shall be equipped with, and operated by, automatic temperature controllers and data recorders conforming to AMS 2750. The heating medium or atmosphere shall cause no surface hardening by carburizing or nitriding.
- 3.3.2.2 Aging Heat Treatment: Headed blanks shall be aged by heating to a temperature within the range 1200 to 1250 °F, holding at the selected temperature within ± 25 °F for 4 to 4.5 hours, and cooling at a rate equivalent to air cooling.
- 3.3.3 Oxide Removal: Surface oxide and oxide penetration resulting from prior heat treatment shall be removed from the full body diameter and bearing surface of the head of the solution heat treated, work-strengthened, and aged blanks prior to cold working the fillet radius and rolling the threads. The oxide removal process shall produce no intergranular attack or corrosion of the blanks. The metal removed from the bearing surface of the head and the full body diameter of the shank shall be as little as practicable to obtain a clean, smooth surface.

SAE AS7475 Revision C

- 3.3.4 Cold Working of Fillet Radius: After removal of oxide as in 3.3.3, the head-to-shank fillet radius of headed parts having the radius complete throughout the circumference of the part shall be cold worked sufficiently to remove all visual evidence of grinding or tool marks. Distortion due to cold working shall conform to Figure 2, unless otherwise specified on the part drawing. It shall not raise metal more than 0.002 inch above the contour at "A" or depress metal more than 0.002 inch below the contour at "B" as shown in Figure 2; distorted areas shall not extend beyond "C" shown in Figure 2. In configurations having an undercut connected with the fillet radius, the cold working will be required only for 90° of fillet arc, starting at the point of tangency of the fillet radius and the bearing surface of the head. For shouldered bolts, having an unthreaded shank diameter larger than the thread major diameter and having an undercut connected with a fillet between the threaded shank and the shoulder of the unthreaded shank, the cold working will be required only for 90° of the fillet arc, starting at the point of tangency of the fillet radius and the shouldered surface of the unthreaded shank. The shank diameter on close tolerance full shank bolts shall not exceed its maximum diameter limit after cold working the head-to-shank fillet radius.
- 3.3.5 Thread Rolling: Thread shall be formed on the finished blanks by a single cold rolling process after removal of oxide as in 3.3.3.
- 3.3.6 Cleaning: Parts, after finishing, shall be degreased and immersed in one of the following solutions for the time and temperature shown:
- One volume of nitric acid (sp gr 1.42) and 9 volumes of water for not less than 20 minutes at room temperature.
 - One volume of nitric acid (sp gr 1.42) and 4 volumes of water for 30 to 40 minutes at room temperature.
 - One volume of nitric acid (sp gr 1.42) and 4 volumes of water for 10 to 15 minutes at 140 to 160 °F.
- 3.3.6.1 Water Rinse: Immediately after removal from the cleaning solution, parts shall be thoroughly rinsed in clean water at 70 to 200 °F.
- 3.4 Product Marking:
- Each part shall be identification marked as specified on the part drawing. The markings may be formed by forging or stamping, raised or depressed 0.010 inch maximum, with rounded root form on depressed characters.
- 3.5 Plating or Coating:
- Where required, surfaces shall be plated or coated as specified by the part drawing. Where coating with solid film lubricants is required, the under head bearing surface, the unthreaded shank, and the threads shall be coated as specified on the part drawing; other surfaces are optional to coat, unless otherwise specified. Plating thickness shall be determined in accordance with the requirements in the applicable plating specification.

SAE AS7475 Revision C

3.6 Mechanical Properties:

Where AS7475 is specified, parts shall conform to the requirements of 3.6.1, 3.6.2, 3.6.3, 3.6.4, and 3.6.5. Where AS7475-1 is specified, parts shall conform to the requirements of 3.6.1, 3.6.3, and 3.6.6. Threaded members of gripping fixtures for tensile tests, and fatigue tests shall be of sufficient size and strength to develop the full strength of the part without stripping the thread. The loaded portion of the shank shall have a minimum of three full threads from the thread runout exposed between the loading fixtures during tensile test.

AS7475 finished parts shall be tested in accordance with the following test methods:

- a. Hardness:NASM 1312-6
- b. Ultimate Tensile Strength at Room Temperature:NASM 1312-8
- c. Ultimate Tensile Strength at 1100 °F:NASM 1312-18
- d. Stress-Rupture Strength at 1100 °F:NASM 1312-10
- e. Fatigue Strength at Room Temperature:NASM 1312-11

AS7475-1 finished parts shall be tested in accordance with the following test methods:

- a. Hardness:NASM 1312-6
- b. Ultimate Tensile Strength at Room Temperature:NASM 1312-8
- c. Ultimate Double Shear at Room Temperature:NASM 1312-13

3.6.1 Ultimate Tensile Strength at Room Temperature:

3.6.1.1 Finished Parts: Tension bolts, such as double hexagon and spline drive heads, shall have an ultimate tensile load not lower than that specified in Table 2 and shall be tested to failure in order to observe fracture location, first measuring and recording the maximum tensile load achieved. If size and shape of the part is such that failure would occur outside the threaded section but part can be tested satisfactorily, such as parts having a shank diameter equal to or less than the thread root diameter or having an undercut, parts shall have an ultimate tensile strength not lower than 260 ksi; for such parts, the diameter of the area on which stress is based shall be the actual measured minimum diameter of the part. Tension fasteners with either standard double hexagon or spline drive heads having a minimum metal condition in the head equal to the design parameters specified in MS21296, shall not fracture in the head-to-shank fillet radius except when this radius is connected with an undercut or with a shank diameter less than the minimum pitch diameter of the thread.

3.6.1.2 Machined Test Specimens: If the size and the shape of the part is such that a tensile test cannot be made on the part, tensile tests shall be conducted in accordance with ASTM E 8 on specimens prepared as in 4.5.7. Specimens may be required by the purchaser to perform confirmatory tests. Such specimens shall meet the following room temperature requirements:

- a. Ultimate Tensile Strength, minimum: 260 ksi
- b. Yield Strength at 0.2% Offset, minimum: 230 ksi
- c. Elongation in 4D, minimum: 6%
- d. Reduction of Area, minimum: 22%

SAE AS7475 Revision C

3.6.1.2.1 When permitted by the purchaser, hardness tests on the end of parts may be substituted for tensile tests of machined specimens.

3.6.2 Ultimate Tensile Strength at 1100 °F:

3.6.2.1 Finished Parts: Tension bolts, such as double hexagon and spline drive heads, heated to 1100 °F, held at heat for 20 minutes before testing, shall have an ultimate tensile load not lower than that specified in Table 2 and shall be tested to failure in order to observe fracture location, first measuring and recording the maximum tensile load achieved. If size and shape of the part is such that failure would occur outside the threaded section but part can be tested satisfactorily, such as parts having a shank diameter equal to or less than the thread root diameter or having an undercut, parts shall have an ultimate tensile strength not lower than 205 ksi; for such parts, the diameter of the area on which stress is based shall be the actual measured minimum diameter of the part. Tension fasteners with either standard double hexagon or spline drive heads having a minimum metal condition in the head equal to the design parameters in MS21296, shall not fracture in the head-to-shank fillet radius except when this radius is connected with an undercut or with a shank diameter less than the minimum pitch diameter of the thread.

3.6.2.2 Machined Test Specimens: If the size and the shape of the part is such that a tensile test cannot be made on the part, tensile tests shall be conducted in accordance with ASTM E 21 on specimens prepared as in 4.5.8. Specimens may be required by the purchaser to perform confirmatory tests. Such specimens shall meet the following requirements when heated to 1100 °F ± 10 °F, held at heat for 20 minutes before testing, and tested at 1100 °F ± 10 °F.

- | | |
|--|---------|
| a. Ultimate Tensile Strength, minimum: | 205 ksi |
| b. Yield Strength at 0.2% Offset, minimum: | 190 ksi |
| c. Elongation in 4D, minimum: | 5% |
| d. Reduction in Area, minimum: | 15% |

3.6.3 Hardness: Shall be uniform and not lower than 44 HRC (see 8.1), but hardness of the threaded section and of the head-to-shank fillet area may be higher than other areas as a result of the cold working operations. Parts shall not be rejected on the basis of hardness if the tensile strength properties specified in 3.6.1 are met.

3.6.4 Stress-Rupture Strength at 1100 °F:

3.6.4.1 Finished Parts: Finished tension bolts, maintained at 1100 °F ± 3 °F while the tensile load specified in Table 2 is applied continuously, shall not rupture in less than 23 hours. If the shank diameter of the bolt is less than the maximum minor (root) diameter of the thread but the bolt can be tested satisfactorily, bolts shall conform to the requirements of 3.6.4.1.1.

3.6.4.1.1 Bolts having a shank diameter less than the maximum minor (root) diameter of the thread shall be tested as in 3.6.4.1, except that the load shall be as specified in 3.6.4.2. The diameter of the area on which the stress is based shall be the actual measured minimum diameter of the bolt.

SAE AS7475 Revision C

- 3.6.4.2 Machined Test Specimens: If the size and shape of the bolt is such that a stress-rupture test cannot be made on the bolt, a test specimen prepared as in 4.5.8, maintained at $1100\text{ }^{\circ}\text{F} \pm 3\text{ }^{\circ}\text{F}$ while a load sufficient to produce an initial stress of 140 ksi is applied continuously, shall not rupture in less than 23 hours. Tests shall be conducted in accordance with ASTM E 139. Specimens may be required by purchaser to perform confirmatory tests.
- 3.6.5 Fatigue Strength: Finished tension bolts tested in tension-tension fatigue at room temperature with maximum load as specified in Table 2 and minimum load equal to 10% of the maximum load shall have an average life of not less than 65,000 cycles with no part having life less than 45,000 cycles. Tests need not be run beyond 130,000 cycles. Life of parts which do not fail in less than 130,000 cycles shall be taken as 130,000 cycles for purposes of computing average life. If the shank diameter of the bolt is less than the minimum pitch diameter of thread, bolts shall withstand fatigue testing as above using loads sufficient to produce a maximum stress of 135 ksi and a minimum stress of 13.5 ksi. The above requirements apply to tension bolts, such as double hexagon and spline drive heads per design parameters specified in MS21296 0.190 inch and larger in nominal thread size, having a head-to-shank fillet radius equal to or larger than that specified in MS21296, and not having an undercut; for all parts to which the above requirements do not apply, fatigue test requirements shall be as specified on the part drawing.
- 3.6.6 Ultimate Shear Strength: Finished parts having a close toleranced full shank as in MS21296 shall have an ultimate double shear load no lower than that specified in Table 2. The double shear test may be discontinued without a complete shear failure after the ultimate double shear load has been reached, first measuring and recording the maximum double shear load achieved. Shear bolts having special shank diameters shall have the minimum ultimate double shear load based on 132 ksi minimum shear strength. Shear tests are not required for the following conditions:
- a. Bolts threaded to head.
 - b. Protruding head bolts having coarse toleranced full shank.
 - c. Protruding head bolts having PD or relieved shank.
- 3.7 Quality:
- Parts shall be uniform in quality and condition, free from burrs (tight burrs may be acceptable if part performance is not affected), foreign materials, and from imperfections detrimental to the usage of the parts.
- 3.7.1 Macroscopic Examination, Headed Blanks: A specimen cut from a headed blank shall be etched in a suitable etchant and examined at a magnification of 20X to determine conformance to the requirements of 3.7.1.1 and 3.7.1.2. The head and shank section shall extend not less than $D/2$ from the bearing surface of the head, where "D" equals the nominal diameter after heading.

SAE AS7475 Revision C

- 3.7.1.1 Flow Lines: After heading and prior to heat treatment, examination of an etched section taken longitudinally through the blank shall show flow lines or heat pattern in the shank, head-to-shank fillet, and the bearing surface which follows the contour of the blank as shown in Figure 1 or Figure 1A. Flow lines or heat pattern in the headed blanks having special heads, such as Dee- or Tee-shaped heads or thinner than MS21296 standard heads, shall be as agreed upon by purchaser and vendor.
- 3.7.1.2 Internal Imperfections: Examination of longitudinal sections of the head and shank shall reveal no cracks, laps, or porosity.
- 3.7.2 Microscopic Examination, Finished Parts: Specimens cut from finished parts shall be polished, etched in Kalling's reagent, Marble's reagent, or other suitable etchant, and examined at 100X magnification to determine conformance to the requirements of 3.7.2.1, 3.7.2.2, 3.7.2.3, 3.7.2.4, 3.7.2.5, and 3.7.2.6.
- 3.7.2.1 Flow Lines: Examination of a longitudinal section through the threaded portion of the shank shall show evidence that the threads were rolled, see Figure 3.
- 3.7.2.2 Internal Imperfections: Examination of longitudinal sections of the head and shank shall reveal no cracks, laps, or porosity. Thread imperfections shall conform to the requirements of 3.7.2.6.
- 3.7.2.3 Microstructure: Parts shall have distorted grain structure indicative of cold worked material free from recrystallization in the areas other than the head.
- 3.7.2.4 Grain Size: The grain size in areas other than the head, shall be ASTM No. 4 or finer, with up to 15% of the area as large as ASTM No. 2, as determined by comparison of a polished and etched specimen with the charts in ASTM E 112. In case of disagreement on the average grain size by the comparison method, the intercept (Heyn) procedure shall be used.
- 3.7.2.5 Surface Hardening: Parts shall have no change in hardness from core to surface except as produced during cold working of the head-to-shank fillet radius and during rolling of the threads. In the case of dispute over the results of the microscopic examination, microhardness testing shall be used as the referee method; a Vickers hardness reading of an unrolled surface which exceeds the reading in the core by more than 30 points shall be evidence of nonconformance to this requirement.
- 3.7.2.6 Threads:
- 3.7.2.6.1 Root imperfections such as laps, seams, notches, slivers, folds, roughness, and oxide scale are not permissible (see Figure 4).
- 3.7.2.6.2 Multiple laps on the flanks of threads are not permissible regardless of location.

3.7.2.6.3 Single Lap on Thread Profile: Shall conform to the following:

- a. Thread Flank Above the Pitch Diameter: A single lap is permissible along the flank of the thread above the pitch diameter on either the pressure or the nonpressure flank (one lap at any cross-section through the thread) provided it extends toward the crest and is generally parallel to the flank (see Figure 5). The lap depth shall not exceed the limit specified in Table 1 for the applicable thread pitch. A lap extending towards the root is not permissible (see Figure 6).
- b. Thread Flank Below the Pitch Diameter: A lap along the thread flank below the pitch diameter, regardless of direction it extends, is not permissible (see Figure 7).
- c. Crest craters, crest laps, or a crest lap in combination with a crest crater are permissible, provided that the imperfections do not extend deeper than the limit specified in Table 1 as measured from the thread crest when the thread major diameter is at minimum size (see Figure 8). The major diameter of the thread shall be measured prior to sectioning. As the major diameter approaches maximum size, values for depth of crest crater and crest lap imperfections listed in Table 1 may be increased by one-half of the difference between the minimum major diameter and the actual major diameter as measured on the part.

3.7.3 Fluorescent Penetrant Inspection: Prior to any required coating, parts shall be subject to fluorescent penetrant inspection in accordance with ASTM E 1417, Type 1, Sensitivity Level 2 minimum.

3.7.3.1 The following conditions shall be cause for rejection of parts inspected:

- 3.7.3.1.1 Discontinuities transverse to grain flow (i.e., at an angle of more than 10° to the axis of the shank), such as grinding checks and cracks.
- 3.7.3.1.2 Longitudinal indications (i.e., at an angle 10° or less to the axis of the shank) due to imperfections, other than seams, forming laps, and nonmetallic inclusions.

3.7.3.2 The following conditions shall be considered acceptable on parts inspected:

- 3.7.3.2.1 Parts having longitudinal indications (i.e., at an angle of 10° or less to the axis of the shank) of seams and forming laps parallel to the grain flow that are within the limits specified in 3.7.3.2.2 through 3.7.3.2.5 provided the separation between indications in all directions is not less than 0.062 inch.
- 3.7.3.2.2 Sides of Head: There shall be not more than three indications per head. The length of each indication may be the full height of the surface but no indication shall break over either edge to a depth greater than 0.031 inch or the equivalent of 2H/3 thread depth (see Table 1), whichever is less.

SAE AS7475 Revision C

- 3.7.3.2.3 Shank or Stem: There shall be not more than five indications. The length of any indication may be the full length of the surface but the total length of all indications shall not exceed twice the length of the surface. No indication shall break into a fillet or over an edge.
- 3.7.3.2.4 Threads: There shall be no indications, except as permitted in 3.7.2.6. Rateable lap indications shall conform to 3.7.2.6.3.a.
- 3.7.3.2.5 Top of Head and End of Stem: The number of indications is not restricted but the depth of any individual indication shall not exceed 0.010 inch as shown by sectioning representative samples. No indication, except those of 3.7.3.2.2, shall break over an edge.

4. QUALITY ASSURANCE PROVISIONS:

4.1 Responsibility for Inspection:

The vendor of parts shall supply all samples and shall be responsible for performing all required tests. Purchaser reserves the right to perform such confirmatory testing as deemed necessary to ensure that the parts conform to the requirements of this specification.

4.2 Responsibility for Compliance:

The manufacturer's system for parts production shall be based on preventing product defects, rather than detecting the defects at the final inspection and then requiring corrective action to be invoked. An effective manufacturing in-process control system shall be established, subject to the approval of the purchaser, and used during production of parts.

4.3 Production Acceptance Tests:

The purpose of production acceptance tests is to check, as simply as possible, using a method which is inexpensive and representative of the part usage, with the uncertainty inherent in the random sampling, that the parts comprising a production inspection lot satisfy the requirements of this specification.

4.4 Classification of Tests:

- a. Tests for all technical requirements are acceptance tests and shall be performed on each production inspection lot. A summary of acceptance tests is specified in Table 3.
- b. Periodic tests which are to be performed periodically on production lots at the discretion of the vendor or purchaser. Ultimate tensile strength test at 1100 °F as in 3.6.2 is classified as a periodic test and shall be performed when requested by the purchaser.

4.5 Acceptance Test Sampling:

- 4.5.1 Material: Sampling for material composition on each heat shall be in accordance with AMS 5842.

SAE AS7475 Revision C

- 4.5.2 Nondestructive Test - Visual and Dimensional: A random sample shall be taken from each production inspection lot; the size of the sample to be as specified in Table 4. The classification of dimensional characteristics shall be as specified in Table 5. All dimensional characteristics are considered non-conforming when out of tolerance.
- 4.5.3 Fluorescent Penetrant Inspection: A random sample shall be selected from each production inspection lot; the size of the sample shall be as specified in Table 4 and as classified in Table 5. The sample units may be selected from those that have been subjected to and passed the visual and dimensional inspection, with additional units selected at random from the production inspection lot as necessary.
- 4.5.4 Stress-Rupture Tests: A random sample of a minimum of one part (or one test specimen where required) shall be selected from each production inspection lot.
- 4.5.5 Macroscopic Examination: A random sample of one part shall be selected from each production lot.
- 4.5.6 Destructive Tests: A random sample shall be selected from each production inspection lot; the size of the sample shall be as specified in Table 6. The sample units may be selected from those that have been subjected to and passed the nondestructive tests and the fluorescent penetrant inspection, with additional units selected at random from the production inspection lot as necessary.
- 4.5.7 Acceptance Quality: Of random samples tested, acceptance quality shall be based on zero non-conformances.
- 4.5.8 Test Specimens: Specimens for tensile testing of machined specimens shall be of standard proportions in accordance with ASTM E 8. Specimens shall be machined from finished parts or coupons of the same lot of alloy and be processed together with the parts they represent. Specimens shall be machined from the center of parts less than 0.800 inch in nominal diameter, or from mid-radius of larger parts or coupons.
- 4.6 Periodic Test Sampling:
- As agreed upon by purchaser and vendor.
- 4.7 Reports:
- The vendor of parts shall furnish with each shipment a report stating that the chemical composition of the parts conforms to the applicable material specification, showing the results of tests to determine conformance to the room temperature ultimate tensile property, hardness, and double shear test (if required), and stating that the parts conform to the other technical requirements. This report shall include the purchase order number, AS7475 and Revision Letter, lot number, contractor or other direct supplier of material, part number, nominal size, and quantity.

4.8 Rejected Lots:

Failure of a destructive test requirement as specified in Table 3 shall constitute scrapping of the entire lot. Failure of a non-destructive test requirement as specified in Table 3 will require vendor of parts to perform corrective action to screen out or rework the non-conforming parts and resubmit for acceptance tests inspection as in Table 3. Resubmitted lots shall be clearly identified as reinspected lots.

5. PREPARATION FOR DELIVERY:

5.1 Packaging and Identification:

5.1.1 Packaging shall be in accordance with ASTM D 3951.

5.1.2 Parts having different part numbers shall be packed in separate containers.

5.1.3 Each container of parts shall be marked to show not less than the following information:

BOLTS, UNS R30159, 260 ksi
AS7475B (or AS7475-1B as applicable)
PART NUMBER
LOT NUMBER
PURCHASE ORDER NUMBER
QUANTITY
MANUFACTURER'S IDENTIFICATION

5.1.4 Threaded fasteners shall be protected from abrasion and chafing during handling, transportation, and storage.

6. ACKNOWLEDGMENT:

A vendor shall mention this specification number in all quotations and when acknowledging purchase orders.

7. REJECTIONS:

Parts not conforming to this specification, or to modifications authorized by purchaser, will be subject to rejection.

8. NOTES:

8.1 Hardness Conversion Tables:

Hardness conversion tables for metals are presented in ASTM E 140.

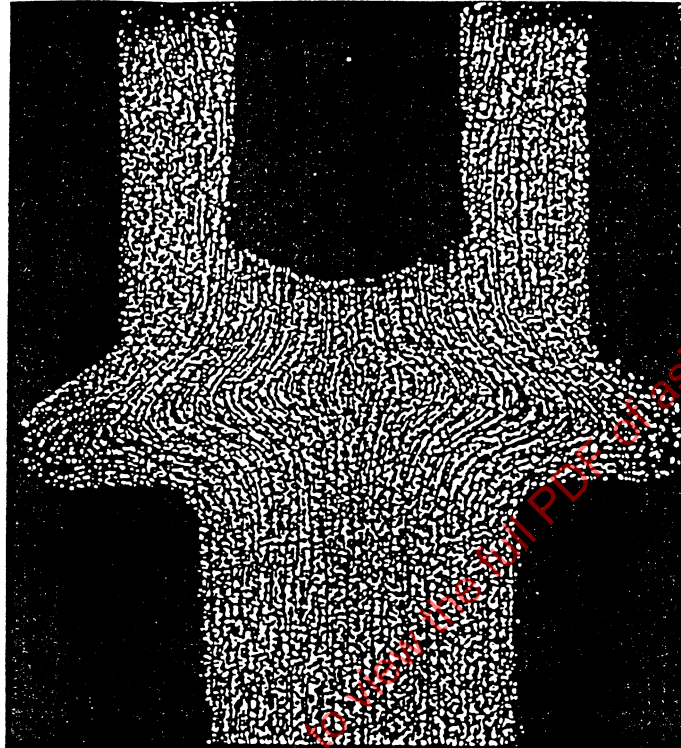
8.2 Key Words:

Bolts, Procurement Specification

- 8.3** The change bar (|) located in the left margin is for the convenience of the user in locating areas where technical revisions, not editorial changes, have been made to the previous issue of this document. An (R) symbol to the left of the document title indicates a complete revision of the document.

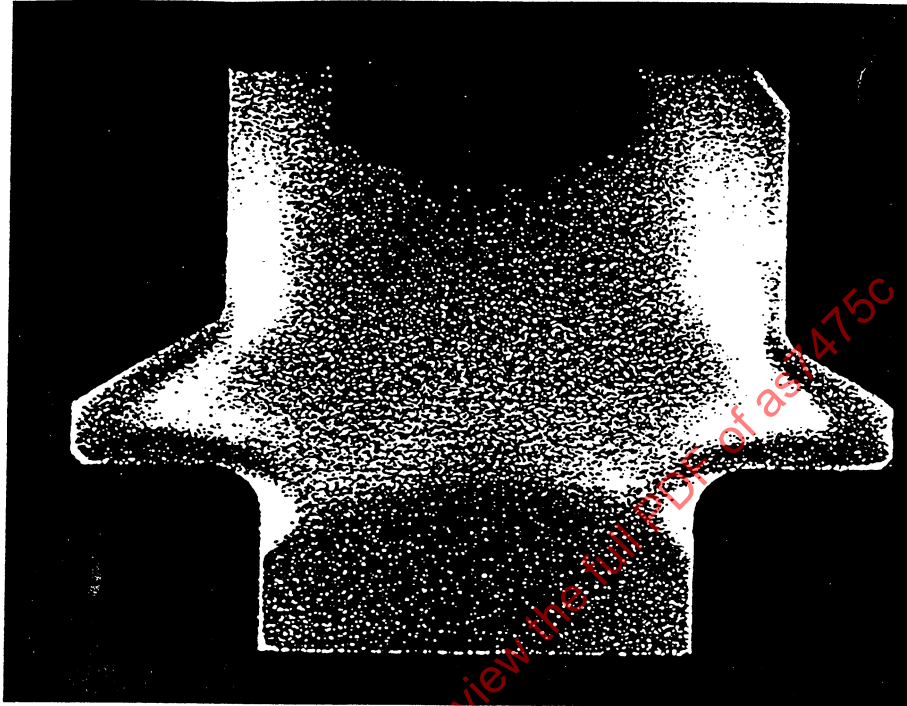
SAENORM.COM : Click to view the full PDF of as7475c

PREPARED UNDER THE JURISDICTION OF
SAE COMMITTEE E-25, GENERAL STANDARDS FOR AEROSPACE PROPULSION SYSTEMS



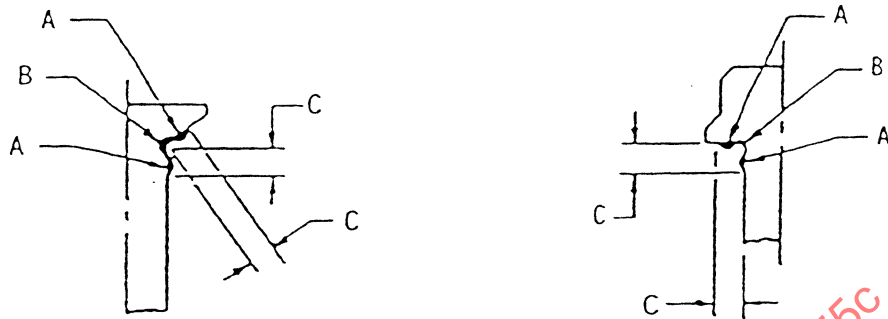
Showing a smooth, well formed grain flow following the contour of the head-to-shank fillet radius.

FIGURE 1 - Satisfactory Grain Flow, Cold Headed Blank, Before Heat Treatment



Shows evidence that head was formed by forging.

FIGURE 1A - Satisfactory Heat Pattern, Hot Headed Blank, Before Heat Treatment



Nominal Bolt Diameter, inch	C max. inch
< 0.3125	0.062
0.3125 to < 0.4375	0.094
0.4375 to < 0.7500	0.125
0.7500 to 1.000	0.156
> 1.000	0.188

FIGURE 2 - Permissible Distortion from Fillet Working



FIGURE 3 - Flow Lines, Rolled Thread

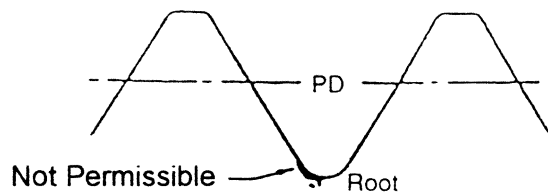


FIGURE 4 - Root Defects, Rolled Thread

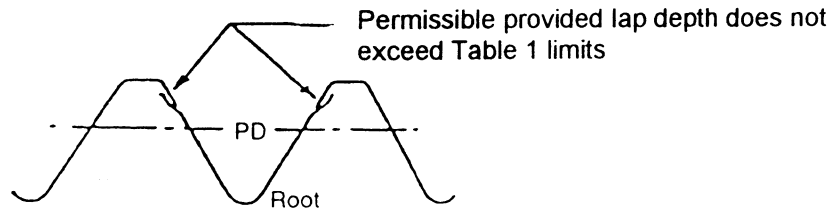


FIGURE 5 - Laps Above Pitch Diameter Extending Towards Crest, Rolled Thread

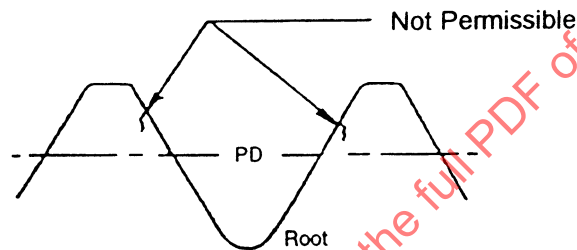


FIGURE 6 - Laps Above Pitch Diameter Extending Towards Root, Rolled Thread

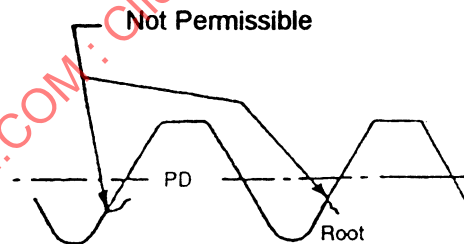
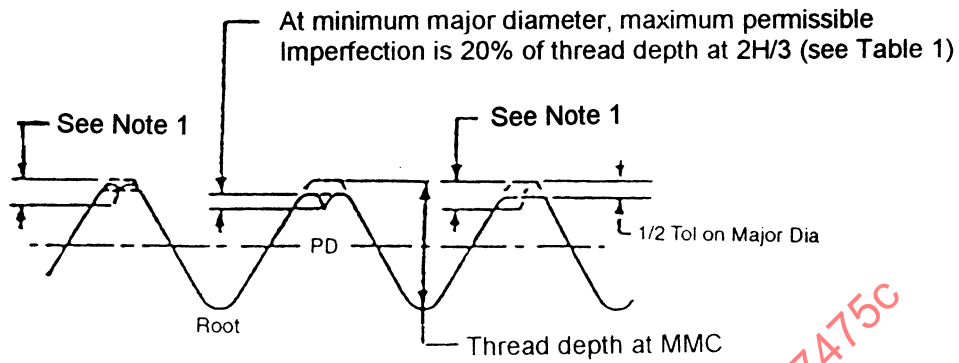


FIGURE 7 - Laps Below Pitch Diameter Extending in Any Direction, Rolled Thread



Note 1: - Maximum depth of imperfection equals 20% of thread depth at $2H/3$ plus half the difference of the actual major diameter and minimum major diameter.

FIGURE 8 - Crest Craters and Crest Laps, Rolled Thread

SAE AS7475 Revision C

TABLE 1 - UNJ External Thread Depth at 2H/3 and Allowable Thread Lap Depth

Thread Pitches Per Inch n	External Thread Depth at 2H/3 Ref inch	Allowable Thread Lap Depth /1/ inch
80	0.0072	0.0014
72	0.0080	0.0016
64	0.0090	0.0018
56	0.0100	0.0021
48	0.0120	0.0024
44	0.0131	0.0026
40	0.0144	0.0029
36	0.0160	0.0032
32	0.0180	0.0036
28	0.0206	0.0041
24	0.0241	0.0048
20	0.0289	0.0058
18	0.0321	0.0064
16	0.0361	0.0072
14	0.0412	0.0082
13	0.0444	0.0089
12	0.0481	0.0096
11	0.0525	0.0105
10	0.0577	0.0115
9	0.0642	0.0128
8	0.0722	0.0144

Note 1: Allowable lap depth is based on 20% of UNJ external thread depth at 2H/3 in accordance with AS8879, and is calculated as follows:

$$\text{External thread depth} = 2H/3 = (2/3) (\cos 30^\circ)/n = 0.57735/n$$

$$\text{Lap depth} = 0.2(2H/3) = 0.2(2/3) (\cos 30^\circ)/n = 0.11547/n$$