

Submitted for recognition as an American National Standard

BOLTS & SCREWS, UNS N07001
760°C, 1210 MPa
1065°C Solution Heat Treatment
Procurement Specification For, Metric

1. SCOPE:

- 1.1 Type: This procurement specification covers aircraft quality metric bolts and screws made from a corrosion and heat resistant nickel-base alloy of the type identified under the Unified Numbering System as UNS N07001.
- 1.2 Application: Primarily for joining parts where high strength at temperatures up to 760°C and oxidation resistance up to 955°C are required.

2. APPLICABLE DOCUMENTS: The following publications form a part of this standard to the extent specified herein. The latest issue of Aerospace Material Specification (AMS) and Aerospace Standard (AS & MA) shall apply. The applicable issue of other documents shall be specified in AMS 2350.

- 2.1 SAE Publications: Available from SAE, 400 Commonwealth Drive, Warrendale, PA 15096.

2.1.1 Aerospace Material Specifications:

AMS 2350 - Standards and Test Methods
AMS 2645 - Fluorescent Penetrant Inspection
AMS 5708 - Alloy Bars, Forgings, Corrosion and Heat Resistant,
58Ni-19.5Cr-13.5Co-4.3Mo-3.0Ti-1.4Al, Consumable
Electrode or Vacuum Induction Melted, 1975°F
(1080°C) Solution Heat Treated

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Comments on this Standard are invited from interested parties and can be submitted in writing to SAE Headquarters.

2.1.2 Aerospace Standards:

- MA 1370 - Metric Screw Threads - MJ Profile
- MA 1518 - Bolts, Screws and Nuts - External Wrenching, Metric MJ Threads - Design Parameters For
- MA 1520 - Areas for Calculating Stress or Load for Metric MJ Externally Threaded Fasteners
- MA 1566 - Gaging Practice and Gage Requirements for MJ Metric Screw Threads
- AS 3062 - Bolts, Screws and Studs, Screw Thread Requirements
- AS 3063 - Bolts, Screws and Studs, Geometric Control Requirements

2.2 ASTM Publications: Available from American Society for Testing and Materials, 1916 Race Street, Philadelphia, PA 19103.

- ASTM E8 - Tension Testing of Metallic Materials
- ASTM E112 - Determining Average Grain Size
- ASTM E139 - Conducting Creep, Creep-Rupture, and Stress-Rupture Tests of Metallic Materials

2.3 ANSI Publications: Available from American National Standards Institute, 1430 Broadway, New York, NY 10018.

- ANSI/ASME B46.1 - Surface Texture (Surface Roughness, Waviness, and Lay)

2.4 U.S. Government Publications: Available from Commanding Officer, Naval Publications and Forms Center, 5801 Tabor Avenue, Philadelphia, PA 19120.

2.4.1 Military Standards:

- MIL-STD-105 - Sampling Procedures and Tables for Inspection by Attributes
- MIL-STD-1312 - Fastener Test Methods

3. TECHNICAL REQUIREMENTS:

3.1 Material: Shall be AMS 5708 heading stock.

3.2 Design: Finished (completely manufactured) parts shall conform to the following requirements:

3.2.1 Dimensions: The dimensions of finished parts, after all processing including plating, shall conform to the part drawing. Dimensions shall apply before coating with dry film lubricants.

3.2.2 Surface Texture: Surface texture of finished parts, prior to plating or coating, shall conform to the requirements as specified on the part drawing, determined in accordance with ANSI/ASME B46.1.

3.2.3 Threads: Metric screw thread MJ profile and dimensions shall be per MA 1370, unless otherwise specified.

3.2.3.1 Incomplete Threads: Incomplete threads are permissible at the chamfered end and the juncture of the unthreaded portion of the shank or adjacent to the head as specified in AS 3062.

3.2.3.2 Chamfer: The entering point of the thread shall be chamfered as specified on the part drawing.

3.2.4 Geometric Tolerances: Part features shall be within the geometric tolerances specified on the part drawing and, where applicable, controlled per AS 3063.

3.3 Fabrication:

3.3.1 Blanks: Heads shall be formed by hot or cold forging; machined heads are not permitted, except lightening holes may be produced by any suitable method. Wrenching recesses may be forged or machined. Flash or chip clearance in machined recesses shall not cause recess dimensions to exceed the specified limits.

3.3.2 Heat Treatment: Headed blanks shall, before finishing the shank and the bearing surface of the head, cold working the head-to-shank fillet radius, and rolling the threads, be solution and stabilization heat treated as follows; precipitation heat treatment shall follow cold working of the fillet radius and rolling the threads:

3.3.2.1 Heating Equipment: Furnaces may be any type ensuring uniform temperature throughout the parts and shall be equipped with, and operated by, automatic temperature controllers. The heating medium shall not cause surface hardening by carburizing or nitriding.

3.3.2.2 Solution Heat Treatment: Blanks shall be solution heat treated by heating to a temperature within the range 1040-1080°C, holding at the selected temperature within $\pm 15^\circ\text{C}$ for 1 to 4 hr, and cooling at a rate equivalent to air cool or faster.

3.3.2.2.1 A temperature lower than 1040°C may be used provided that the furnace control is such that during the holding period no part is below 1025°C.

3.3.2.3 Stabilization Heat Treatment: Solution heat treated blanks shall be stabilization heat treated by heating to $845^\circ\text{C} \pm 8$, holding at heat for $4 \text{ hr} \pm 0.5$, and cooling in air.

3.3.2.4 Precipitation Heat Treatment: After cold working the fillet radius as in 3.3.4 and rolling the threads as in 3.3.5, parts shall be precipitation heat treated by heating to $760^\circ\text{C} \pm 8$, holding at heat for $16 \text{ hr} \pm 1$, and cooling in air.

- 3.3.3 Oxide Removal: Surface oxide and oxide penetration resulting from prior heat treatment shall be removed from the full body diameter and the bearing surface of the head of the solution and stabilization heat treated blanks prior to cold working the fillet radius and rolling the threads. The oxide removal process shall produce no intergranular attack or corrosion of the blanks. The metal removed from the bearing surface of the head and the full body diameter of the shank shall be as little as practicable to obtain a clean, smooth surface and in no case shall be so great as to produce more cutting of flow lines in the head-to-shank junction than shown in Fig. 1B.
- 3.3.4 Cold Working of Fillet Radius: After removal of oxide as in 3.3.3, the head-to-shank fillet radius of headed parts having the radius complete throughout the circumference of the part shall be cold worked sufficiently to remove all visual evidence of grinding or tool marks. Distortion due to cold working shall conform to Fig. 2 unless otherwise specified on part drawing. It shall not raise metal more than 0.05 mm above the contour at "A" or depress metal more than 0.05 mm below the contour at "B" as shown in Fig. 2; distorted areas shall not extend beyond "C" as shown in Fig. 2. In configurations having an undercut associated with the fillet radius, the cold working will be required only for 90 deg of fillet arc, starting at the point of tangency of the fillet radius and the bearing surface of the head. In addition to cold working the head-to-shank fillet radius, shouldered bolts, having an unthreaded shank diameter larger than the thread major diameter and having an undercut associated with a fillet between the threaded shank and the shoulder of the unthreaded shank, the cold working will be required only for 90 deg of fillet arc, starting at the point of tangency of the fillet radius and the shouldered surface of the unthreaded shank. For parts with compound radii between head and shank, cold work only the radius that blends with the head.
- 3.3.5 Thread Rolling: Threads shall be formed on the finished blanks by a single rolling process after removal of oxide as in 3.3.3.
- 3.3.6 Cleaning: Parts, after finishing, shall be degreased and then immersed in one of the following solutions for the time and the temperature shown:
- One volume of nitric acid (sp gr 1.42) and 9 volumes of water for not less than 20 min. at room temperature.
 - One volume of nitric acid (sp gr 1.42) and 4 volumes of water for 30-40 min. at room temperature.
 - One volume of nitric acid (sp gr 1.42) and 4 volumes of water for 10-15 min. at 60-70°C.
- 3.4 Product Marking: Each part shall be identification marked as specified by the part drawing. Unless otherwise specified, the markings may be formed by forging or stamping, raised or depressed not more than 0.25 mm max, with rounded root form on depressed characters.

3.5 Plating: Where required, all surfaces shall be plated as specified by the part drawing.

3.6 Mechanical Properties: Parts shall conform to the requirements of 3.6.1, 3.6.2 and 3.6.3. Threaded members of gripping fixtures for tensile and stress-rupture tests shall be of sufficient size and strength to develop the full strength of the part without stripping the thread. The loaded portion of the shank shall have three full thread turns from thread runout exposed between the loading fixtures during tensile and stress-rupture tests. Finished parts shall be tested in accordance with the following applicable test methods of MIL-STD-1312.

Requirement	Test Method
Hardness	No. 6
Room Temperature Tensile Strength	No. 108
Stress-Rupture	No. 10

3.6.1 Tensile Strength at Room Temperature:

3.6.1.1 Finished Parts: Parts shall withstand the minimum tensile load specified in Table II. If the size or shape of the part is such that failure would occur outside the threaded section but the part can be tested satisfactorily, such as parts having a shank diameter equal to or less than the thread root diameter or having an undercut, parts shall conform to only the tensile strength requirements of 3.6.1.2; for such parts, the diameter on which stress is based shall be the actual measured minimum diameter of the part. Tension fasteners with either standard spline drive or hexagon-type heads having a minimum metal condition in the head equal to the design parameters specified in MA 1518 shall not fracture in the head-to-shank fillet radius except when this radius is associated with an undercut or with a shank diameter less than the minimum pitch diameter of the thread.

3.6.1.2 Machined Test Specimens: If the size or shape of the part is such that a tensile test cannot be made on the part, tensile tests shall be conducted in accordance with ASTM E8 on specimens prepared as in 4.3.3. Such specimens shall meet the following requirements:

Tensile Strength, min	1210 MPa
Yield Strength at 0.2% Offset, min	790 MPa
Elongation in 5D, min	15%
Reduction of Area, min	18%

3.6.1.2.1 When permitted by purchaser, hardness tests on the end of parts may be substituted for tensile tests of machined specimens.

3.6.2 Hardness: Shall be uniform and within the range 34-44 HRC or equivalent, but hardness of the threaded section and of the head-to-shank fillet area may be higher as a result of the cold working operations.

3.6.3 Stress-Rupture Strength at 735°C:

3.6.3.1 Finished Parts: Finished parts, maintained at $735^{\circ}\text{C} + 2$ while the tensile load specified in Table II is applied continuously, shall not rupture in less than 23 hours. If the shank diameter of the part is less than the maximum minor diameter of the thread but the part can be tested satisfactorily, parts shall conform to the requirements of 3.6.3.1.1.

3.6.3.1.1 Parts having a shank diameter less than the maximum minor diameter of the thread shall be tested as in 3.6.3.1 except that the load shall be as specified in 3.6.3.2. The diameter on which stress is based shall be the actual measured minimum diameter of the part.

3.6.3.2 Machined Test Specimens: If the size or shape of the part is such that a stress-rupture test cannot be made on the part, a test specimen prepared as in 4.3.3, maintained at $735^{\circ}\text{C} + 2$ while a load sufficient to produce an initial axial stress of 520 MPa is applied continuously, shall not rupture in less than 23 hours. Tests shall be conducted in accordance with ASTM E139.

3.7 Quality: Parts shall be uniform in quality and condition, clean, sound, smooth, and free from burrs and foreign materials and from internal and external imperfections detrimental to their performance.

3.7.1 Macroscopic Examination: Parts or sections of parts as applicable, etched in a solution consisting of approximately 40% hydrochloric acid (sp gr 1.19), 10% of a 30% solution of hydrogen peroxide, and 50% water, or other suitable etchant, for sufficient time to reveal flow lines but not longer than 30 min., shall be examined at a magnification of approximately 20X to determine conformance to the following requirements, except that examination for the thread imperfections as specified in 3.7.1.3 may be made by microscopic examination of specimens polished and etched as in 3.7.2.

3.7.1.1 Flow Lines:

3.7.1.1.1 Head-to-Shank: Examination of a longitudinal section through the part shall show flow lines in the shank, head-to-shank fillet, and bearing surface which follow the contour of the part as shown in Fig. 1A, except that slight cutting of flow lines by oxide removal process of 3.3.3 is permissible as shown in Fig. 1B; excessive cutting of flow lines in the shank, head-to-shank fillet, and bearing surface, as shown in Fig. 1C, is not permissible except when an undercut is associated with the fillet radius. The head style shown in Figs. 1A through 1C is for illustrative purposes only but other symmetrical head styles shall conform to the above requirements. Flow lines in heads on parts having special heads, such as Dee- or Tee-shaped heads or thinner than MA 1518 standard heads, shall be as agreed upon by purchaser and vendor.

- 3.7.1.1.2 Threads: Flow lines in threads shall be continuous, shall follow the general thread contour, and shall be of maximum density at root of thread (See Fig. 3).
- 3.7.1.2 Internal Defects: Examination of longitudinal sections of the head and shank and of the threads shall reveal no cracks, laps, or porosity except laps in threads as permitted in 3.7.1.3.3 and 3.7.1.3.4. The head and shank section shall extend not less than $D/2$ from the bearing surface of the head and the threaded section shall extend not less than $D/2$ beyond the thread runout where "D" is the nominal diameter of the shank after heading. If the two sections would overlap, the entire length of the part shall be sectioned and examined as a whole.
- 3.7.1.3 Threads:
- 3.7.1.3.1 Root defects such as laps, seams, notches, slivers, folds, roughness, and oxide scale are not permissible (See Fig. 4).
- 3.7.1.3.2 Multiple laps on the flanks of threads are not permissible regardless of location. Single laps on the flanks of threads that extend toward the root are not permissible (See Figs. 5 and 6).
- 3.7.1.3.3 There shall be no laps along the flank of the thread below the pitch diameter (See Fig. 7). A single lap is permissible along the flank of the thread above the pitch diameter on either the pressure or non-pressure flank (one lap at any cross-section through the thread) provided it extends toward the crest and generally parallel to the flank (See Fig. 7).
- 3.7.1.3.4 Crest craters, crest laps, or a crest lap in combination with a crest crater are permissible provided that the imperfections do not extend deeper than 20% of the basic thread height (See Table I) as measured from the thread crest when the thread major diameter is at minimum size (See Fig. 8). The major diameter of the thread shall be measured prior to sectioning. As the major diameter of the thread approaches maximum size, values for depth of crest crater and crest lap imperfections listed in Table I may be increased by one-half of the difference between the minimum major diameter and actual major diameter as measured on the part.
- 3.7.2 Microscopic Examination: Specimens cut from parts shall be polished, etched in Kalling's reagent (100 cm³ of absolute ethyl alcohol, 100 cm³ of hydrochloric acid (sp gr 1.19), and 5 g of cupric chloride), Marble's reagent (20 cm³ of hydrochloric acid (sp gr 1.19), 20 cm³ of water, and 4 g of cupric sulfate pentahydrate), or other suitable etchant, and examined at not lower than 100X magnification to determine conformance to the requirements of 3.7.1.3, 3.7.2.1, 3.7.2.2, and 3.7.2.3.

- 3.7.2.1 Microstructure: Parts shall have microstructure of completely recrystallized material except in the area of the threads and the head-to-shank fillet radius.
- 3.7.2.2 Grain Size: Shall be predominantly 2-6 with no grains finer than 7 or coarser than 1 as determined by comparison of the specimen with the chart in ASTM E112. In case of disagreement on grain size by the comparison method, the intercept (Heyn) procedure shall be used.
- 3.7.2.3 Surface Hardening: Parts shall have no change in hardness from core to surface except as produced during cold working of the head-to-shank fillet radius and during rolling of threads. There shall be no evidence of carburization or nitriding. In case of dispute over results of the microscopic examination, microhardness testing shall be used as a referee method; a Vickers hardness reading within 0.08 mm of an unrolled surface which exceeds the reading in the core by more than 30 points shall be evidence of nonconformance to this requirement.
- 3.7.3 Fluorescent Penetrant Inspection: Parts shall be subject to fluorescent penetrant inspection in accordance with AMS 2645.
- 3.7.3.1 The following conditions shall be cause for rejection of parts inspected.
- 3.7.3.1.1 Discontinuities transverse to grain flow (i.e., at an angle of more than 10 degrees to the axis of the shank), such as grinding checks and quench cracks.
- 3.7.3.1.2 Longitudinal indications (i.e., at an angle of 10 degrees or less to the axis of the shank) due to imperfections other than seams, forming laps, and nonmetallic inclusions.
- 3.7.3.2 The following conditions shall be considered acceptable on parts inspected.
- 3.7.3.2.1 Parts having longitudinal indications (i.e., at an angle of 10 degrees or less to the axis of the shank) of seams and forming laps parallel to the grain flow that are within the limits specified in 3.7.3.2.2 thru 3.7.3.2.5 provided the separation between indications is not less than 1.6 mm in all directions.
- 3.7.3.2.2 Sides of Head: There shall be not more than three indications per head. The length of each indication may be the full height of the surface but no indication shall break over either edge to a depth greater than 0.8 mm or the equivalent of the basic thread height (See Table I), whichever is less.
- 3.7.3.2.3 Shank or Stem: There shall be not more than five indications. The length of any indication may be 5 mm with a depth not exceeding 0.05 mm but the total length of all indications shall not exceed twice the length of the surface. No indication shall break into a fillet or over an edge.

3.7.3.2.4 Threads: There shall be no indications, except as permitted in 3.7.1.3.

3.7.3.2.5 Top of Head and End of Stem: The number of indications is not restricted but the depth of any individual indication shall not exceed 0.25 mm, as shown by sectioning representative samples. No indication, except those of 3.7.3.2.2 shall break over an edge.

4. QUALITY ASSURANCE PROVISIONS:

4.1 Responsibility for Inspection: The vendor of parts shall supply all samples and shall be responsible for performing all required tests. Results of such tests shall be reported to the purchaser as required by 4.4. Purchaser reserves the right to perform such confirmatory testing as he deems necessary to ensure that the parts conform to the requirements of this specification.

4.2 Classification of Tests: The inspection and testing of parts are classified as follows:

- a) Acceptance tests as in 4.3.1 which are to be performed on each production inspection lot.
- b) Periodic tests which are to be performed periodically on production lots at the discretion of the vendor or purchaser. None required in this specification.

4.3 Production Inspection Lot: A production inspection lot shall be all finished parts of the same part number, made from a single heat of alloy, heat treated at the same time to the same specified condition, produced as one continuous run, and submitted for vendor's inspection at the same time.

4.3.1 Acceptance Tests: The acceptance tests shall be performed on each production inspection lot. The acceptance tests consist of all the tests specified in Table III.

4.3.2 Acceptance Test Sampling:

4.3.2.1 Non-Destructive Test - Visual and Dimensional: A random sample will be selected from each production inspection lot; the size of the sample to be as specified in Table IV. The classification of defects for parts shall be as specified in Table V. Defects not classified in Table V shall be classified as Minor B defects. All dimensional characteristics are considered defective when out of tolerance.

4.3.2.2 Hardness Test (See 3.6.2): A random sample shall be selected from each production inspection lot; the size of the sample shall be as specified in Table VI, column A. The sample units may be selected from those that have been subjected to and passed the visual and dimensional inspection, with additional units selected at random from the production inspection as necessary.

- 4.3.2.3 Non-Destructive Inspection: Parts shall be subject to fluorescent penetrant inspection.
- 4.3.2.4 Destructive Tests: A random sample shall be selected from each production inspection lot; the size of the sample shall be as specified in Table VI, column B. The sample units may be selected from those that have been subjected to and passed the non-destructive tests with additional units selected at random from the production inspection lot as necessary.
- 4.3.3 Test Specimens: Specimens for tensile and stress-rupture testing of machined test specimens shall be of standard proportions in accordance with ASTM E8 with either 6 mm diameter at the reduced parallel gage section or smaller specimens proportional to the standard when required. Specimens shall be machined from finished parts or coupons of the same lot of alloy and be processed together with the parts they represent. Specimens shall be machined from the center of parts 18 mm and under in diameter, from the center of coupons 20 mm and under in nominal diameter or distance between parallel sides, and from mid-radius of larger parts or coupons.
- 4.3.4 Acceptance Quality: The acceptance quality level and acceptance number of defectives for the acceptance tests shall be as specified in Tables IV and VI.
- 4.4 Reports: The vendor of parts shall furnish with each shipment a report stating that the chemical composition of the parts conform to the applicable material specification, showing the results of tests to determine conformance to the room-temperature tensile property, hardness, and stress-rupture requirements, and stating that the parts conform to the other technical requirements of this specification. This report shall include the purchase order number, this specification number, contractor or other direct supplier of material, part number, nominal size, and quantity.
- 4.5 Resampling and Retesting: If any part or specimen used in the above tests fails to meet the specified requirements for mechanical properties and quality as in 3.6 and 3.7, disposition of the parts may be based on the results of testing three additional parts or specimens for each original nonconforming part or specimen. Failure of any retest part or specimen to meet the specified requirements shall be cause for rejection of the parts represented and no additional testing shall be permitted. Results of all tests shall be reported.
5. PREPARATION FOR DELIVERY:
- 5.1 Packaging and Identification:
- 5.1.1 Parts having different part numbers shall be packed in separate containers.

5.1.2 Each container of parts shall be marked to show the following information:

- Ø METRIC FASTENERS, NICKEL BASE ALLOY, CORROSION AND HEAT RESISTANT
MA 3378A
PART NUMBER _____
PURCHASE ORDER NUMBER _____
QUANTITY _____
MANUFACTURER'S IDENTIFICATION _____

5.1.3 Threaded fasteners shall be suitably protected from abrasion and chafing during handling, transportation and storage.

5.1.4 Containers of parts shall be prepared for shipment in accordance with commercial practice and in compliance with applicable rules and regulations pertaining to the handling, packaging, and transportation of the product to ensure carrier acceptance and safe delivery. Packaging shall conform to carrier rules and regulations applicable to the mode of transportation.

5.1.5 For direct U.S.A. Military procurement, packaging shall be as specified in the request for procurement.

6. ACKNOWLEDGMENT: A vendor shall mention this specification number and its revision letter in all quotations and when acknowledging purchase orders.

7. REJECTIONS: Parts not conforming to this specification or to authorized modifications authorized by purchaser will be subject to rejection.

8. NOTES:

8.1 Marginal Indicia: The phi (Ø) symbol is used to indicate technical changes from the previous issue of this specification.

8.2 For direct U.S. Military procurement, purchase documents should specify not less than the following:

Title, number, and date of this specification
Part number or size of parts desired
Quantity of parts desired
Applicable level of packaging

TABLE I

Thread Pitch, mm	Basic Thread Height mm, Ref (See Note 1)	20% Basic Thread Height
0.5	0.30	0.06
0.6	0.36	0.07
0.7	0.42	0.08
0.8	0.48	0.10
1	0.60	0.12
1.25	0.75	0.15
1.5	0.90	0.18
1.75	1.05	0.21
2	1.20	0.24
2.5	1.50	0.30
3	1.80	0.36

Note 1. Basic thread height is defined as being equivalent to 0.6 times the pitch.

TABLE II

Thread Size	Tensile Strength Load kN min Standard MJ Threads Room Temp.	Stress-Rupture Tensile Test Load kN
3 x 0.5	6.175	2.398
3.5 x 0.6	8.318	3.218
4 x 0.7	10.78	4.161
5 x 0.8	17.39	6.786
6 x 1	24.69	9.589
7 x 1	35.33	13.95
8 x 1	47.87	19.14
10 x 1.25	74.81	29.91
12 x 1.25	112.3	45.52
14 x 1.5	152.0	61.46
16 x 1.5	203.9	83.15
18 x 1.5	263.4	108.1
20 x 1.5	330.4	136.3
22 x 1.5	405.1	167.8
24 x 2	468.2	192.1

Note 1. Requirements above apply to parts with metric MJ threads to the sizes shown, to class 4h6h tolerances. Area upon which stress for tensile strength load requirements is based on the tensile stress area as defined in MA 1520, for threads rolled prior to precipitation heat treatment, and calculated from equation:

$$A = 0.7854 [1/2 (d_2 \text{ max} + d_3 \text{ max})]^2$$

where, A = tensile stress area at mean dia between $d_2 \text{ max}$ & $d_3 \text{ max}$
 $d_2 \text{ max}$ = maximum pitch diameter
 $d_3 \text{ max}$ = maximum minor (root) diameter

Area upon which stress-rupture tensile test load requirements is based is the area at the maximum minor (root) diameter for MJ threads as defined in MA 1520, calculated from the equation:

$$A = 0.7854 (d_3 \text{ max})^2$$

where, A = area at maximum minor (root) diameter
 $d_3 \text{ max}$ = maximum minor (root) diameter

TABLE II (Continued)

Note 1. (Continued)

Load requirements are based on:

1210 MPa for tensile strength load

520 MPa for stress-rupture tensile test load

Note 2. For sizes not shown, tensile strength loads and stress-rupture tensile test loads for parts tested as parts, not as specimens machined from parts or from coupons of the stock, shall be based upon the respective areas and stresses given above.

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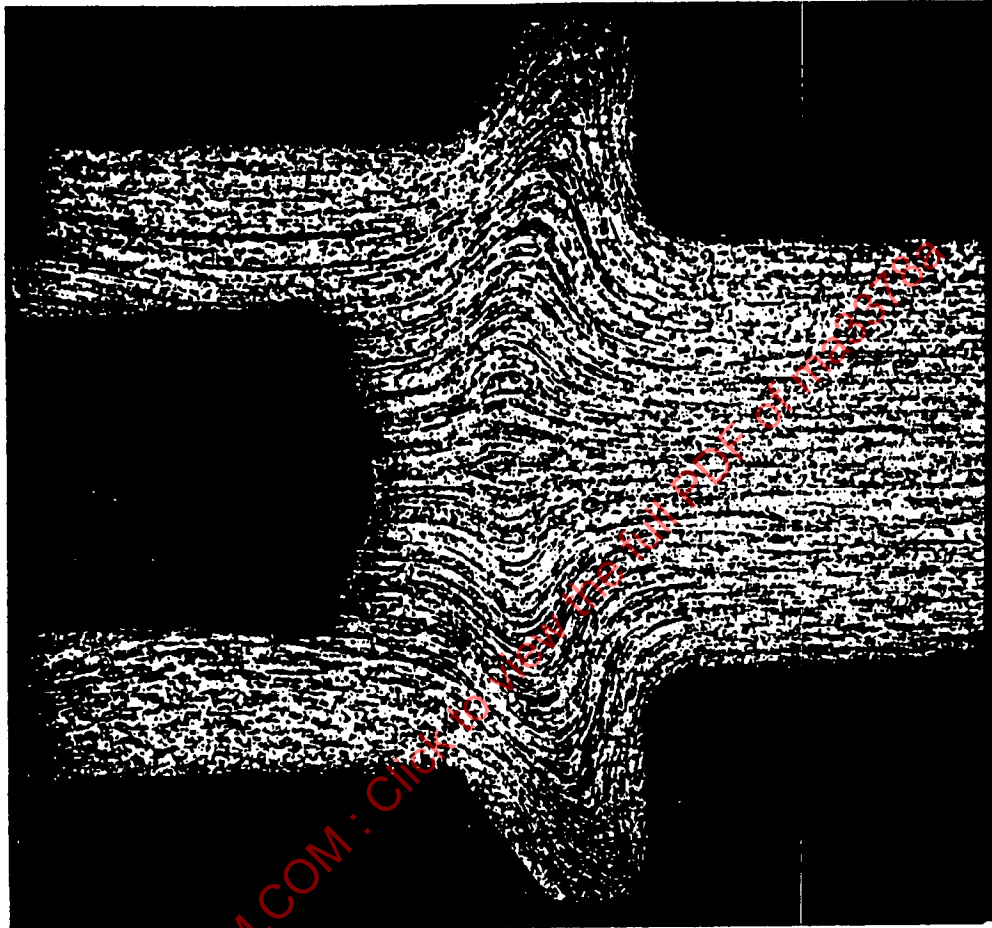


FIGURE 1A - SATISFACTORY GRAIN FLOW

Showing a smooth well formed grain flow following the contour of the under head fillet radius.

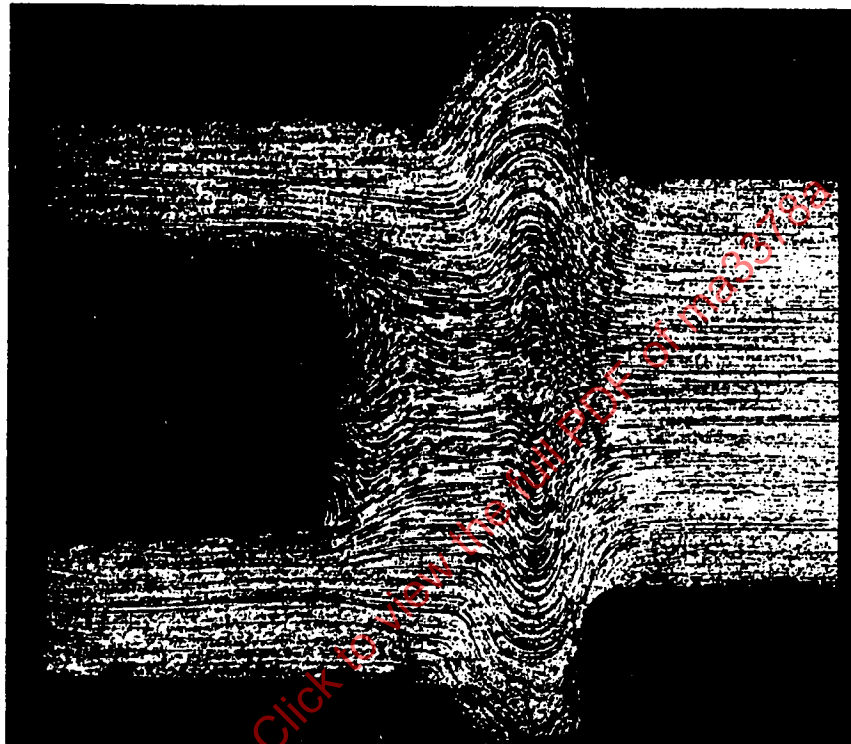


FIGURE 1B - MINIMUM ACCEPTABLE STANDARD

Showing maximum permissible cutting of grain flow
after machining to remove contamination oxide.

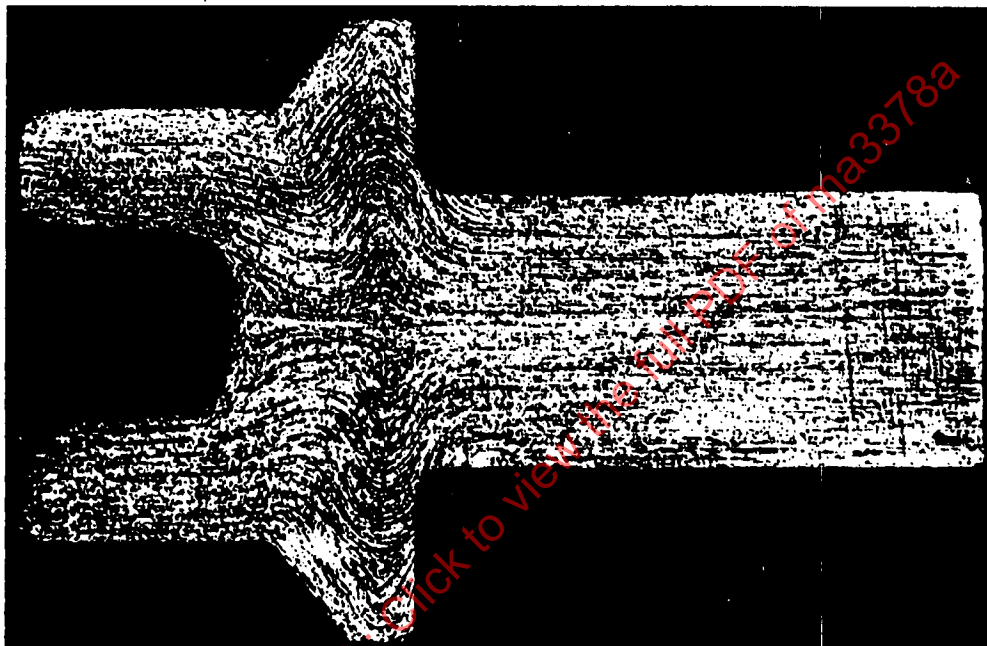
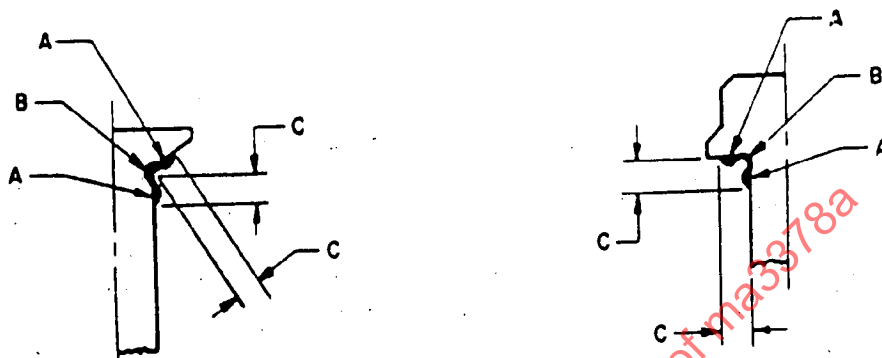


FIGURE 1C - UNACCEPTABLE GRAIN FLOW

Showing excessive cutting of grain flow in the shank, fillet and bearing surface which is not permissible.



Nominal Bolt
Diameter, mm

C, max
mm

Up to 8, excl
8 & 10
12 - 16 incl
18 - 24 incl
Over 24

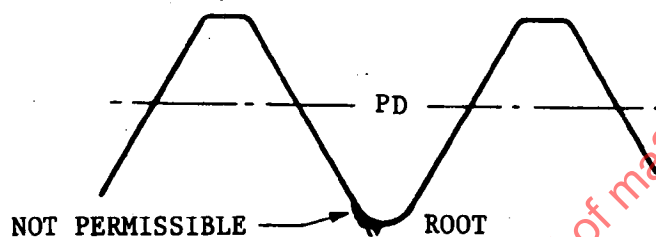
1.6
2.4
3.2
4.0
4.8

PERMISSIBLE DISTORTION FROM FILLET WORKING

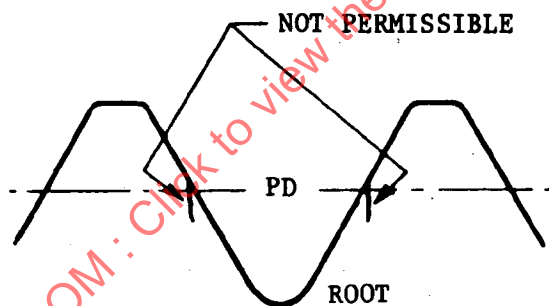
FIGURE 2



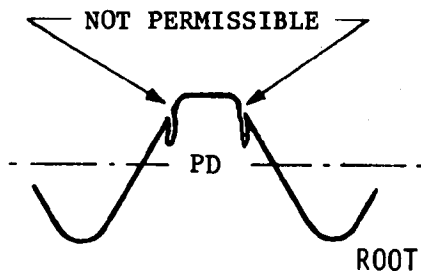
FLOW LINES, ROLLED THREAD
FIGURE 3



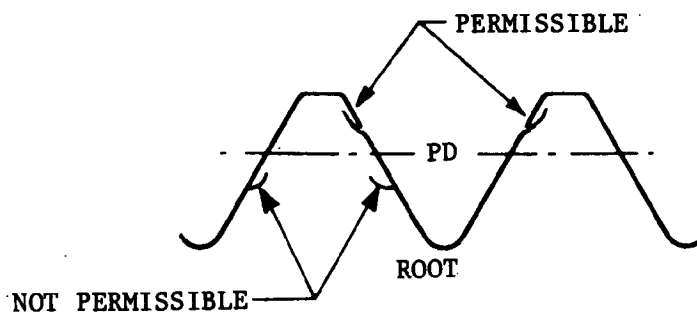
ROOT DEFECTS, ROLLED THREAD
FIGURE 4



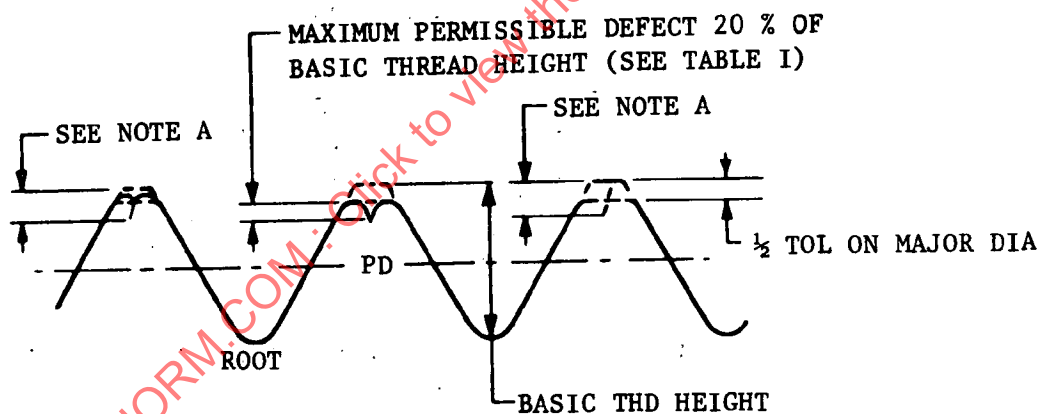
MULTIPLE LAPS BELOW PD EXTENDING TOWARD ROOT, ROLLED THREAD
FIGURE 5



MULTIPLE LAPS ABOVE PD EXTENDING TOWARD ROOT, ROLLED THREAD
FIGURE 6



LAPS EXTENDING TOWARDS CREST, ROLLED THREAD
FIGURE 7



Note A: Depth of defect equals 20% of basic thread height plus 1/2 the difference of the actual major diameter and minimum major diameter.

CREST CRATERS & CREST LAPS, ROLLED THREAD
FIGURE 8